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Development of Acceptance Plans for Airport Pavement Materials

Vol. I—Development

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Final Report

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| 16. Abstract The objective of this research is to develop statistically based acceptance/rejection plans and payment adjustment schedules for five specifications covered under the Federal Aviation Administrations (FAA) Advisory Circular (AC) No. 150/5370/10, Standards for Specifying the Construction of Airports, namely: P-152, Excavation and Embankment, P-209, Crushed Aggregate Base Course, P-304, Cement Treated Base Course, P-306, Econocrete Subbase Course, P-501, Portland Cement Concrete Pavement. Previously, the Pennsylvania State University developed plans for Specification P-401, Plant Mix Bituminous Pavements, which were adopted for use in 1984. This report includes the statistical analysis of data, development of payment adjustment plans (PAP), and development of PAP computer diskette system. (Test data used for this effort were collected from field sources. The developed PAP formulas, schedules, and computer diskette system were verified using new pavement construction projects. This report is divided into two volumes with Volume I, Development, describing the development of PAP, and Volume II, Computer Operator's Manual, describing the operation details of the PAP diskette system. (S100-1) | | | |
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| Approximate Conversions from Metric Measures | | | |
|--|-----------------------------------|-------------|------------------------|
| Symbol | When You Know | Multiply by | To Find |
| LENGTH | | | |
| m | meters | 39.37 | inches |
| cm | centimeters | 2.54 | inches |
| mm | millimeters | 0.03937 | inches |
| m | meters | 1.0936 | yards |
| km | kilometers | 0.62137 | miles |
| AREA | | | |
| m ² | square meters | 1.196 | square yards |
| ha | hectares (10,000 m ²) | 2.471 | acres |
| MASS (weight) | | | |
| g | grams | 0.00220462 | ounces |
| kg | kilograms | 2.20462 | pounds |
| t | tonnes (1000 kg) | 1.10231 | short tons |
| VOLUME | | | |
| m ³ | cubic meters | 35.234 | cubic feet |
| l | liters | 1.05669 | quarts |
| kl | kiloliters | 1.35982 | gallons |
| m ³ | cubic meters | 1.35 | cubic yards |
| TEMPERATURE (Celsius) | | | |
| °C | Celsius temperature | 1.8 | Fahrenheit temperature |
| °F | Fahrenheit temperature | 0.5556 | Celsius temperature |

METRIC CONVERSION FACTORS

PREFACE

The overall objective of this effort was to develop and test a statistically based acceptance plan and a payment adjustment schedule for five types of airport pavement materials.

The effort was divided into three work elements, with the first being existing pavement test data collection, the second being development of the acceptance and payment adjustment plan, and the third being testing of this plan.

Work Element No. 1 includes a literature search of any published reports of a similar nature, collection of applicable airport pavement test data, and performing a feasibility study of the practicality of having acceptance plans and payment adjustment schedules on certain materials. Important activities of this Work Element are listed in Chapter 2.

Work Element No. 2 includes an organizational analysis of collected data, development of PAP specifications and acceptance control procedures, and incorporation into a computerized program. Details of these activities are listed in Chapters 3 through 6 of this report.

Work Element No. 3 includes a field evaluation of the developed PAP computerized formulation program at airport pavement construction projects and a final fine tune adjustment of the PAP program. Details of these activities are listed in Chapters 7 through 10 of this report.

The study to develop the acceptance plans and payment adjustment schedules was awarded to John E. Foster and Associates, Inc., with Resource International, Inc. providing statistical analysis assistance.

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During the preparation of this report, Dr. Aston McLaughlin was the Technical Officer for the Federal Aviation Administration.

A special thanks to the Federal Aviation Administration offices, airport consultants/engineers, and airport authorities, who provided valuable information and test data. The list is too extensive to include here; however, it is included in Chapter 2, Table 2.4 of this report.

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LIST OF ABBREVIATIONS

Abbreviations

| | |
|-------------------|---|
| ANOVA | Analysis of Variance |
| AQL | Acceptable Quality Limit |
| BMDP | Biomedical Computer Programs |
| DBMS | Data Base Management System |
| DOS | Disk Operating System |
| EPAL _m | Estimated Percentage Above Limit |
| LTPD | Lot Tolerance Percent Defective |
| MS-DOS | Microsoft Disk Operating System |
| OC | Operating Characteristic |
| PAL | Percentage Above Limit |
| P-152 | P-152, Excavation and Embankment |
| P-209 | P-209, Crushed Aggregate Base Course |
| P-304 | P-304, Cement Treated Base Course |
| P-306 | P-306, Econocrete Subbase Course |
| P-401 | P-401, Bituminous Surface Course |
| P-501 | P-501, Portland Cement Concrete Pavement |
| PAP | Payment Adjustment Plans |
| PWL | Percent Within Limits |
| Q | Quality Index |
| QC | Quality Control |
| RQL | Rejection Quality Limit |
| SAS | Statistical Analysis System |
| SPSS | Statistical Programs Social Science |
| TRIS | Transportation Research Information Systems |
| UMVU | Uniformly Minimum Variance Unbiased |
| UQL | Unacceptable Quality Limit or (RQL) Rejection Quality Limit |

Organizations

| | |
|--------|--|
| AASHTO | American Association of State Highway and Transportation Officials |
| A/E | Architectural/Engineering |
| ASCII | American National Standard Code for Information Interchange |
| ASTM | American Society for Testing and Materials |
| DIALOG | Information Services, Inc., Palo Alto, CA |
| FAA | Federal Aviation Administration |
| FHWA | Federal Highway Administration |
| IBM | International Business Machines Corporation |
| JEFA | John E. Foster and Associates, Inc. |
| RII | Resource International, Inc. |
| TRB | Transportation Research Board |
| USCE | U.S. Army Corps of Engineers |
| WES | U.S. Army Corps of Engineers Waterways Experimental Station |

LIST OF SYMBOLS

| | |
|------------|---|
| \bar{x} | Average (of tests), sample mean |
| S | Standard Deviation |
| Q | Quality Index |
| L | Lower Limit of Material Specification |
| μ | Population mean |
| ϵ | $r * \sigma$ units by which the sample mean deviates from the population mean |
| $1-\delta$ | Probability of occurrence |
| σ | Population standard deviation |
| n | Sample size |
| r | real number |

1. INTRODUCTION

1.1 Background

In 1978, the Federal Aviation Administration (FAA) revised Item P-501, Portland Cement Concrete Pavement, to reflect research and updated practices in the field of concrete pavement construction. Among the major changes in the FAA specification is the adoption of flexural strength pay penalty factors based upon statistical concepts. Similarly, in 1981, the FAA adopted Item P-304, Cement-Treated Base Course, to include the field density as a criterion for its pay adjustment schedule.

Specifications for P-152, Excavation and Embankment, and P-209, Crushed Aggregate Base Course, have not been revised to include quality control criteria and pay penalty factors. Current FAA specifications for these items are based on acceptance/rejection density such that a minimum level of compaction must be achieved. P-306, Econocrete Subbase Course, was adopted in 1981, but has found little usage in the FAA Eastern Region.

Based on a need in the FAA Eastern Region, a payment adjustment schedule has been developed by the FAA for mat and joint densities, as well as for air voids in P-401 Bituminous Surface Course construction. This development was based on a statistical approach which evaluated test results from several airport construction sites in the FAA Eastern Region. The original approach was generated for the FAA by Pennsylvania State University and later field tested by Clemson University under two successive contracts.[5,6,7]

In September 1986, John E. Foster and Associates, Inc., was retained by the FAA to study the possibility of, and to develop, acceptance/rejection plans and payment adjustment schedules for the following specifications included in the FAA Advisory Circular (AC) No. 150/5370-10, Standards for Specifying the Construction of Airports:

- P-152, Excavation and Embankment.
- P-209, Crushed Aggregate Base Course.
- P-304, Cement Treated Base Course.
- P-306, Econocrete Subbase Course.
- P-501, Portland Cement Concrete Pavement.

This research study entitled "Development of Statistically Based Acceptance/Rejection Plans and Payment Adjustment Schedules for Airport Pavement Materials" was divided into three (3) major work elements.

These work elements were as follows:

- No. 1 Literature Review, Data Collection, and Feasibility Study.
- No. 2 Develop Statistical Payment Adjustment Schedules.
- No. 3 Field Testing of Payment Adjustment Schedule on Three (3) Construction Projects.

This Final Report summarizes work performed during Work Element Numbers 2 and 3, and contains important excerpts from Work Element No. 1 listed in Chapter 2.

1.2 Objectives

The overall objective of this effort were to develop a statistically based acceptance plan and a follow-up payment adjustment schedule applicable for specification densities, thicknesses, and/or strengths for the above listed five types of airport pavement materials. The methodology for this plan had previously been developed for the FAA and was utilized to apply to these new materials.

The objectives of Work Element No. 1 were to conduct a "Literature Search" from the appropriate technical documentation, conduct personal interviews, and collect and analyze airport pavement construction test data within the FAA Eastern Region. This effort included a "Feasibility Analysis" concerning the desirability of, and the best means of, assessing adjustments on all selected materials, except for P-501.

The objective of Work Element No. 2 was to utilize the airport pavement construction test data collected during Work Element No. 1 to calculate percentage factors which was to be a basis for the development of tabular payment adjustment schedules. The methodology used, and the computer simulations generated, during these exercises were similar to and compatible with those previously developed for the FAA by Pennsylvania State University and Clemson University on the P-401 material specifications.

Work Element No. 3 applied this developed payment adjustment schedule to three (3) construction projects to verify its application and refine the payment adjustment schedule.

Resource International, Inc. assisted John E. Foster and Associates, Inc. as a subcontractor, providing statistical analysis.

2. LITERATURE SEARCH, DATA COLLECTION, AND FEASIBILITY STUDY

2.1 Literature Search

A detailed review of existing literature was undertaken at the start of this study to:

- o Identify procedures and methods that exist, and can be used in statistical specification development.
- o Evaluate the applicability of various methods for determining pay adjustment plans.
- o Locate any published sources of data that could be used to supplement the data to be collected from the field.

Twenty-four sources of published information were obtained and reviewed to identify methods that had potential application to developing statistical curves and payment adjustment schedules for this study. In addition, unpublished work developed by William DeGraaff, Pavement Engineer, FAA Eastern Region Airports Division Office, relating to the P-401 and P-501 specifications were reviewed.

Of primary interest during the literature review was the question of how pay adjustment schedules (equations or tables) are derived, along with locating potential sources of test data for specifications considered by this study.

The general conclusions of the literature review on the subjects mentioned are:

- o Individual material quality test data are not reported in the literature that is generally available to the public, nor are data readily available from the airport operators/managers.
- o Test data are generally reported to the airport managers in the form of letter reports and these are generally not available without site and/or contractor visits.
- o The concepts used in statistical specification development are discussed in detail by several authors; the most notable of these are Weed, Willenbrock, Kopac, and Burati. There is general agreement that PAL methods and operating characteristic curves should be used. It is also proposed to follow these procedures in this study.
- o Very little guidance is offered for developing pay adjustment schedules for materials where lack of compliance effects cannot readily be determined from mechanistic design considerations.

- o Detailed statistical analysis of the test data was required for determining reasonable levels for pay factors which incorporate variabilities due to testing methods, in addition to within lot and among lot variabilities, as well as between contractor variabilities. The methods discussed by Burati and Siddiqui will be used in this study.

The following recommendations are made as a result of the literature review:

- o The PAL concept based on standard deviation should be used in developing operating characteristic curves.
- o Pay adjustment schedules should be developed based on detailed statistical analysis of quality control test data as well as engineering judgement.
- o Operating characteristic curves should be used in developing expected payment schedules.
- o Bonus payment plans should be considered to make payment schedules more receptive to the contractor.
- o The reasonableness of the combined payment schedule, based on various combinations of individual factors, should be investigated rather than relying on the procedures outlined by Burati or Weed.

2.2 Airport Data Collection

A vital activity of this study was collecting, assembling, editing, and entering airport pavement test data in an organized and accurate data base. This data base would provide the necessary information to perform statistical analysis during the Development of Statistical Payment Adjustment Schedules, Task D.

The test data collection phase consisted of several tasks including a search for published test data, establishing criteria for the airport data sources, establishing type and quantities of test data required, securing test data from possible sources, and sorting and entering the test data into a computer data base. The main focus on the data collection during Work Element No. 1 was confined to the seven (7) states of the FAA Eastern Region, which includes New York, New Jersey, Pennsylvania, Delaware, Maryland, Virginia, and West Virginia, and the District of Columbia. Data were obtained on 146 projects from 27 sources and cover 52 airports.

The majority of airports within the FAA Eastern Region are constructed with P-401, Bituminous Surface Course Pavement, more frequently than P-501, Portland Cement Concrete Pavement. P-304, Cement Treated Base Course, and P-306, Econocrete Subbase Course, are rarely used in construction in the FAA Eastern Region.

The literature search indicated very little published data was available, and that the needed quality control data would have to be collected from the field. Consequently, the original approach to the statistical data collection plan was revised. The revised plan was developed to secure, from the FAA District Offices, lists of airports that had pavement construction within the last ten years. Upon contacting the airport authorities, it was learned that they rarely had any test data available at the central office and referrals were made to their engineering consultants, where the majority of the test data was located.

Concurrently, while searching for published airport pavement construction test data, the five (5) specifications were reviewed and a collection Survey Information form was developed to assist the survey teams' interviews with the airport staff.

Meetings were held with the FAA Eastern Region Airports Division administrators and engineers in the four FAA Airport District Offices. They provided documentation on payment adjustment schedules that have not been published. A list of projects and sources of data were identified, with their assistance, and contacts were made with 45 airport staff and consultants in the seven state area of the Eastern Region. Overall, five (5) meetings were held with FAA offices and 31 meetings with airport staff and consultants. Refer to Table 2.1 for a list of these meetings.

The test data received were screened and analyzed for completeness, quantity, and quality, and compared to the airport selection criteria. It was then entered into a computer data base to be used for statistical analysis.

The original screening criteria established for acceptance/-rejection of test data sets were as follows:

- o Data to be from an Eastern Region airport.
- o Data to be for one of the five (5) specifications required for this effort.
- o Data must have at least 20 test points.
- o The contractor must be a "Competent contractor".
- o Any data "too perfect" or with abnormalities is to be rejected.

Additional criteria were established by the FAA as follows:

- o Use sand-cone test data only; no nuclear test data to be included.
- o Use flexural strength tests and thickness for Item P-501.
- o Data can be collected from nearby regions, if there are insufficient data within the Eastern Region. All data for a specification item must be collected from the same region.

While reviewing the test data for conformity with the required screening criteria, some problems were discovered as follows:

- o Very little test data contained the exact type of material specification that the test was performed on. The data had to be reviewed for pertinent information to indicate the material specification; sometimes there was still insufficient information to properly identify the material.
- o Some data sheets did not include the airport name or its location.
- o Some data sheets contained two different specification items on the same sheet, without specifying the difference between the two types of material.
- o Some Item P-501 test sheets did not indicate if the data were for pavements, foundations, or other structures.
- o Pavement tests below acceptable standards without apparent retesting or documentation of passing tests at the same location were frequent.
- o Some test sheets were disorganized and required considerable sorting of information to arrange into a usable and understandable form.

During the data entry phase, most data were transferred, rearranged, and edited from the test data sheets to the Survey Information forms, because of inconsistent test data sheets and lack of information. Refer to Tables 2.2, 2.3 and 2.4.

In order to make the effort manageable, the dBASE III data base computer program was selected for data entry operation. The software has superior data manipulation features that can be used during the statistical calculation phase of this study.

The total number of projects that were entered into the computer data base and appeared to be valid and usable were as follows:

| | | |
|-------|--|-------------|
| P-152 | Excavation and Embankment (Sand cone data). | 26 Projects |
| P-209 | Crushed Aggregate Base Course (Sand cone data)..... | 21 Projects |
| P-304 | Cement Treated Base Course..... | 05 Projects |
| P-306 | Econocrete Subbase Course Compressive Strength Data..... | 05 Projects |
| | Thickness Data..... | 01 Project |
| P-501 | Portland Cement Concrete Pavement Flexural Strength Data..... | 18 Projects |
| | Thickness Data..... | 03 Projects |

Screening the data for acceptable statistical analysis eliminated a large amount of collected data and resulted in the following acceptable data:

- o Item P-152, Excavation and Embankment: Data were collected on 57 projects; however, eliminating nuclear test data resulted in 26 projects and was sufficient to perform statistical analysis.
- o Item P-209, Crushed Aggregate Base Course: Data were collected on 40 projects; however, eliminating nuclear test data resulted in 21 projects, which was sufficient to perform statistical analysis.
- o Item P-304, Cement Treated Base Course: Data were collected on five projects tested by the sand cone method. Cement Treated Base Course has very limited application in the Eastern Region.
- o Item P-306, Econocrete Subbase Course: Data were collected on five projects using compressive tests with only one project with thickness data. Econocrete Subbase Course appears to be more prevalent in the Southern Region, than in the Eastern Region.
- o Item P-501, Portland Cement Concrete Pavement: Screening out small projects and compressive tests resulted in 18 acceptable flexural strength projects and were sufficient to develop operating curves. However, this data base contained only four projects with thickness data, which were insufficient to develop operating curves based on thickness.

2.3 Feasibility Study

The framework to conduct the feasibility study was divided into two steps:

- o Conduct a literature search for acceptable procedures that have been implemented in the field.
- o Based on the above, develop a plan to:
 - Outline the procedure for developing the Pay Adjustment Plan (PAP), considering applicability to this study.
 - Conduct the feasibility study.

The best means of developing PAP was to adopt the percent within limits (PAL) for specification acceptance plan, and the operating characteristic curve (OC) to relate the actual quantity measure to its probability of acceptance at any possible payment level.

The price adjustment is a policy-related measure determined by the user agency to be reasonable and equitable. The discrete price adjustment schedules for P-304 density and P-501 strength will be modified to a continuous adjustment curve. The price adjustment schedule of P-306 is currently based on thickness requirements; however, price adjustment on the basis of strength and thickness should be developed similar to that of Item P-501 in the current FAA specification.

Feasibility Study Approach

The objective of the feasibility study was to explore the desirability of, and the best means of, assessing adjustments on all selected materials, except for P-501. In this context, there were two steps to affect the feasibility study.

The first step was to consider the opinions of the various engineering staffs during the interviews and form a consensus of these opinions for each specification item. Recommendations were made to provide the best approach of a payment adjustment plan and an evaluation will be made of accuracy and precision of testing methods.

The second step was to evaluate the collected information and view its suitability for developing PAP. Following the first step and during the interviews, different opinions of the engineers and administrators about the use of Pay Adjustment Plans (PAP) for Items P-152, and P-209 were noticeable; PAP for Items P-304, P-306, and P-501 were generally accepted.

The following observations were representative of the opinions offered by the various consultants and airport agency staff engineers regarding PAP for Items P-152 and P-209:

- o Weaknesses and problems associated with these items are more expensive to correct, as it may require the removal of the surface and base course; whereas, problems with the surface layers are less expensive in comparison.
- o Experience shows that the contractor will factor into the bid price an allowance for penalties that might be imposed, which may result in a lesser quality product at a higher price.
- o Better pavement will result since the contractor will increase effort to achieve a higher quality control level in order to avoid penalties.
- o A weak spot in one area will not be offset by a 120 percent improvement in another. A weak spot will affect the performance of the entire runway.
- o There will be greater assurance of a high quality job since the contractor would likely recompact to receive 100 percent payment than to accept a penalty.
- o The use of PAP's should be included as an option for the contractor. In this case, a threshold level for recompaction should be specified as a requirement to comply with design and performance variables.
- o The use of PAP's will reduce the number of litigations, and will speed up the project by eliminating the questionable recompactions.

Information required to establish target specification limits and thresholds for recompaction for Items P-152 and P-209 are available. However, the impact of establishing these levels on performance and service life of the pavement as a whole will require further investigation.

As for the testing methodology for Items P-152 and P-209, again there was a diverse opinion about testing procedures; one was use of the sand cone method, ASTM D-1556, and the other was use of the nuclear gauge method, ASTM D-2922. FAA specification for Item P-209 allows both methods to be used, with the provision for adequate calibration of the nuclear gauge against standard material and against density obtained by the sand cone method at each project activity. The FAA specification does not allow for nuclear density testing on Item P-152.

As cited above, the second step in the feasibility study was directed to ascertain the above conclusions with objective evaluation derived from the collected data. Two methods to do this were:

- o To select subsets of data for each specification item and develop PAP trends (i.e., rough curves).
- o Select a statistically sound sample of data points for each specification item and evaluate its quality and reproducibility.

The second method was selected, wherein the analysis considered the following criteria:

- o Sample size (i.e. data quality): This measure was used to ensure that enough data was available to reach appropriate conclusions based on sound statistical methodology.
- o Data quality (i.e. variability): This measure was used to judge the variation of data within each project, as well as between projects, for each specification.
- o Analysis approach: Considering the collected data, a frame work for Work Element No. 2 analysis was outlined, accounting for the best means of assessing the pay adjustment plans.

Data Source and Availability

Data sets from 13 airports were considered for the analysis. The data included: 9 sets of P-152, 8 sets of P-209, 3 sets of P-304, and 5 sets of P-306. Due to the limitation of the computer package capability at this stage, the total number of data sets was limited to a maximum of ten. Additional data sets for Items P-304 and P-306 were not available at this time.

A list of the airports, with the corresponding specifications, are shown below:

| Airport | Specification(s)* |
|---|-----------------------|
| 1. Allentown-Bethlehem-Easton, PA | P-152, P-209 |
| 2. Chess-Lamberton, PA | P-152, P-209 |
| 3. Chesterland County, VA | P-152, P-304 |
| 4. DuBois-Jefferson County, PA | P-152 |
| 5. Greater Pittsburgh International, PA | P-152, P-209, P-306 |
| 6. Louisa County, VA | P-152 |
| 7. Pocono Mountains Municipal, PA | P-152, P-209 |
| 8. Manassas Mun./Davis Field, VA | P-152 (2 sets), P-304 |

| | |
|-------------------------------|----------------|
| 9. Lancaster, PA | P-209 |
| 10. Mifflin County, PA | P-209 (2 sets) |
| 11. Blue Ridge, VA | P-304 |
| 12. Harrisburg International, | P-306 (4 sets) |
| 13. Newark International, NJ | P-209 |

* One data set of each specification item, unless otherwise indicated.

Data Reduction and Manipulation

All raw data were transferred and organized on summary sheets. The summary sheets included the specification item, airport name, target specification, test number, and data test location (station and offset), density or strength values and percentage of target specification. These data were then entered in a data base (dBASE III Plus Software) for processing. At this initial stage, only the percentage of target specification was considered for the feasibility study analysis. The data sets that contained "retest" values of failed sections were eliminated.

The Biomedical Computer Programs (BMDP) package was used for statistical analysis. The data was transferred from dBASE III operating environment to other files (temporary) compatible with BMDP programs through an ASCII file. The BMDP procedures used are as follows:

- o BMD07D: Used to find mean (\bar{X}), standard deviation (σ), and coefficient of variation (CV).
- o BMD05D: Used to provide graphs and histograms.
- o BMD07D: Used to check data reliability.

Hardware/Software Requirements

The original approach of a payment adjustment schedule was generated for the FAA by Pennsylvania State University, field tested by Clemson University and applied to Item P-401. This study was to use the same methodology used by the original study, which had the statistical analysis performed on a mainframe computer with the final payment adjustment schedule in a chart form. This effort included writing programming on an IBM-compatible floppy data disks in amounts and contents as required to technically administer a computerized program, default files, and source program listing.

This required developing and performing the statistical analysis on an IBM compatible personal computer. The statistical analysis utilized the methodology similar to the original approach but in more detail.

- o Hardware requirements: IBM or compatible.
- o Software requirements: Several alternatives for use of available software packages have been identified. These are:
 - DBMS/analysis programs of Clemson (P-401) Study.
 - Engineering Economics Research, Inc.
 - Corps of Engineers programs.
 - Any other with the understanding that FAA's proprietary rights in the computer package is to be considered.

By reviewing the literature and contacting the relevant parties, the following was concluded:

- o The DBMS/analysis program of the Clemson (P-401) Study was developed for a mainframe environment and would need to be converted to a microcomputer environment for utilization in this study.
- o The PC-FOCUS was a self-contained DBMS/statistical analysis package; however, some of the required procedures for this study are not included (e.g. calculation of the area under the non-central t-distribution).
- o The Corps of Engineers used Lotus 1-2-3 for data manipulations and analyses on previous FAA projects. This program does not include the statistical procedures, as is required for this study.
- o Any other available source: Under this alternative, two options are available:
 - To use commercially available statistical packages (e.g. BMDP, SPSS, etc.) with DBMS (e.g. dBASE II, dBASE III, etc.) and develop interface softwares, as well as any required subroutine, not available in the commercial statistical package.
 - To convert the Clemson mainframe package to a micro-computer environment.

It should be noted that DBMS/statistical analysis procedure is an intermediate step required for the development of the pay adjustment plans, but not required by the end user. However, if FAA authority needs to fine-tune the adjustment plans when more data becomes available, or for any other reason, then the software of the intermediate step (or equivalent) will be needed.

Statistical Analysis and Results

Airports surveyed indicated that there are approximately 626 airports in the FAA Eastern Region, of which, data were collected on 30 airports, i.e. roughly 5 percent of all airports. 5 percent to 10 percent sample size is generally judged acceptable for the study purpose. Assuming that only 50 percent of the airports have construction projects relevant to this study, then the number of airports for each specification item, to satisfy sample size requirements, should be 15. Since airports can provide information on one or more construction projects, then the required number of airports (15 in this case) could be relaxed to about 10, provided that information on about 15 projects is available. The number of points required for each project depends on the required precision of the relevant specification items, as explained in the next paragraph.

The Weak Law of large numbers is often used by statisticians for determining the number of points required. This law is based upon "Tschebycheff's Inequality" which states that the probability that a random variable falls within $r\sigma$ units of μ is greater than or equal to $1 - 1/r^2$. The mathematical expression for this law is:

$$\text{Prob.}(|\bar{x} - \mu| < \epsilon) > 1 - \delta ; \delta > \sigma^2/n\epsilon^2 \quad (2-1)$$

where,

- \bar{x} = the sample mean,
- μ = the population mean,
- $\epsilon = r * \sigma$ units by which the sample mean deviates from the population mean,
- $1 - \delta$ = probability of occurrence,
- σ = the population standard deviation,
- n = sample size,
- r = real number.

Of importance are the following assumptions:

$\epsilon = r * \sigma = 1 * \sigma$; i.e., it is desirable to have the mean of the scores of any item for a project deviation from the true value by not more than one standard deviating unit. Furthermore, if at least 95 percent confident that $\epsilon = 1 * \sigma$ is required, then $1 - \delta = .95$.

To sum, the following could be written:

$$1 - \delta = 1 - \sigma^2/n\epsilon^2 \quad (2-2)$$

$$.95 = 1 - \sigma^2/n\sigma^2 = 1 - 1/n ; \text{ therefore } n = 20 \quad (2-3)$$

The number of data points required for each project should not be less than 20, in order to be at least 95 percent confident that the mean value for any specification item of any project will not deviate by more than one standard deviation unit of the true value.

Sample Size Requirements

In line with the above discussion, the minimum number of projects required for each specification item was 15, and the minimum number of data points for each project was 20. The following was concluded:

- o There was sufficient amount of data on specification Items P-152 and P-209 to carry out the feasibility study analysis and thereafter the development of PAP.
- o There was not sufficient amount of data on specification Items P-306 and P-309 to carry out the feasibility study analysis and thereafter the development of PAP.
- o Specification Item P-501 (thickness) was contractually excluded from the feasibility study.

As for Items P-304 and P-306, the question was not whether or not to collect more data for these two items, but whether or not it was desirable to do so. To answer this question, an analysis of the quality (or variability) of the data was conducted. Two outcomes were possible:

- o If the data quality was judged to be too variable, then it may not be desirable to collect more data.
- o If the data quality was judged to be good, then it was desirable to collect more data.

Data Quality

The quality measures include the sample mean value, \bar{x} , the sample standard deviation, s , the coefficient of variation CV ($CV = s/\bar{x}$), the maximum and minimum values, and the number of data points, N .

Most of the histograms show probability density function similar to the normal distribution; especially the graph for the "pool" of all projects of each specification item. Recalling the assumption that it is required to be 95 percent confident that the true value (μ of the spec. limit) does not deviate from the sample mean, \bar{x} , by more than one standard deviation, s , then:

$$\bar{x} * \mu/s = 1.645 \text{ and hence } |\bar{x} - \mu| = 1.645 s \quad (2-4)$$

By examining the values of Items P-152 and P-209, using the above formula, it could be concluded that all the average values are within the 95 percent confidence limits assumed.

The next question to be answered is whether or not the project's data for each specification item belong to the same population. To answer this question, a test of hypothesis was formulated as follows:

$$H_0 = \mu_1 = \mu_2 = \mu_3 = \dots = \mu \quad (2-5)$$

(called the null hypothesis)

$$H_1 = \text{not all } \mu \text{ are equal} \quad (2-6)$$

(called the alternative hypothesis)

with decision rule being,

$$F < F^* \text{ conclude } H_0 \quad (2-7)$$

$$F > F^* \text{ conclude } H_1 \quad (2-8)$$

where,

μ_i = is the population mean of Project i for the relevant specification item,

H_0 = the hypothesis that the population means are equal,

H_1 = the hypothesis that not all the population means are equal,

F = test statistic for the above hypothesis,

F^* = threshold value for F-statistic at any specified confidence limit.

By examining these results it can be concluded that the following projects contribute significantly to rejection of the null hypothesis:

Projects for Item P-152 = DUJ, W98, FKL,
 Projects for Item P-209 = EWR209, RVL209A,
 Projects for Item P-304 = ----,
 Projects for Item P-306 = MDT688.

DUJ, W98, FKL, EWR209, RVL209, and MDT688 are data base file names based on the three letter airport designation.

When these projects were eliminated from the data base, improvement of the F-statistic was noticeable and the null hypothesis was accepted at the 99 percent confidence limit only for Items P-209 and P-304. However, Item P-152 is still rejected under the null hypothesis. It can be concluded that the project's data for this item may represent two different populations. Accordingly, the results of the t-statistic were used to group Item P-152 projects into two sets. When these two groups were examined, it was found that projects in one group represented cohesive soil data and projects in the second group represented cohesionless soil data. Each set was then treated as if it was representing a population.

The F-ratio was calculated and the null hypothesis was accepted only after eliminating Project DUJ from Set #1 and Project W98 from Set #2. The only item showing some variability is Item P-306. There are data available for only 5 projects. The reduction to 4 projects by eliminating Project MDT68C has improved the F-ratio and the elimination of Project MDT68B further improved the F-ratio from 21.2 to 12.5. However, the null hypothesis was still rejected. It is believed that if more data was available, the procedure similar to the one used for Item P-152 may prove successful.

Conclusions:

In conclusion, the feasibility study indicated the following:

- o Statistical analysis could be performed on an IBM-compatible personal computer.
- o Analysis of the data obtained indicates that there was sufficient quality data to develop PAP for Items P-152 and P-209, and it was feasible to develop PAP for these two items.
- o There was not sufficient data at this point to develop PAP for Item P-304. However, it was desirable to collect data for this item since the analysis of collected data indicates that it was of good quality.
- o There was not sufficient data at this point to develop PAP for Item P-306. However, the data variability was judged to be marginal. One reason for this variation was the offset in the age at which the samples were tested (e.g. 36 days instead of 28 days). However, it was concluded that it was desirable to collect more data for this item, and select test data for only 28-day results.
- o Analysis of data for Items P-152 included two projects with the density values measured by the nuclear gauge. It was noted, however, that the effect of these two projects on the results is minor.

- o For Item P-152, it appeared that the variability of the material depends on the subgrade type (i.e., cohesive or cohesionless soil) more strongly than the type of test performed (i.e., sand cones versus nuclear gauge). In effect, a PAL specification could be developed for each of the two soil types with the test specification of the sand cone method. However, data for the nuclear gauge will be retained in the data base for future use.
- o The best means of developing a PAP was to develop a PAL specification for each item and use an OC curve to relate the actual quantity measured to its probability of acceptance at any possible payment level. In addition, a price adjustment schedule should be developed and used as a general policy measure for all items. Price adjustment should be fair and equitable to all contractors, as well as reasonable to the airport authority.
- o The opinions of the consulting engineers and airport agency staff engineers were too diverse to develop a position on the desirability of developing PAP adjustment plans for the specifications other than P-501. However, the plans should be developed and implemented on a selective basis until its practicality or otherwise can be determined.
- o The testing procedures and equipment in use are sufficiently accurate to assure reasonable values for purposes of pay adjustment plans.

TABLE 2.1
DATA COLLECTION VISITS

A meeting was held with the FAA Eastern Region Airports Division, Safety and Standards Branch as follows:

| | | |
|----------|----------------|---|
| 02/11/87 | Eastern Region | Mr. Carl Steinhauer, Manager Mr. William DeGraaf |
|----------|----------------|---|

Meetings were held with the four FAA District Offices as follows:

| | | |
|-----------|----------------|--|
| *03/16/87 | Washington ADO | Mr. William Whittle, Chief Mr. Terry Page Ms. Lori Lehnard |
| 04/03/87 | New York ADO | Mr. Robert Mendez, Manager Mr. Tom Felix Mr. Robert A. Bacza Mr. Kenneth P. Knoll Mr. Timothy Dyer Mr. John Moretto |
| 04/08/87 | Harrisburg ADO | Mr. Dan Cassidy Mr. Fred Waldmer |
| *04/10/87 | Beckley AFO | Mr. Joseph H. Scheff, Manager Mr. Jim Tartal |

The above listed meetings with the FAA District Offices resulted in the following meetings with airports, airport consultants/ engineers and airport authorities:

| | |
|-----------|--|
| *03/17/87 | Hayes, Seay, Mattern, Mattern; Rockville, MD |
| *03/24/87 | CH2M Hill; Reston, VA |
| 03/25/87 | Greiner Engineering; Timonium, MD |
| 03/25/87 | Washington National Airport, Engineering Div., Washington, D.C. |
| *03/26/87 | Manassas Municipal Airport; Manassas, VA |
| 03/26/87 | R.E. Byrd International Airport; Richmond, VA |
| *03/27/87 | Norfolk International Airport; Norfolk, VA |
| *03/27/87 | R. Kenneth Weeks, Engineer; Norfolk, VA |
| *05/11/87 | Washington County Airport; Washington, PA |
| *05/11/87 | Michael Baker, Jr., Inc.; Beaver, PA |
| *05/12/87 | Biro-Tech, Inc.; Coraopolis, PA |
| *05/13/87 | Pittsburgh International Airport, Pittsburgh, PA |
| *05/27/87 | Harrisburg international Airport, Middletown, PA |
| *05/27/87 | Lancaster Airport, Lancaster, PA |
| *05/28/87 | Sanders, Wall & Wyre, State College, PA |
| *05/28/87 | Mifflin County Airport, Reedsville, PA |
| *06/01/87 | Philadelphia International Airport, Philadelphia, PA |

TABLE 2.1 (continued)

| | |
|-----------|--|
| *06/02/87 | Pottstown-Limerick Airport, Pottstown, PA |
| *06/02/87 | Atlantic Engineers & Contractors, Inc., Kimberton, PA |
| *06/02/87 | G. Edwin Pidock Co., Allentown, PA |
| *06/10/87 | FAA Technical Center-Atlantic City Airport, Atlantic City, NJ |
| 06/16/87 | Washington National Airport, Washington, D.C. |
| 06/16/87 | Greiner Engineering, Washington National Airport |
| 06/18/87 | EI Group, East Orange, NJ |
| *06/23/87 | Hoyle, Tanner & Associates, Inc., Bedford, NH |
| *06/24/87 | Calcerinos-Spina, Liverpool, NY |
| *06/25/87 | Nigara Frontier Transportation Authority, Buffalo, NY |
| * | Delta Associates, P.E., Inc. Richmond, VA |
| * | Talbert, Cox and Associates, Wilmington, NC |
| * | The LPA Group of North Carolina, p.a., Raleigh, NC |
| * | Roy D. McQueen, Oakton, VA |
| * | L. Robert Kimball & Associates |
| * | New York Port Authority, New York, NY |
| * | Pan American World Airways, Inc., Teterboro, NJ |
| * | Lee-Simpson Associates, Inc., Dubois, PA |
| * | Stilson & Associates, Inc., Columbus, OH |

* Indicates data received.

TABLE 2.2
AIRPORT TEST DATA COLLECTED BY SPECIFICATION

Pavement construction test data collected from the FAA Eastern Region is as follows:

| | | |
|-------|------------------------------------|-------------|
| P-152 | Excavation & Embankment..... | 57 Projects |
| P-209 | Crushed Aggregate Base Course..... | 40 Projects |
| P-304 | Cement Treated Base Course..... | 12 Projects |
| P-306 | Econocrete Subbase Course | |
| | Compressive Strength Data..... | 05 Projects |
| | Thickness Data..... | 01 Project |
| P-501 | Portland Cement Concrete Pavement | |
| | Flexural Strength Data..... | 27 Projects |
| | Thickness Data..... | 04 Projects |

This test data have been collected from the following airports (not all the data were found to be usable):

o Item P-152, Excavation and Embankment:

1. Chesterfield County Airport, Chesterfield, VA (2 Projects)
2. Louisa County Airport, Louisa, VA
3. Buckhannon-Upshur County Airport, Buckhannon, WV
4. Allentown-Bethlehem-Easton, Allentown, PA (4 Projects)
5. Chester County-G.O. Carlson, Coatesville, PA
6. Chess-Lamberton Airport, Franklin, PA
7. DuBois-Jefferson County, DuBois, PA
8. Lancaster Airport, Lancaster, PA (2 Projects)
9. Westmoreland County Airport, Latrobe, PA
10. Pocono Mountains Municipal, Mount Pocono, PA (2 Projects)
11. Greater Pittsburgh International, Pittsburgh, PA (2 Projects)
12. Pottstown Limerick Airport, Pottstown, PA
13. Washington County Airport, Washington, PA (4 Projects)
14. Rochester Monroe County Airport, Rochester, NY
15. Syracuse-Hancock International, Syracuse, NY (3 Projects)
16. Virginia Highlands Airport, Abingdon, VA (2 Projects)
17. Roanoke Municipal/Woodrum Airport, Roanoke, VA (4 Projects)
18. Easton Municipal Airport, Easton, MD
19. Frederick Municipal Airport, Frederick, MD
20. New Kent County Airport, Quinton, VA (2 Projects)
21. Clarion County Airport, Clarion, PA (2 Projects)
22. Culpeper Municipal/T.I. Martin Airport, Culpeper, VA
23. Washington County Regional Airport, Hagerstown, MD (2 Projects)

TABLE 2.2 (continued)

24. Greater Buffalo International Airport, Buffalo, NY
 25. Charlottesville-Albermarle Airport, Charlottesville, VA
 26. Essex County Airport, Caldwell, NJ (2 Projects)
 27. East Hampton Airport, East Hampton, NY
 28. Niagara Falls International Airport, Niagara Falls, NY
(2 Projects)
 29. Mifflin County Airport, Reedsville, PA (2 Projects)
 30. Mercer County Airport, Bluefield, WV
 31. Martin State Airport, Baltimore, MD
 32. Manassas Municipal/Davis Field Airport, Manassas, VA (2
Projects)
 33. Teterboro Airport, Teterboro, NJ (2 Projects)
- o Item P-209, Crushed Aggregate Base Course:
1. Allentown-Bethlehem-Easton, Allentown, PA (7 Projects)
 2. Chess-Lamberton Airport, Franklin, PA
 3. Lancaster Airport, Lancaster, PA
 4. Westmoreland County Airport, Latrobe, PA (2 Projects)
 5. Pocono Mountains Municipal, Mount Pocono, PA
 6. Greater Pittsburgh International, Pittsburgh, PA
(2 Projects)
 7. Clinton County Airport, Plattsburgh, NY
 8. Syracuse-Hancock International, Syracuse, NY (3 Projects)
 9. Newark International Airport, Newark, NJ
 10. Virginia Highlands Airport, Abingdon, VA
 11. Chesterfield County Airport, Chesterfield, VA
 12. Roanoke Municipal/Woodrum Airport, Roanoke, VA
 13. Danville Municipal Airport, Danville, VA
 14. Easton Municipal Airport, Easton, MD
 15. New Kent County Airport, Quinton, VA (2 Projects)
 16. Patrick Henry International Airport, Newport News, VA
(2 Projects)
 17. Indiana County/Jimmy Stewart Airport, Indiana, PA
 18. VPI/Virginia Tech Airport, Blacksburg, VA (2 Projects)
 19. Doylestown Airport, Doylestown, PA
 20. Reading Municipal Airport, Reading, PA
 21. Baltimore-Washington International, Baltimore, MD
 22. Essex County Airport, Caldwell, NJ (2 Projects)
 23. East Hampton Airport, East Hampton, NY
 24. La Guardia Airport, New York, NY
 25. Washington National Airport, Washington DC
 26. Martin State Airport, Baltimore, MD

TABLE 2.2 (continued)

- o Item P-304, Cement Treated Base Course:
 - 1. Martin State Airport, Baltimore, MD
 - 2. Chesterfield County Airport, Chesterfield, VA
 - 3. Blue Ridge Airport, Martinsville, VA (2 Projects)
 - 4. Virginia Highlands Airport, Abingdon, VA
 - 5. Roanoke Municipal/Woodrum Airport, Roanoke, VA (2 Projects)
 - 6. Culpeper Municipal/T.I. Martin Airport, Culpeper, VA
 - 7. Washington County Regional Airport, Hagerstown, MD
 - 8. Manassas Municipal/Davis Field Airport, Manassas, VA
 - 9. Salisbury-Wicomico County Airport, Salisbury, MD
 - 10. Washington National Airport, Washington D.C.

- o Item P-306, Econocrete Subbase Course:
 - 1. Harrisburg International, Middletown, PA (4 Projects)
 - 2. Greater Pittsburgh International, Pittsburgh, PA

- o Item P-501, Portland Cement Concrete Pavement:
 - 1. Dulles International, Washington, D.C.
 - 2. Baltimore-Washington International, Baltimore, MD
 - 3. Charlottesville-Albermarle, Charlottesville, VA
 - 4. Norfolk International, Norfolk, VA (3 Projects)
 - 5. Salisbury-Wicomico County, Salisbury, MD
 - 6. Greater Pittsburgh International, Pittsburgh, PA (2 flex & 2 tk Projects)
 - 7. Greater Buffalo International, Buffalo, NY (3 flex & 1 tk Projects)
 - 8. Rochester Monroe County, Rochester, NY
 - 9. Syracuse-Hancock International, Syracuse, NY (2 Projects)
 - 10. FAA Tech Center, Atlantic City, NJ (1 flex & 1 tk Projects)
 - 11. Patrick Henry International Airport, Newport News, VA (2 Projects)
 - 12. Beaver County Airport, Beaver, PA
 - 13. Philadelphia International Airport, Philadelphia, PA
 - 14. Harrisburg International Airport, Middletown, PA (3 Projects)
 - 15. Niagara Falls International Airport, Niagara Falls, NY (2 Projects)
 - 16. Martin State Airport, Baltimore, MD
 - 17. Manassas Municipal/Davis Field Airport, Manassas, VA

TABLE 2.3
AIRPORT TEST DATA USED AS DATA BASE

The test data received were screened and analyzed by a pavement engineer for completeness, quantity, and quality and compared to the airport selection criteria. All projects that were found acceptable were then entered into a computer data base to be used for statistical analysis.

These acceptable projects were as follows:

| | | |
|-------|--|-------------|
| P-152 | Excavation & Embankment (Sand cone data)... | 26 Projects |
| P-209 | Crushed Aggregate Base Course (Sand cone data)..... | 21 Projects |
| P-304 | Cement Treated Base Course..... | 05 Projects |
| P-306 | Econocrete Subbase Course Compressive Strength Data..... | 05 Projects |
| | Thickness Data..... | 01 Project |
| P-501 | Portland Cement Concrete Pavement Flexural Strength Data..... | 18 Projects |
| | Thickness Data..... | 03 Projects |

The valid, usable data were from the following airports:

o Item P-152, Excavation and Embankment:

1. Chesterfield County Airport, Chesterfield, VA (2 Projects)
2. Allentown-Bethlehem-Easton, Allentown, PA (4 Projects)
3. Chester County-G.O. Carlson, Coatesville, PA
4. Chess-Lamberton Airport, Franklin, PA
5. Westmoreland County Airport, Latrobe, PA
6. Pocono Mountains Municipal, Mount Pocono, PA (2 Projects)
7. Pottstown Limerick Airport, Pottstown, PA
8. Washington County Airport, Washington, PA (4 Projects)
9. Syracuse-Hancock International, Syracuse, NY (3 Projects)
10. Virginia Highlands Airport, Abingdon, VA (2 Projects)
11. Roanoke Municipal/Woodrum Airport, Roanoke VA (4 Projects)
12. Easton Municipal Airport, Easton, MD
13. New Kent County Airport, Quinton, VA (2 Projects)
14. Washington County Regional Airport, Hagerstown, MD

o Item P-209, Crushed Aggregate Base Course:

1. Allentown-Bethlehem-Easton, Allentown, PA (6 Projects)
2. Pocono Mountains Municipal, Mount Pocono, PA
3. Clinton County Airport, Plattsburgh, NY

TABLE 2.3 (Continued)

4. Syracuse-Hancock International, Syracuse, NY (3 Projects)
 5. Newark International Airport, Newark, NJ
 6. Virginia Highlands Airport, Abingdon, VA
 7. Chesterfield County Airport, Chesterfield, VA
 8. Roanoke Municipal/Woodrum Airport, Roanoke, VA
 9. Easton Municipal Airport, Easton, MD
 10. New Kent County Airport, Quinton, VA (2 Projects)
 11. Doylestown Airport, Doylestown, PA
 12. Reading Municipal Airport, Reading, PA
 13. La Guardia Airport, New York, NY
- o Item P-304, Cement Treated Base Course:
1. Chesterfield County Airport, Chesterfield, VA
 2. Blue Ridge Airport, Martinsville, VA
 3. Virginia Highlands Airport, Roanoke, VA
 4. Roanoke Municipal/Woodrum Airport, Roanoke, VA (2 Projects)
- o Item P-306, Econocrete Subbase Course:
1. Harrisburg International, Middletown, PA (4 Projects)
 2. Greater Pittsburgh International, Pittsburgh, PA
- o Item P-501, Portland Cement Concrete Pavement:
1. Dulles International, Washington, D.C.
 2. Baltimore-Washington International, Baltimore, MD
 3. Charlottesville-Albermarle, Charlottesville, VA
 4. Norfolk International, Norfolk, VA
 5. Salisbury-Wicomico County, Salisbury, MD
 6. Greater Pittsburgh International, Pittsburgh, PA (2 flex & 2 tk Projects)
 7. Greater Buffalo International, Buffalo, NY (3 flex & 1 tk Projects)
 8. Rochester Monroe County, Rochester, NY
 9. Syracuse-Hancock International, Syracuse, NY (2 Projects)
 10. FAA Tech Center, Atlantic City, NJ (1 flex & 1 tk Projects)
 11. Patrick Henry International Airport, Newport News, VA
 12. Philadelphia International Airport, Philadelphia, PA
 13. Niagara Falls International Airport, Niagara Falls, NY (2 Projects)

TABLE 2.4
DATA COLLECTION SOURCES

Pavement test data sources, for Task C, were as follows:

1. Atlantic Engineers & Consultants, Inc., Kimberton, PA, Morris W. Holman, Jr.; Chester County Airport, Coatesville, PA; Pottstown Limerick Airport, Pottstown, PA.
2. Biro Tech, Inc., Corapolis, PA, Richard W. Dorothy; Beaver County Airport, Beaver, PA; Clarion County Airport, Clarion, PA; Indiana County/Jimmy Stewart Airport, Indiana, PA.
3. Calocerinos and Spina, Liverpool, NY, Bob Masterpol; Rochester Monroe County Airport, Rochester, NY; Syracuse-Hancock International Airport, Syracuse, NY.
4. CH2M Hill, Reston, VA, Micheal L. Churchill; Louisa County Airport, Louisa, VA.
5. Commonwealth of Pennsylvania, Bureau of Aviation, Middletown, PA, Francis F. Strouse; Harrisburg International Airport, Middletown, PA.
6. Delta Associates P.E., Inc., Richmond, VA, Charles Lamb; Easton Municipal Airort, Easton, MD; Fredrick Municipal, Frederick, MD; Washington County Regional Airport, Hagerstown, MD; Virginia Highlands Airport, Abingdon, VA; Chesterfields County Airport, Chesterfield, VA; Culpeper Municipal/Martin Airport, Culpeper, VA; Danville Municipal Airport, Danville, VA; Roanoke Municipal/Woodrum Airport, Roanoke, VA; New Kent County Airport, Quinton, VA.
7. FAA, Technical Center, Atlantic City, NJ, Bob J. Warner; Atlantic City Airport, Atlantic City, NJ.
8. FAA, Washington District Office, Falls Church, VA, William Whittle; Chesterfield County Airport, Chesterfield, VA.
9. FAA, West Virginia Field Office, Beaver, WV, Joseph H. Scheff; Mercer County Airport, Princeton, WV.
10. G. Edwin Pidcock Co., Allentown, PA, Sherwood F. Clause; Allentown-Bethlehem-Easton Airport, Allentown, PA; Pocono Mountain Municipal Airport, Mount Pocono, PA.; Reading Municipal Airport, Reading PA; Doylestown Airport, Doylestown, PA.

TABLE 2.4 (Continued)

11. Greater Pittsburgh International Airport, Pittsburgh, PA, William C. Stuenkel; Greater Pittsburgh International Airport, Pittsburgh, PA.
12. Hayes, Seay, Mattern and Mattern, Rockville, MD, Charles H. Porter; Baltimore/Washington International Airport, Baltimore, MD; Blue Ridge Airport, Martinsville, VA; Martin State Airport, Baltimore, MD; Norfolk International Airport, Norfolk, VA; Suffolk Municipal Airport, Suffolk, VA.
13. Hoyle, Tanner & Associates, Inc., Bedford, NH, Barry W. Lussier; East Hampton Airport, East Hampton, NY; Essex County Airport, Fairfield, NJ.
14. Lancaster Airport, Lancaster, PA, Norman Lamar; Lancaster Airport, Lancaster, PA.
15. Lee-Simpson Associates, Inc., DuBois, PA, Edward S. Nasuti; DuBois-Jefferson County Airport, DuBois, PA; Chess-Lamberton Airport, Franklin, PA; Westmoreland County Airport, Latrobe, PA.
16. The LPA GROUP of North Carolina, P.A., Raleigh, NC., James C. Farthing; Virginia Tech Airport, Blacksburg, VA.
17. L. Robert Kimball & Associates, Ebensburg, PA, William R. Reeves and Rick Genday; Buckhannon-Upshur County Airport, Buckhannon, WV.
18. Michael Baker, Jr., Inc., Beaver, PA, Allan R. Berenbrok; Washington County Airport, Washington, PA.
19. New York Port Authority, Jamaica, NY, Ray Finnegan; Newark International Airport, Newark, NJ; La Guardia Airport, New York, NY.
20. Niagara Frontier Transportation Authority, Buffalo, NY, Walt Zmuda; Greater Buffalo International Airport, Buffalo, NY; Niagara Falls Airport, Niagara Falls, NY.
21. Pan American World Airways, Inc., Teterboro Airport, NJ, Charles W. Kurtz; Teterboro Airport, Teterboro, NJ.
22. Philadelphia International Airport, Philadelphia, PA, Jay Beratan; Philadelphia International Airport, Philadelphia, PA.
23. R. Kenneth Weeks, Engineers, Norfolk, VA, Wilbur D. Marshall; Norfolk International Airport, Norfolk, VA.

TABLE 2.4 (Continued)

24. Roy D. McQueen & Associates, Oakton, VA, Roy D. McQueen; Charlottesville-Ablemarle Airport, Charlottesville, VA; Dulles International Airport, Washington, D.C.; Manassas Municipal Airport, Manassas, VA, Wicomico County Airport, Salisbury, MD.
25. Sanders, Wall and Wyre, State College, PA, Charles Wall; Mifflin County Airport, Reedsville, PA.
26. Stilson and Associates, Inc., Columbus, OH, David L. Weir; Wheeling-Ohio County Airport, Wheeling, WV.
27. Talbert, Cox and Associates, Inc., Wilmington, NC, John Talbert, III; Patrick Henry Airport, Newport News, VA.

Pavement test data sources, for Task F, were as follows:

28. FAA, Washington District Office, Falls Church VA, William Whittle and Kenneth C. Jacobs; Dulles International Airport, Washington D.C.
29. Greiner Engineering Services, Inc., Baltimore, MD; Baltimore/Washington International Airport, Baltimore, MD.
30. Mellon Stuart Company, Dick Enterprisers, Pittsburgh, PA, James A. Long and Kevin Wiley; Greater Pittsburgh International Airport, Pittsburgh, PA.
31. National Ready Mixed Concrete Association and the National Aggregates Association, Silver Spring, MD, Richard C. Meininger; Wichita Mid-Continent Airport, Wichita, KA.
32. R. Kenneth Weeks, Engineers, Norfolk, VA, Edward L. Owens; Norfolk International Airport, Norfolk, VA.

3. QUALITY CONTROL CONSIDERATIONS

3.1 Basic Concepts from Quality Control

This study was primarily concerned with use of statistically based ideas in the application of product quality control, as such a few comments initially on quality control are warranted.

Quality control is a general term that includes two different types of controls over the product. These are: accept/reject control and process control. Acceptance/rejection control is concerned with monitoring product quality as the product is delivered in batches or lots to the buyer. Accept/reject control involves the decision to accept or reject a lot based on a random sample from the lot. Process control, however, is concerned with the detection of changes in product performance and taking the necessary action to control the process to correct the change in performance. Accept/reject control is primarily the concern of the buyer while process control is primarily the concern of the producer. Both components of quality control, accept/reject and process controls, are based on statistical theories and associated sampling methods. A number of sampling schemes exist and are used in the various specifications. A brief discussion of sampling needs for accept/reject control will be presented in what follows. Since process control is not the explicit concern of this study, no further discussion of this component will be given.

3.2 The Accept/Reject Control Component

A preliminary judgement and an essential part of accept/reject control is an estimation of the material quality. In fact, when a producer delivers a lot of material, the engineer (consumer) needs to know the quality of the material in the lot. In the current FAA approach, if the lot quality is found to be at or above the consumer's upper quality standard, the consumer accepts the lot and pays the producer in full. On the other hand, if the lot quality is found to be at or below the consumer's lower quality standard, the consumer rejects the lot and pays the producer nothing. If the lot quality is found to be between the two quality standards, the consumer accepts the lot and pays the producer a reduced price according to a payment adjustment schedule, where the reduction depends on the level of lot quality.

The above scenario depends on the assumption that the quality of a lot can be known with certainty. Unfortunately, complete knowledge of lot quality requires 100% inspection - a task that is usually prohibitively expensive and sometimes impossible (destructive testing). An alternative to obtaining complete knowledge of quality relies on sampling and statistical acceptance plans to provide an estimate of lot quality.

An estimate of lot quality is subject to sampling variability. This implies that the payment decision for a few lots of suitable quality material would be penalized with rejection or a payment adjustment, and a few lots of poor quality material would get full payment. These two situations should be controlled in the payment adjustment.

3.3 Previous Work of Interest

Statistical acceptance plans have been in use for some time. A thorough treatment of the subject appeared as early as 1957, in the military publication MIL-STD 414.[1] A key element of that work is the formula for the best - uniformly minimum variance unbiased (UMVU) - estimate of the percentage of a lot of material above an arbitrary limit (PAL). A recent treatment of statistical acceptance plans appears in texts by Duncan [2] and Wetherill [3].

The methodology in MIL-STD 414 was applied to pavements in the middle 1970's by Willenbrock and Kopac [5,13]. This same methodology was applied to bituminous airport runway materials in 1979 by Burati and Willenbrock, [6]. Payment adjustment schedules were used in these applications [6,7]. The following work draws heavily on previous results for the statistical acceptance plan.

3.4 Accept/Reject Parameters

As mentioned earlier, primary tasks in this work are to develop a statistical acceptance plan and an integrated payment schedule that successfully deals with the variability in the estimate of lot quality. Using well known statistical procedures it was possible to determine the probability of acceptance for a specific lot quality. Typically, two numbers are determined that quantify the lower bound of acceptable quality and the upper bound of unacceptable quality. If 100% error-free inspection could be performed, these two numbers would be the same. In this scenario, the lot would be accepted if it met or exceeded the given quality limit; otherwise, the lot is rejected. Such an acceptance plan is illustrated by the operating characteristic (OC) curve of Figure 3.1.

Even if the inspection were nondestructive, 100% inspection, unless necessary, should be avoided if for no other reason than for cost considerations. Quality Control (QC) practices suggest choosing a sample of n items that will be the basis of any acceptance/rejection of the lot of material. Since the sample provides only an estimate of the lot quality, the choice of the two numbers mentioned above is based on probabilistic concerns.

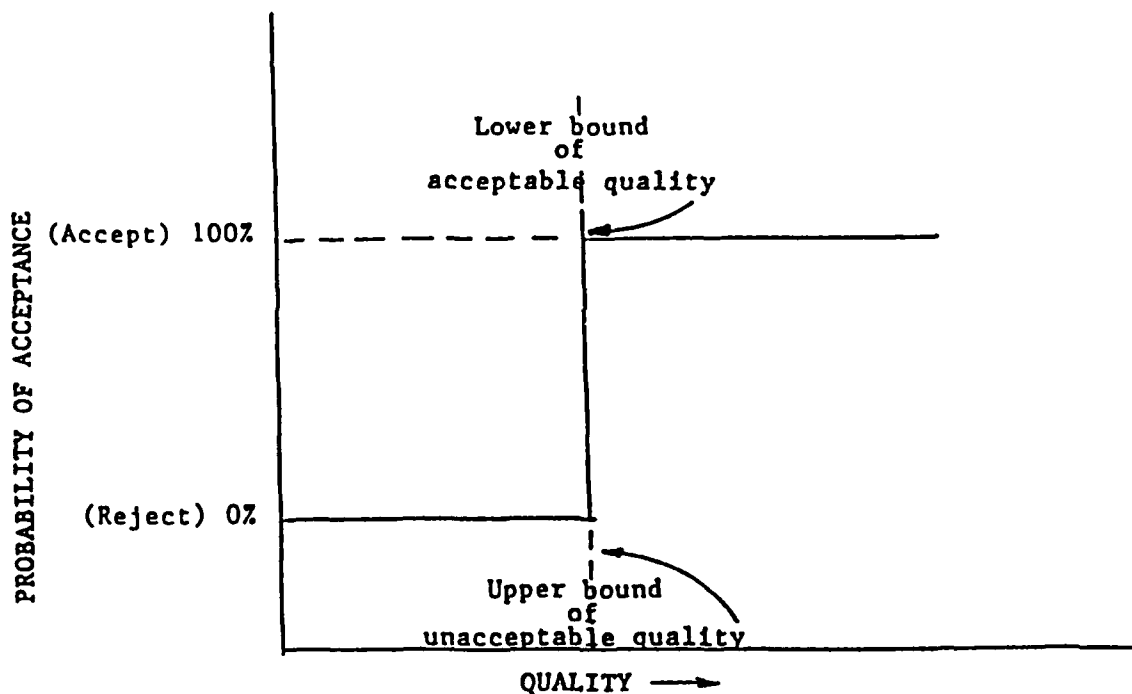


FIGURE 3.1. TYPICAL OPERATING CHARACTERISTIC CURVE

The first number is often called the Acceptable Quality Limit, (AQL). The AQL is the minimum acceptable quality and is assigned a $100(1 - \alpha)\%$ probability of being accepted. The probability of rejecting a lot with a quality level equal to the AQL is called the producer's risk, α , which is set to a relatively low value (often .05). The second number is termed the Unacceptable Quality Limit, (UQL), [other terms for this are the Rejection Quality Limit (RQL) or Lot Tolerance Percent Defective (LTPD)]. It has a probability of acceptance equal to β , called the consumer's risk. This represents a quality level that the organization (often referred to as the consumer) wants a low probability of accepting. A value of .10 is typical for β .

In standard Quality Control (QC) practice, each lot is accepted or rejected. This results in either 100% or 0% payment for the lot. The expected payment for lots produced at a consistent quality level is 100 times (Probability of Acceptance) given the quality level. If the lots were consistently produced at the AQL, the expected payment would be $100(1 - \alpha)\%$. Similarly for lots produced at the UQL, the expected payment is $100(\beta)\%$.

In most QC cases historical data provides both mean and variability estimates of the material to be produced, so that the AQL and UQL may be selected to meet the desired quality goals. For this study, the FAA desires an investigation into statistically based pay factors. This investigation selects a possible AQL and UQL pair to demonstrate the use of the proposed statistical procedure. In practice, the FAA must work closely with the producers to determine realistic values for these quality parameters.

The current FAA practice uses a pay adjustment factor to determine the actual payment to a contractor on a lot by lot basis. The statistical procedure proposed in this report is based on an estimate of quality, as described later in this report. This procedure also computes a pay adjustment factor on a lot by lot basis. In classical QC inspections, a lot would receive either 100% or 0% pay, as mentioned above. A lot by lot statistical procedure should result in roughly the same expected pay for a given lot quality, as the classical QC approach. Thus, a lot with a true quality level equal to the AQL should have an expected pay factor equal to $100(1 - \alpha)\%$, while a lot with a quality level equal to the UQL, should have an expected pay factor of $100(\beta)\%$.

In the following sections, a statistical acceptance plan and a payment adjustment schedule for each of five materials used in airport runway construction will be developed. Although the accomplished goals shown in this report are for only one of the five materials (P-501 Concrete, flexural strength), developments of an acceptance plan and a payment adjustment schedule, where appropriate, for other airport pavement materials are similar.

The integrated system of a statistical acceptance plan and a payment adjustment schedule must be practical and serve the purpose intended by the user: to encourage suitable quality production by rewarding producers of suitable quality material with full pay, and penalizing producers of unsuitable quality material with a payment adjustment or rejection.

4. TECHNICAL DISCUSSION

4.1 Approach

This chapter presents the details of the development of a statistical acceptance plan and an integrated payment adjustment schedule for P-501 Concrete. The development of an integrated payment adjustment schedule depends on the specific statistical acceptance plan chosen by the consumer, so the development of the acceptance plan is presented first in Section 4.2 and is followed by the development of the corresponding payment adjustment schedule in Section 4.3.

Section 4.2 begins with an outline of the basic steps of the general statistical acceptance plan and is followed by a discussion of the set of values that must be chosen by the consumer in order to specify a particular acceptance plan: AQL, UGL, α , and β . Next, definitions of unit and lot quality for P-501 Concrete are given. This is followed by a discussion of the method of obtaining the best estimate of lot quality. Formulas for calculating the estimates are given for various lot sample sizes.

Next is a discussion of an analysis of data and the rationale for choosing the values of AQL and UQL, followed by a discussion of the choices for α and β . This is followed by a presentation of the procedure for taking these values and calculating the lot sample size and acceptance value. This is the final step in specifying a particular statistical acceptance plan and the formulas are applied to the values for P-501 Concrete and the results are presented.

Before continuing to the payment adjustment schedule, the operating characteristic (OC) is introduced. The OC is derived from the specific statistical acceptance plan and is used in the development of the payment adjustment schedule.

Section 4.3 begins with a review of the statistical acceptance plan for P-501 Concrete, developed in the preceding section, and is followed by a discussion of the basic philosophy of an integrated payment adjustment schedule. Next, a discussion of the statistical acceptance plan and integrated payment adjustment schedule, used with the P-401 Asphalt, is presented. Then, the payment adjustment schedule for P-501 Concrete is presented and discussed. Finally, comments regarding application of the technology to the other materials of interest from this work are presented.

4.2 Statistical Acceptance Plan

Acceptance sampling is a statistical procedure used to achieve quality assurance [2,3]. For a given lot of material, the procedure consists of the following: (1) Draw a fixed number of samples from the lot, (2) Measure the quality of each sample, (3) Compute an estimate of lot quality from the sample measurements, and (4) Accept or reject the lot, depending on whether the estimate is above or below an acceptable value. The complete procedure consists of repeating the steps for each lot in a series of lots.

To specify a particular acceptance plan, four values are chosen: the acceptable quality limit (AQL), the unacceptable quality limit (UQL), the producer's risk (α), and the consumer's risk (β). These values are used to compute the acceptable value and the lot sample size. The calculations ensure that for lots produced at the AQL, there will be a small probability of rejection (α), and for lots produced at the UQL, there will be a small probability of acceptance (β). In this way, quality assurance is achieved. The consumer knows that in the long run, 100 (1- α)% of the lots of acceptable quality will be accepted and 100 (1- β)% of the lots of unacceptable quality will be rejected.

The measure of quality for a unit of P-501 Concrete is the 28-day flexural strength, measured in pounds per square inch (psi) [4]. The corresponding definition of quality for a lot of P-501 Concrete is the percentage of units in the lot that have a 28-day flexural strength greater than a fixed (but arbitrary) limit. Applying the normal distribution model, we assume that the unit flexural strength values in a lot are normally distributed with a particular mean and standard deviation. Under this model, the percentage above a given limit (PAL) is equal to $100 \Phi [(\mu-L)/\sigma]$ where Φ is the standard normal distribution function, μ is the lot mean, L is the limit, and σ is the lot standard deviation [See Appendix A].

For a given lot and limit, the PAL can be found by (1) finding the number of units with test values greater than the limit and dividing by the total number of units, and (2) finding the mean and standard deviation of all the unit test values and computing $100 \Phi [(\mu-L)/\sigma]$; both are impractical because they require all the units to be tested. An alternative is to estimate PAL and use the estimate as a proxy for the unknown PAL. The best (unbiased minimum variance) estimator of PAL is a function of the sample quality index and depends on the lot sample size [5]; the sample quality index is computed from the sample average and the sample standard deviation. The sample average, sample standard deviation, sample quality index, and best estimator formulas are, respectively,

$$\text{Average: } \bar{X} = \frac{1}{n} \sum_{i=1}^n X_i, \quad (4-1)$$

$$\text{Standard Deviation: } S = \frac{1}{(n-1)} \sum_{i=1}^n (X_i - \bar{X})^2, \quad (4-2)$$

$$\text{Quality Index: } Q = \frac{(\bar{X} - L)}{S}, \quad (4-3)$$

$$\text{Estimated PAL: } EPAL_n = 100 \left(1 - \int_0^A \text{beta}(X; n/2 - 1) dX \right), \quad (4-4)$$

$$= 100 \Phi(Q)$$

where,

n = lot sample size,

X_i = i th sample value,

$EPAL_n$ = estimator of PAL for lot sample size equal to n ,

A = $\max [0, 1/2 - 1/2 Q (n^{1/2}/n-1)]$,

$\text{beta} = (X; n/2 - 1)$ = beta density with $\alpha = \beta = n/2 - 1$.

Values of $EPAL_n$ have been tabulated for various Q and for n from three to 12, eliminating the burden of working with Equation (4-4) [5]. However, using a table of integrals and the binomial formula, Equation (4-4) has been reduced to a set of algebraic equations (procedure outlined in Appendix B) eliminating the need for the tables:

$$EPAL_3 = 100 \{ .5 + (1/\pi) \sin^{-1}(1-2A) \}, \quad (4-5)$$

$$EPAL_4 = 100 (1 - A), \quad (4-6)$$

$$EPAL_5 = 100 \{ (2/\pi) (1-2A) (A-A^2)^{1/2} \} + EPAL_3, \quad (4-7)$$

$$EPAL_6 = 100 (1 - 3A^2 + 2A^3), \quad (4-8)$$

$$EPAL_7 = 100 \{ (16/3\pi) (1-2A) (A-A^2)^{3/2} \} + EPAL_5, \quad (4-9)$$

$$EPAL_8 = 100 (1 - 10A^3 + 15A^4 - 6A^5), \quad (4-10)$$

$$EPAL_9 = 100 \{ (256/15\pi) (1-2A) (A-A^2)^{5/2} \} + EPAL_7, \quad (4-11)$$

$$EPAL_{10} = 100 \{ 1 - 35A^4 + 84A^5 - 70A^6 + 20A^7 \}, \quad (4-12)$$

$$EPAL_{11} = 100 \{ (2048/35\pi) (1-2A) (A-A^2)^{7/2} \} + EPAL_9, \quad (4-13)$$

$$EPAL_{12} = 100 \{ 1 - 126A^5 + 420A^6 - 540A^7 + 315A^8 + 70A^9 \}, \quad (4-14)$$

An important fact about estimating PAL is that as n increases, $100\Phi(Q)$ approaches $100\Phi[(\mu-L)/\sigma]$. This implies that for n large enough (perhaps greater than about 25), an approximate value for PAL can be calculated by finding $\Phi(Q)$ in a standard normal table. This is much simpler than using Equation (4-4).

The AQL and UQL that are used in the discussion that follows were computed from an analysis of the available historical data for P-501 Concrete. Simply put, the AQL is the minimum level of quality that the consumer desires to accept with high probability, $(1-\alpha)$, and the UQL is the maximum level of quality that the consumer desires to reject with a high probability $(1-\beta)$. Shown in Figure 4.1 is a histogram illustrating the quality index computed from 4 samples from each of 316 lots of P-501 Concrete. These data were taken from recent airport construction projects in the FAA Eastern Region.

The cumulative distribution of the quality index for these 316 lots is shown in Figure 4.2. The procedures used to generate the histogram and cumulative distribution and subsequently pick values for AQL and UQL are given in Chapter 4 for P-501 Concrete. The cumulative distribution is a relationship between the sample population and level of quality index achieved. The tabular listing of the cumulative distribution is presented in Table 4.1. As it turns out, roughly 50% of the values are above 1.2. Use Equation (4-6) to determine that roughly 50% of the lots have an estimated PAL of at least 90. That is,

$$EPAL_4 = 100 (1-A)$$

$$A = \max [0, 1/2 - 1/2Q(n^{1/2}/n-1)]$$

$$\text{for } Q = 1.2 \text{ and } n = 4$$

$$A = \max [0, .1] = .1$$

$$EPAL_4 = 100(1-A) = 100 (1-.1)$$

$$\text{or } EPAL_4 = 90$$

This value will serve as the AQL.

TABLE 4.1. CUMULATIVE DISTRIBUTION OF QUALITY INDEX (Q)
FOR P-501 CONCRETE

| Percentile | Q |
|------------|-------|
| 99 | 11.0 |
| 95 | 7.0 |
| 90 | 4.5 |
| 80 | 2.8 |
| 70 | 2.2 |
| 60 | 1.7 |
| 50 | 1.4 |
| 40 | 1.0 |
| 30 | 0.8 |
| 20 | 0.5 |
| 10 | 0.0 |
| 5 | - 0.5 |
| 1 | - 1.3 |

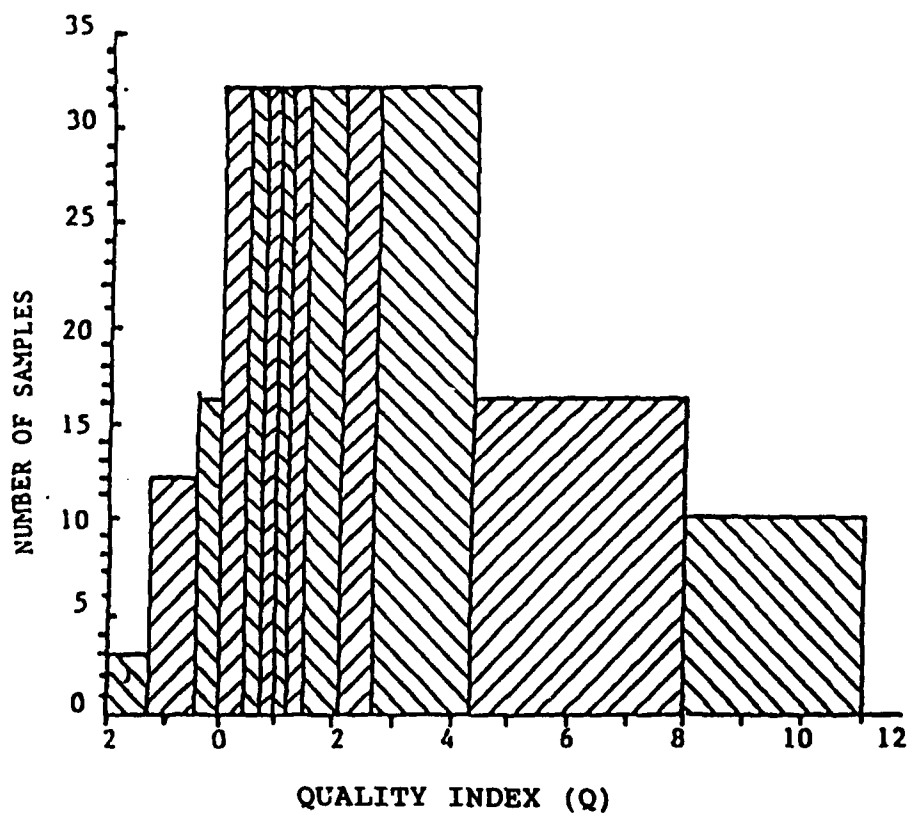


FIGURE 4.1 HISTOGRAM FOR QUALITY INDEX: P-501 CONCRETE

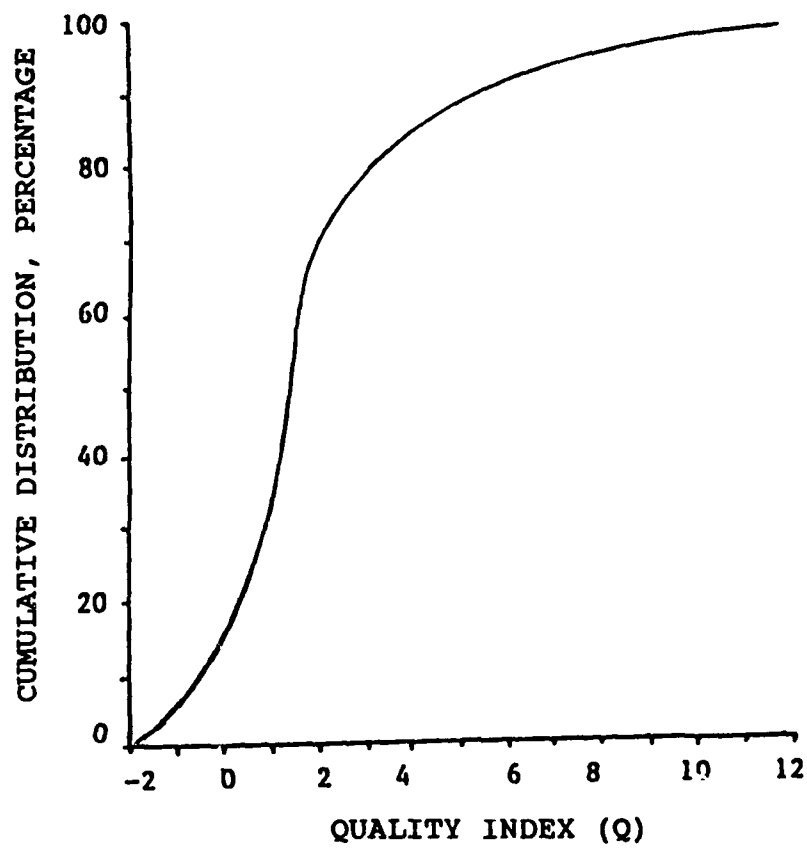


FIGURE 4.2 CUMULATIVE DISTRIBUTION FOR QUALITY INDEX
P-501 CONCRETE

The reason for choosing the 50th percentile of the distribution in Table 4.1 is that, assuming the quality control methods for concrete production are generally working and in statistical control, this value is a good estimate of the process mean. Note also that roughly 10% of the values are below a value of $Q = .15$. Using Equation (4-6), it can be seen that roughly 10% of the lots have an estimated PAL of at most 55. This value is suggested to serve as the UQL; with an AQL of 90 PAL, it is reasonable to expect production to be above 55 PAL.

The acceptance value, as used here, is a value against which the estimated PAL (EPAL) for each lot will be compared. If the EPAL for a lot is above the upper acceptance value, the lot is accepted; if the EPAL for a lot is below the lower acceptance value, the lot is rejected.

In order to compute the acceptance value and lot sample size, it remains to choose α and β . These values can be chosen somewhat arbitrarily, but should be relatively small. Practice has shown that values of $\alpha = .05$ and $\beta = .10$ work well and these values are used here. The acceptance value and lot sample size are calculated using the following procedure from [2]:

$$K = (Z_\alpha Z_2 + Z_\beta Z_1) / (Z_\alpha + Z_\beta), \quad (4-15)$$

$$n = (1 + K^2/2) [(Z_\alpha + Z_\beta) / (Z_1 - Z_2)]^2, \quad (4-16)$$

where,

K = parameter used in calculation of acceptance value,

Z_α = $1-\alpha$ point of the standard normal distribution,

Z_β = $1-\beta$ point of the standard normal distribution,

Z_1 = AQL/100,

Z_2 = UQL/100,

n = lot sample size.

For the case of P-501 Concrete and the results from the foregoing discussion we have:

$\alpha = .05$, $\beta = 0.10$, AQL = 90, and UQL = 55.

As such, from the definitions presented above

$Z_\alpha = 1-\alpha = .95$

$Z_\beta = 1-\beta = .90$

$Z_1 = .90$

$Z_2 = .55$,

and from a normal distribution table

$$Z_{\alpha} = N(.95) = 1.645$$

$$Z_{\beta} = N(.90) = 1.282$$

$$Z_1 = N(.90) = 1.282$$

$$Z_2 = N(.55) = .1256$$

whereupon, from Equation (4-15)

$$K = \frac{(1.645 \cdot .1256 + 1.282 \cdot 1.282)}{(1.645 + 1.282)} = 0.6321$$

We use Equation (16) to determine the sample size.

$$n = (1 + (.6321)^2/2) ((1.645 + 1.282)/(1.282 - .1256))^2 = 7.7 \text{ or } 8.$$

Although the values used for the parameters yield a value of sample size $n = 8$ from Equation (4-16), the values of Q , calculated from the actual construction project data, used sample size $n = 4$. The implications of this will be discussed later. As it turns out, K is the specific value for the quality index (Q) from all possible values for Q from the sample lots and is used in calculating the expected PAL. For the acceptance value so calculated we can calculate the EPAL using, for this case, Equation (4-10).

$$EPAL_0 = 100(1 - 10A^3 + 15A^4 - 6A^5)$$

$$A = \max [0, 1/2 - 1/2Q(n^{1/2}/(n-1))]$$

and here $K=Q=.6321$ which gives for $n=8$

$$A = .3723. \text{ Then}$$

$$EPAL_0 = 100(1 - 10 \cdot .3723^3 + 15 \cdot .3723^4 - 6 \cdot .3723^5)$$

$$EPAL_0 = 72.92 \text{ or } 73\%$$

Therefore, with an acceptance value of .6321, which implies an $EPAL_0$ of 73%, the consumer can expect to accept lots of 90 PAL about 95% of the time, and the consumer can expect to reject lots of 55 PAL about 90% of the time. The values of $AQL = 90$ PAL and $UQL = 55$ PAL are not what the FAA is currently using. These are suggested values for consideration for an increase in product quality.

The operating characteristic (OC), corresponding to a particular level of PAL, is defined as the probability that a lot of the given PAL will be rejected [3]. Consider the suggested acceptance plan for P-501 Concrete. The OC for a lot that is 90 PAL is .05, (α), and the OC for a lot that is 55 is .90, ($1-\beta$). In other words, for lots of 90 PAL, EPAL, will be less than 73% approximately 5% of the time, just by chance. Likewise, for lots of 55 PAL, EPAL, will be less than 73% approximately 90% of the time, just by chance. The OC corresponding to other levels of PAL have been calculated and are presented in Table 4.2 and are shown graphically in Figure 4.3. (The procedure is explained in Appendix C).

This information is used in computing the expected payments discussed in the following section. It should be noted that a 90 PAL results in a rejection probability of .044, which is very close to the $\alpha = .05$ that was specified in the sampling plan. Similarly, a 55 PAL has a rejection probability of .892, which is close to $(1-\beta) = .90$ specified in the sampling plan. This implies that the acceptance sampling plan, even though the actual sample size is 4, is meeting the desired goals. Thus, the theoretical (calculated) value of sample size from Equation (4-16) may be somewhat conservative.

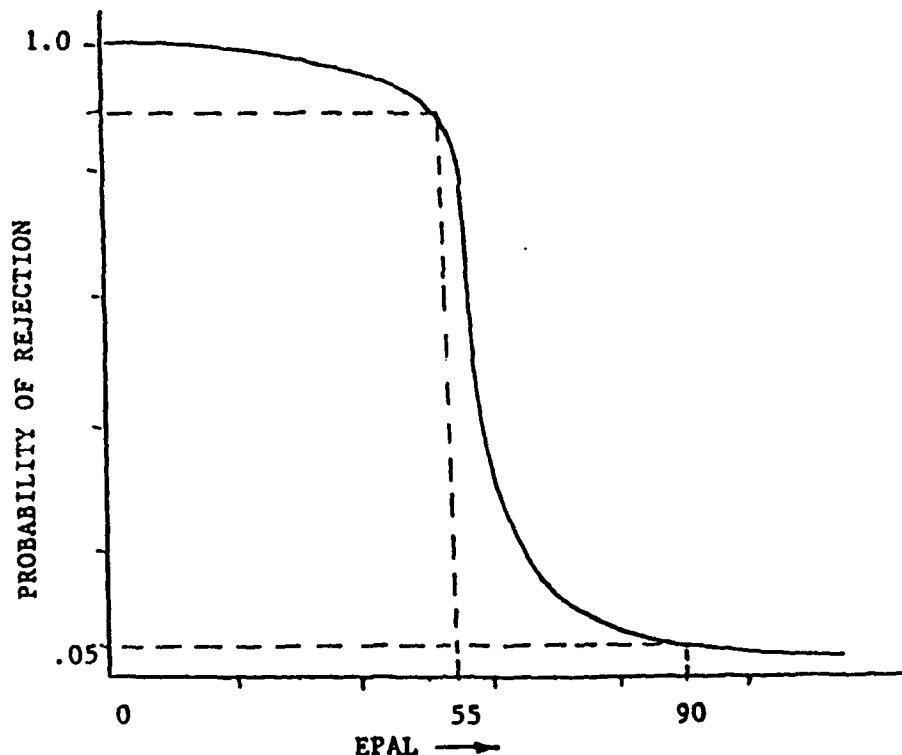


FIGURE 4.3. OPERATING CHARACTERISTIC (OC) CURVE FOR P-501 CONCRETE

TABLE 4.2. OPERATING CHARACTERISTIC (OC) FOR P-501 CONCRETE FOR VARIOUS LEVELS OF PAL

| PAL | OC |
|-----|------|
| 95 | .004 |
| 90 | .044 |
| 85 | .140 |
| 80 | .278 |
| 75 | .437 |
| 70 | .589 |
| 65 | .718 |
| 60 | .820 |
| 55 | .892 |

4.3 Payment Adjustment Schedule

The statistical acceptance plan for P-501 Concrete was developed in the previous section. It was determined that the acceptance plan is to consist of executing the following for each lot in a series of lots: (1) Draw (theoretically) 8 samples, (2) Measure the 28-day flexural strength of each sample, (3) Compute an estimate of lot quality (EPAL₀), and (4) Accept or reject the lot, depending on whether the estimate is above or below the acceptance value of $Q = .6321$. This results in the consumer being assured that on average, 5% of the lots that are at least 90 PAL will be rejected, and that on average, 90% of the lots that are at most 55 PAL will be rejected. This section presents the development of integrated payment schedules for P-401 Asphalt Concrete and P-501 Concrete.

In many situations, the reject decision, as the last step of the statistical acceptance plan, is inappropriate. For example, lots of concrete of less than ideal quality might still have value to the consumer. Furthermore, lots of concrete cost very much to produce and even more to replace. Both considerations imply that the reject decision may not be appropriate or practical. In such cases, it is desirable to have an alternative. A payment adjustment schedule provides an alternative, by introducing a price adjustment system, in lieu of complete rejection.

According to the philosophy of a payment adjustment schedule, for a lot with quality above some upper critical value, the decision is to accept, as before; but for a lot of quality below the upper critical value, the decision is to accept at a reduced price, rather than reject (of course, a lot with quality below some lower critical value is rejected). This allows the consumer to penalize the producer for a lot of less than ideal quality, without having to completely reject the lot. Again, this is particularly important when lots of less than ideal quality have some salvage value and are expensive to replace.

A reasonable payment adjustment schedule is one where the upper critical value is set at the AQL, the lower critical value is set at the UQL, and payment adjustment is based directly on the estimate of lot quality, with lower estimates receiving more severe payment adjustments than those of higher estimates for quality [6].

4.3.1 P-401 Asphalt Concrete, Density

As an example of a payment adjustment plan of the type mentioned above, the statistical acceptance plan and integrated payment adjustment schedule for P-401 Asphalt will be considered. This plan, and corresponding schedule, consists of executing the following for each lot in a series of lots: (1) Draw 4 samples, (2) Measure the density of each sample, (3) Estimate the lot quality using EPAL₄, and (4) Make the payment adjustment according to a schedule such as that shown in Table 4.3 [6]. The AQL is assumed to be 90 PAL.[6]

The probability of receiving each of the payment adjustment factors in Table 4.3 (or, equivalently, the probability the estimate will fall into each of the intervals in Table 4.3), given a particular level of PAL, is presented in Table 4.4 [5] for various values of PAL. These probabilities are used to compute the expected payments.

TABLE 4.3. PAY ADJUSTMENT FACTOR FOR P-401 ASPHALT CONCRETE

| Interval for Q for Estimate | Payment Adjustment Factor |
|--------------------------------|------------------------------|
| 90-100 | 1.00 |
| 85-89 | .98 |
| 80-84 | .95 |
| 75-79 | .90 |
| 70-74 | .80 |
| 65-69 | .70 |
| 0-65 | 0 or .50 |

TABLE 4.4. PROBABILITY OF PAY FACTORS FOR P-401 ASPHALT CONCRETE

| | Probability of Receiving Given Payment Adjustment Factor | | | | | | | |
|-----|---|------|------|------|------|------|------|------|
| PAL | 1.00 | .98 | .95 | .90 | .80 | .70 | .50 | 0 |
| 50 | .048 | .015 | .022 | .031 | .043 | .059 | .587 | .195 |
| 60 | .103 | .030 | .040 | .053 | .069 | .086 | .464 | .155 |
| 70 | .200 | .050 | .063 | .078 | .092 | .101 | .313 | .103 |
| 80 | .358 | .072 | .084 | .092 | .095 | .089 | .189 | .021 |
| 90 | .611 | .081 | .081 | .073 | .060 | .043 | .051 | 0 |
| 98 | .914 | .037 | .025 | .014 | .007 | .003 | 0 | 0 |

The expected payment corresponding to a particular PAL is defined as the average fraction of full pay a producer receives for a series of lots produced at the given PAL [6]. For each level of PAL, the expected payment is calculated by multiplying each payment adjustment factor by the corresponding probability and summing the results. For example, for a series of lots with PAL of 80, the expected payment is $(1.00) (.358) + (.98) (.072) + (.95) (.084) + (.90) (.092) + (.80) (.095) + (.70) (.089) + (.50) (.189) + (0) (.021) = .824$. Expected payments corresponding to this and other levels of PAL are presented in Table 4.5 [2] for P-401 Asphalt Concrete.

TABLE 4.5. EXPECTED PAY FACTORS FOR P-401 ASPHALT CONCRETE

| Lot Quality (PAL) | Expected Payment |
|----------------------|---------------------|
| 98 | .992 |
| 90 | .937 |
| 80 | .824 |
| 70 | .680 |
| 60 | .566 |
| 50 | .481 |

Note that the expected payment corresponding to the AQL (90) is equal to .937. This is very close to the $100(1-\alpha)\% = 95\%$ that would be theoretically correct. As the PAL falls away from the AQL, the expected payment drops: there is approximately an 18% expected payment decrease for PAL of 80, approximately a 32% expected payment decrease for PAL of 70, and approximately a 43% expected payment decrease for PAL of 60.

4.3.2 P-501, Portland Cement Concrete Pavement, Flexural Strength

A method for creating a pay adjustment factor for P-501 Concrete is presented in the following. The method for establishing an acceptance plan for P-501 Concrete was given in a previous section and the need for a payment plan that provides for the capability to accommodate for pay factors between zero (no pay) and one (full pay) was stated. What remains then is to follow the same path for the acceptance plan for P-501 Concrete, as outlined previously, and state the rationale for choice of relationship between estimate of quality (EPAL) and corresponding pay factor between values of zero and full payment.

As also noted previously, the choice of values for AQL and UQL were made from historical data for P-501 Concrete. This historical data included data from airport construction projects that provided information from over 500 lots of concrete as the source for an estimation of quality for each lot of concrete. As it turned out, some of the information received from the airport construction projects was not admissible as data for quality estimation. Some of this data was from seven and fourteen day cure time specimens. Only data from lots of concrete that satisfied the 28-day cure time and 4 samples from each lot were considered.

Also, data were eliminated from consideration if those data yielded strength values for concrete that were unreasonably different from that considered typical for P-501 Concrete. Consideration of these factors resulted in data from around 316 lots as admissible input to calculate parameters to estimate individual lot quality. These data are the basis for the information shown in Figures 4.1 and 4.2. Again, these data are used to illustrate the procedure that is used to take data from the project file and create the necessary input to generate histograms, cumulative distribution, and suggest values for AQL and UQL.

From these data, the AQL was set at 90 PAL and the UQL value was set at 55. These choices for AQL and UQL are suggested for the sake of improved quality. Use of values for AQL and UQL, currently employed by the FAA to estimate pay factors, will be illustrated in the following discussion. The values for α and β were set at .05 and .10, respectively. The pay factor adjustment to be shown herein was based on four samples from each lot of P-501 Concrete and, strictly speaking, that is inconsistent with the sample size calculated from Equation (4-16). However, it will be shown that use of four samples from each lot to estimate lot quality provides for pay factors that are consistent with the choices for AQL, UQL, α , and β .

There is no universally specified or accepted way to bridge the gap between pay factors of one (full pay) and zero (no pay). Currently, the pay factor for P-501 Concrete is made according to a discrete relationship between pay and two parameters from the

flexural tests performed on field specimens from each lot of concrete (See Advisory Circular No. 150/5370-10). The two test parameters are M, modulus of rupture (specified 28-day flexural strength) and R, range of a sample of size $n = 4$, which is the difference between the largest and smallest test values. We can convert the parameters M and R into equivalent EPAL and state the current pay factor for P-501 Concrete according to:

| <u>Pay Factor</u> | <u>Estimated PAL</u> <u>(Based on 28 day Strength, 4 Samples)</u> |
|-------------------|--|
| 1.00 | $60 \leq \text{EPAL}$ |
| .95 | $50 \leq \text{EPAL} \leq 59$ |
| .85 | $43 \leq \text{EPAL} \leq 49$ |
| .75 | $37 \leq \text{EPAL} \leq 42$ |
| .50 | $\text{EPAL} \leq 36$ |

This discrete relationship between EPAL and Pay Factor for P-501 Concrete, currently in use by the FAA, is graphically shown in Figure 4.4. The discrete nature of this relationship presents the obvious dilemma, equal pay factor for less quality product. That is, if the value for EPAL is, say, 49 for a given lot of concrete and the value for EPAL for another lot of concrete is 44, then the pay factor is, from Figure 4.4, the same for both lots, namely 85% of full pay.

It is desirable to have a unique value of pay factor for each value of EPAL between pay factors of one and zero. Thus, a continuous relationship between pay factor and EPAL should be established for values of pay factor between one and zero. As mentioned in the beginning of Section 4.3, the shape of the functional relationship between pay factor and EPAL should be such that higher pay factors should be associated with higher quality and lower pay factors associated with lower quality. As such, the slope of the curve (functional relationship between pay factor and EPAL) should be mild, or less steep, as pay factor is reduced from one. Further, reduction in a value of EPAL should be reflected in a steeper slope in the curve that represents the functional relationship between pay factor and EPAL. These are the basic thoughts that went into the establishment of the pay factor for P-501 Concrete from this work.

A brief discussion follows that illustrates how the functional relationship between pay factor and EPAL for values of pay between one and zero can be established. It was also mentioned before that the values for AQL and UQL should be and were derived from historical data. In the case of P-501 Concrete this amounted to examination of data from 316 lots of concrete from past and ongoing airport construction projects. If the relationship between pay factor and EPAL is thought of as analogous to a plot of x vs. y , two points in x, y space can be defined immediately; namely, pay

factor equal to one and EPAL equal to AQL - call this point (x_1, y_1) and pay factor equal to zero (or some agreed on minimum payment) and EPAL equal to UQL - call this point (x_2, y_2) . This is illustrated in Figure 4.5.

PAYMENT ADJUSTMENT SCHEDULE
CURRENT P-501

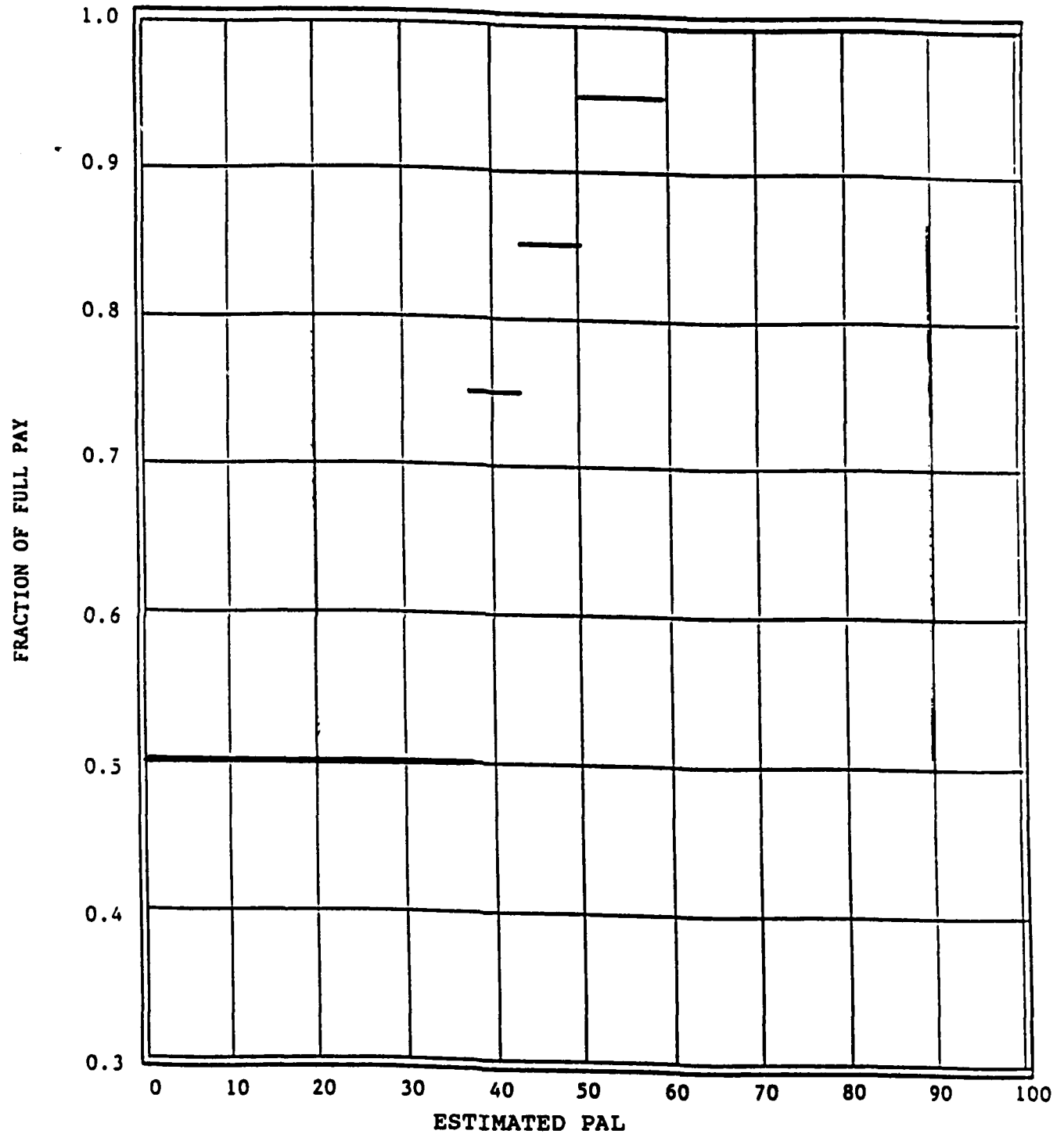


FIGURE 4.4 PAY FACTOR FOR P-501 CONCRETE CURRENTLY IN USE BY FAA

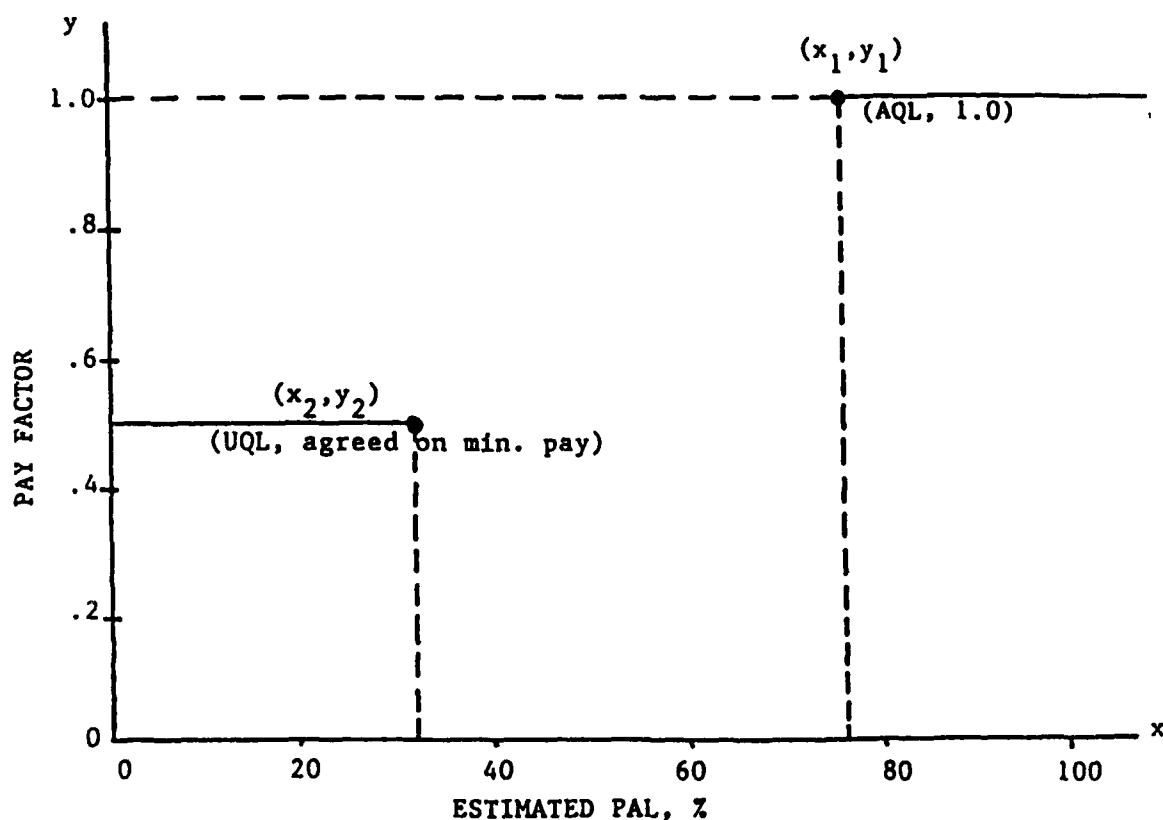


FIGURE 4.5. DEFINITION OF AQL, UQL, AND PAY FACTOR IN TERMS OF x AND y

The task is to bridge the gap between the two points (x_1, y_1) and (x_2, y_2) . A quadratic function (second degree in power of x) was selected such that the slope of the curve is gradual, when moving away from point (x_1, y_1) to the left. The slope of the function is quite steep, as the curve joins point (x_2, y_2) from the right. The equations that describe this type of behavior follow and Figure 4.6 is helpful in explaining the parameters involved.

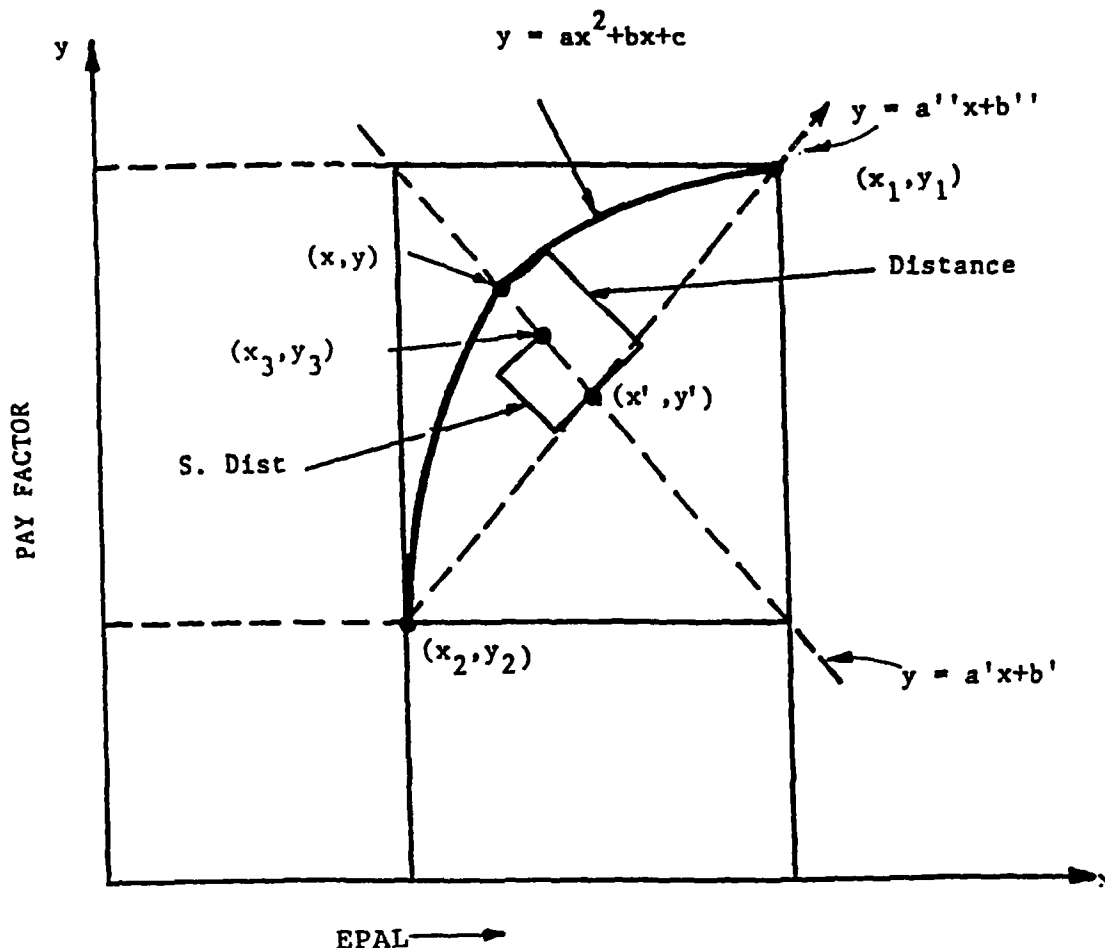


FIGURE 4.6. PAY FACTOR VS. EPAL BETWEEN VALUES OF AQL AND UQL

A few words concerning the parameters involved in generating the function between points (x_2, y_2) and (x_1, y_1) are worthwhile. The straight line joining (x_2, y_2) and (x_1, y_1) in Figure 4.7 can be thought of as a limiting curve (clearly the simplest) to bridge the gap. In fact, any function or curve to the right of this line would punish the producer of higher quality work more than the producer of lower quality work. Consistent with this is the distance from the point (x, y_2) on the straight line to the general quadratic form, $y = ax^2 + bx + c$, at (x, y) . The distance in this direction is considered positive.

The S-Dist is a fraction of the distance from the straight line and the general quadrature function. The end points of the S-Dist are (x, y) and (x_3, y_3) . Thus, the limiting curves (for nonnegative values of distance) are the straight line and the general function $y = ax^2 + bx + c$. When S-Dist = 0, the curve is the straight line and when S-Dist = Distance, the curve is the general quadratic. The following formulas have been used to define the parameters used in the quadratic function between points (x_1, y_1) and (x_2, y_2) .

$$a = \frac{Y_2 - Y_1}{x_2^2 - 2x_2x_1 + x_1^2} ; b = -2x_1a ; c = x_1^2a + y_1$$

$$a' = \frac{Y_1 - Y_2}{x_2 - x_1} ; b' = -x_1a' + y_2$$

$$a'' = \frac{Y_1 - Y_2}{x_1 - x_2} ; b'' = -x_2a'' + Y_2$$

$$x = (a' - b) + [(b-a')^2 - 4a(c-b')]^{1/2} ; y = a'x + b'$$

$$x' = \left(\frac{b'' - b'}{a' - a''} \right) ; y' = a''x + b''$$

$$\text{Distance} = [(x' - x)^2 + (y' - y)^2]^{1/2}$$

$$x_3 = x' - (S\text{-Dist}) \cos[\tan^{-1}(y_3 - y_2)/(x_3 - x_2)]$$

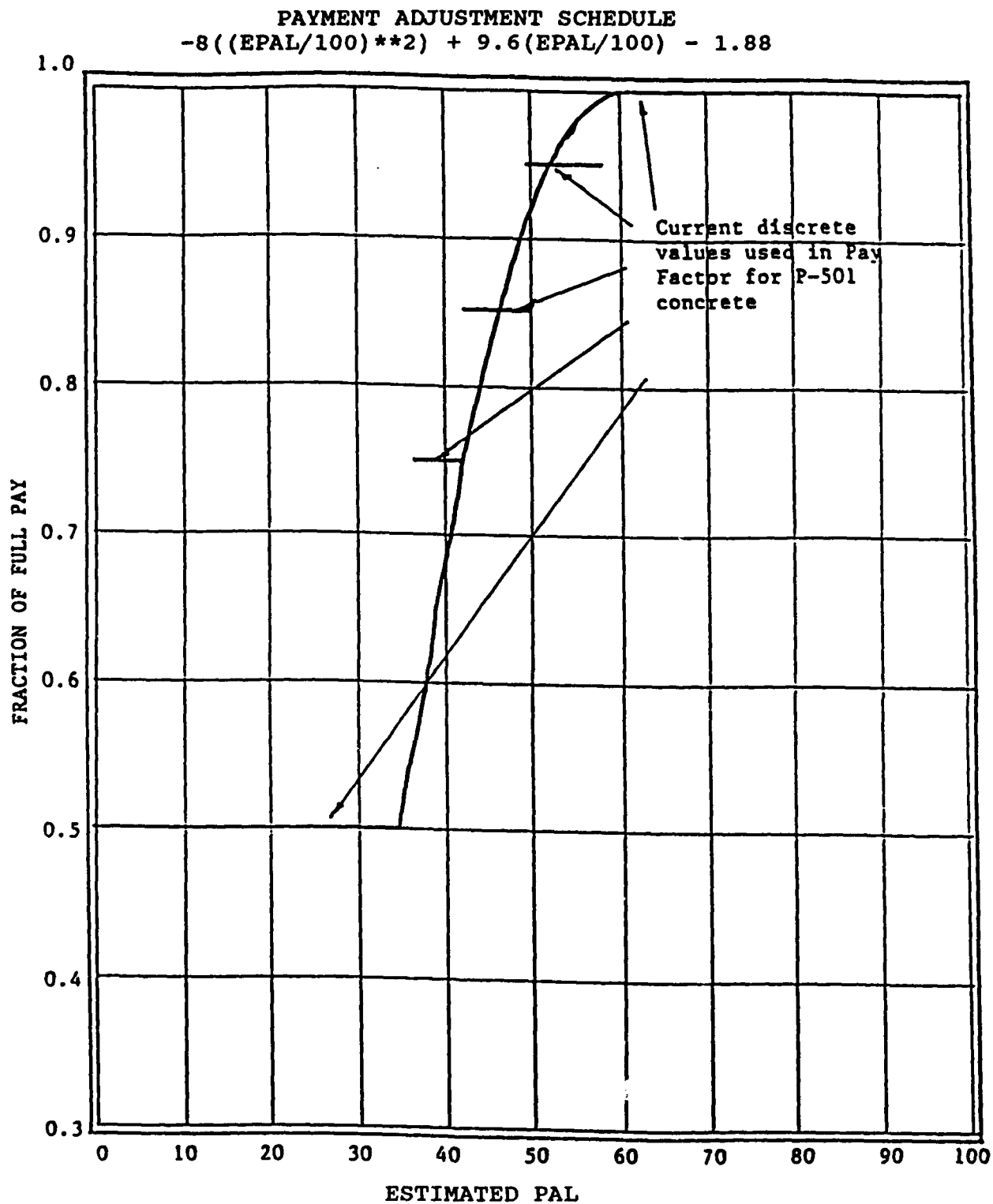
$$y_3 = a'x_3 + b'$$

The advantage of this technique is that it is flexible enough to handle most conditions that can be practically implemented as far as pay factors are concerned. AQL and maximum pay factor equal to one are the coordinates for (x_1, y_1) and UQL and minimum pay factor are the coordinates for (x_2, y_2) . Calculations of distance dictates how severe producers of poorer quality will be penalized for quality between AQL and UQL.

This method was applied to the current P-501 Concrete pay factor where AQL = 59% and UQL = 37%. The graphical results are shown in Figure 4.7. Also superposed in Figure 4.7 are the discrete values of pay factor according to what is currently in use. The distance parameter in Figure 4.7 was chosen so as to obtain close to average values for pay factor between the various discrete range values.

If we now consider the values of AQL = 90 PAL and UQL = 60 PAL that is close to the values previously generated from the historical data base for P-501 Concrete and choose a value for S-Dist = 0.6, the following quadratic function is generated.

$$\text{Pay Factor} = -3.212 * EPAL^2 + 6.4347 * EPAL - 2.235$$



**FIGURE 4.7 APPLICATION OF METHODOLOGY TO CURRENTLY USED
VALUES OF AQL AND UQL FOR P-501 CONCRETE**

This pay factor, as a function of EPAL, is shown in Figure 4.8. Therein, we have arbitrarily set pay factor = 0 if EPAL < 60%. But again, the flexibility in the method should be noted, since a broad range of values can be selected for AQL, UQL, S-Dist, and minimum pay, depending on how severe the punishment for poor quality should be.

The foregoing has shown that a payment adjustment schedule can be successfully integrated with a statistical acceptance plan by first following the well-known procedure for developing a statistical acceptance plan. The plan can be used as a basis for the payment adjustment schedule, that assigns a payment adjustment to an individual lot.

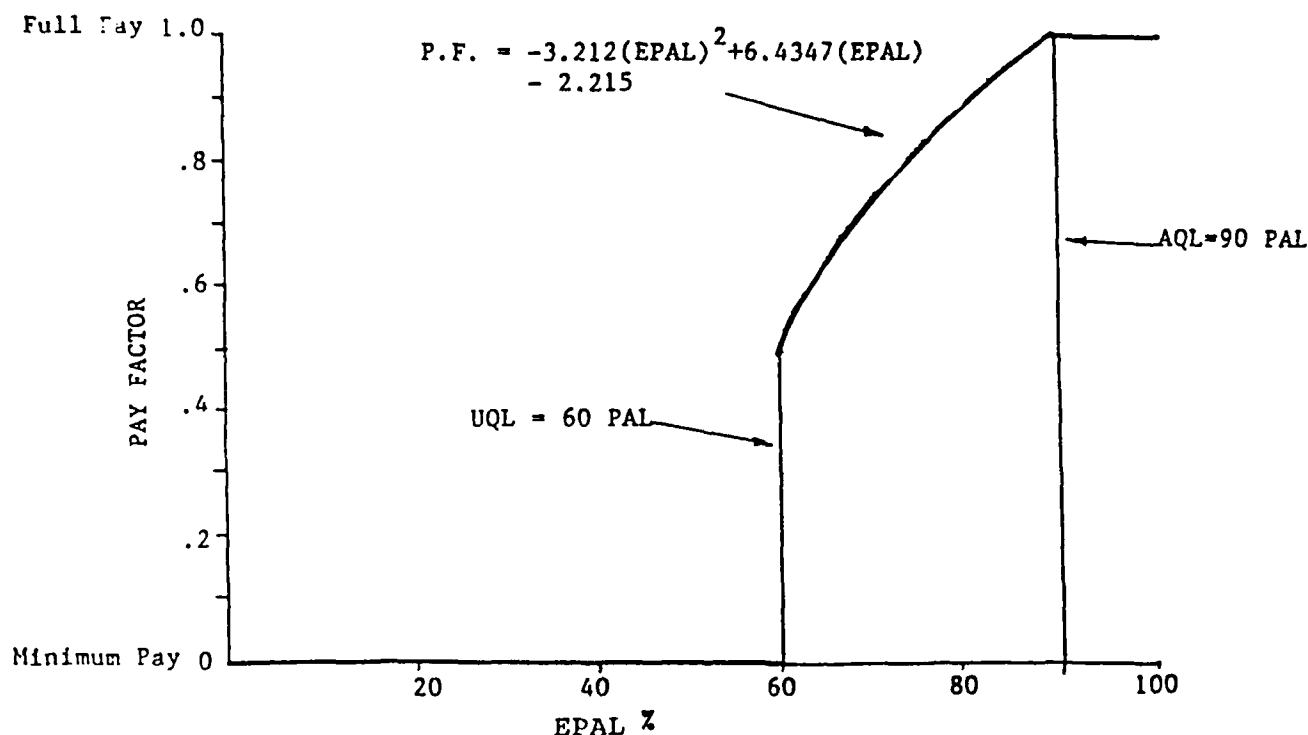


FIGURE 4.8. APPLICATION OF METHODOLOGY FOR P-501 CONCRETE USING VALUES OF AQL AND UQL DERIVED FROM HISTORICAL DATA

In the following subsections the applicability of the methodology to the other material specifications P-152, Excavation and Embankment, Density; P-209, Crushed Aggregate Base Course, Density; P-304, Cement Treated Base Course, Density; P-306, Econocrete Subbase Course, Density; and P-501, Portland Cement Concrete Pavement, Thickness will be discussed.

4.3.3 P-152, Excavation and Embankment, Density

During data collection interviews involving contractor personnel and FAA field personnel, airport personnel and consulting engineers, it was apparent that most engineering monitors preferred a construction contractor to continue to rework and reroll this material until a "pass" was obtained from the "pass/fail" tests, rather than offer a payment adjustment for the section for which the tests failed.

This situation was consistent with that discovered by the FAA in interviews with pavement industry personnel and field engineers. As such, it was mutually agreed that further development of a statistically based pay adjustment plan be suspended, because changing from the current method of testing will be resisted by those required to use it.

4.3.4 P-209, Crushed Aggregate Base Course, Density

It was mutually agreed that no further effort be made to develop a pay adjustment plan for this item for the same reasons stated in Subsection 4.3.3.

4.3.5 P-304, Concrete Treated Base Course, Density

Sufficient pavement material test data were not available in the FAA Eastern Region for this item to develop a statistically based pay adjustment schedule. A significant amount of effort was spent by the contractor in the attempt to locate this data.

It was mutually agreed that since there is no guarantee that meaningful data would result from any other FAA region for this item, no further attempt would be made to acquire data for P-304. For this reason, and the reasons explained in Subsection 4.3.3, there would be no requirement to develop a pay adjustment factor for P-304, Concrete Treated Base Course, density.

4.3.6 P-306, Econocrete Subbase Course, Density

For the exact reasons stated in Subsection 4.3.5, it was agreed not to develop a pay adjustment for the density specification for P-306 Econocrete. However, the current FAA specification for P-306 Econocrete involves a pay adjustment for the item based on thickness, with limitations placed on slump, air content and compressive strength. It was agreed that since compressive strength for P-306 Econocrete is monitored in almost the same manner as that for P-501 Concrete flexural strength, a pay factor for P-306 Econocrete, based on compressive strength, could be accomplished with the data on hand. This effort was undertaken and

the results are included in a later chapter.

4.3.7 P-501, Portland Cement Concrete Pavement, Thickness

Sufficient pavement material test data were not available in the FAA Eastern Region to be able to develop a pay adjustment schedule for this item. This is because, as was discovered during the data collection attempt, most engineers monitoring this item approve thickness by measuring concrete form depth instead of requiring destructive thickness core tests.

It was mutually agreed that because there was not a guarantee for any improvement in the collection of core test data for this item from any other FAA region, no additional effort should be put forth to collect such data and as such, no pay adjustment factor for P-501, Portland Cement Concrete Pavement, thickness would be required.

5. USE OF PROJECT DATA TO GENERATE AQL AND UQL FOR P-501 CONCRETE

5.1 Need for AQL and UQL for P-501 Concrete

In the discussions contained in Chapters 3 and 4, Acceptable Quality Limit (AQL) and Unacceptable Quality Limit (UQL) were defined and hints were given as to the choice of values for these two parameters; these are key ingredients in the establishment of integrated acceptance and pay adjustment plans. Recall in Chapter 3, the histogram for Quality from P-501 Concrete flexural strength test values from past airport construction projects was presented in Figure 4.1. Also, the corresponding cumulative distribution of Quality for those projects was presented in Figure 4.2. In the discussion that involved Figures 4.1 and 4.2, values for choices of AQL and UQL were stated.

The intent of the material presented in this chapter is to justify and explain how the choice for those values is made. The explanation that follows will present the procedure that can be used to gain insight into the choice of values for AQL and UQL and as such the initial values for AQL and UQL so derived may be just that, initial values. Final values may include an iterative process wherein the pay factors are generated using the initial values of AQL and UQL and the resulting curve that bridges the gap from AQL to UQL.

These pay factors can then be compared with what appears reasonable, as far as pay penalty applied to the contractor is concerned. That is, does the initial choice of AQL and UQL result in pay factors that are too harsh or too lenient? If so, then a second choice for values of AQL and UQL can be made and the procedure repeated until the resulting pay factors are consistent with what the agency feels represents the required level of quality needed at the project site and at the same time is an attainable level that can be achieved by the contractor for an acceptable cost.

To aid in this procedure, simple computer programs have been written and the use of these programs will be detailed in the material which follows. Specifically, there are two such computer programs. One creates a data base, and the second uses this data base together with a statistical analysis package, SAS, which generates the information upon which the decision for initial choice of AQL and UQL is made.

5.2 Computer Programs to Combine Field Test Values into Data Base

The first activity that must be performed after data have been received from various construction projects is to create a data

base which contains test values for the attributes that are estimated to measure quality for the construction material of interest.

In this effort, the material was P-501 Concrete and the attribute was flexural strength. The program outlined in this sub-section allows data to be added to an existing data base or generate entirely new data by replacing the old data with the new data. The program is written in dBASE III. During this effort, the data would only be admissible to the data base if the test results were from 28-day cured test specimens.

5.2.1 Program Description 'JOIN'

This dBASE III program is called 'JOIN' and must be executed to combine all the data base files (construction project information) together and generate an ASCII file which will be used by the SAS program. The 'JOIN' program requires all data base files to include four common fields, otherwise the program will not execute. These fields are:

1. AGE: Age of the sample (program will elect records with AGE=28).
2. TEST DATE: Date when test was performed.
3. STR: Strength of the tested sample.
4. LOT NO: Lot identification number.

To run the program at the DOS prompt type:
(Do not type the ' ' around JOIN)

'JOIN' and press <enter>

1. If the (existing) combined data base contains data from a previous execution, the user is asked:

'JOIN.DBF file already contains some data'
'Please enter <D> or <A> ? (D/A) ---->'

Responding: 'D' will delete all the data in the combined file
Responding: 'A' will add new data to the file keeping the old data.

2. The user will then be asked the following question:

'ENTER THE FILE NAME (? TO STOP) ----->'

Entering: '?' will go to step 3
 Entering: 'any' file name', disk is searched for the specified file name.
 If found: test date, strength and lot number are copied from the specified file name to the combined file.
 not found: user is prompted:

'FILE NAME DOES NOT EXIST, PLEASE RE-ENTER...'

3. The user will be asked the following question:

'Do you wish to create an ASCII File? (Y/N) -->'

Responding: 'Y' will create an ASCII file called 'JOIN.TXT' which will be used by the SAS program; process is then terminated.

Responding: 'N' will not create an ASCII file, process is then terminated.

'JOIN' PROGRAM LISTING

*Program name: Join

*Description: This program combines several data files together

```
CLEAR
SET TALK OFF
STORE .T. TO CONT
SELE 1
USE JOIN
*-----*
* FOLLOWING LOOP WILL CHECK PRIOR TO EXECUTION OF THE PROGRAM *
* IF ANY DATA ALREADY EXISTS IN THE JOIN.DBF FILE. IF ANY *
* FOUND THE USER IS ASKED WHETHER THEY WISH TO DELETE THE *
* ALREADY EXISTING DATA IN THE FILE OR APPEND TO IT. *
*-----*
IF .NOT. EOF()
DO WHILE CONT
STORE ' ' TO ANS
@ 1,1 SAY 'JOIN.DBF file already contains some data ....'
@ 3,1 SAY 'Please enter <D>elete or <A>ppend ? (D/A)---->'
@ 3,49 GET ANS
READ
IF UPPER(ANS)='D' .OR. UPPER (ANS)='A'
STORE .F. TO CONT
LOOP
ENDIF
ENDDO
IF UPPER(ANS) = 'D'
ZAP
ENDIF
ENDIF
```

```

*****
* FOLLOWING LOOP WILL ASK THE USER FOR THE FILE NAME TO BE *
* INCLUDED IN THE JOIN.DBF FILE. IF FOUND THE FOLLOWING THREE*
* FIELDS ARE COPIED TO THE JOIN.DBF: *
* *
* AGE: AGE OF THE SAMPLE (THIS PROGRAM SEARCHES FOR THE *
* 28 DAY TESTS. *
* TEST DATE: TEST DATE, WHEN THE TEST WAS PERFORMED *
* STR: STRENGTH OF THE MATERIAL *
* LOTNO: LOT NUMBER THE TEST WAS DONE *
* *
* NOTE: .....ALL FILES MUST HAVE AT THE MINIMUM ALL THE *
* ABOVE MENTIONED DATA ELEMENTS *
*-----*
CLEAR
STORE .T. TO CONT
DO WHILE CONT
    STORE ' ' TO NAME
    @ 1,1 SAY 'ENTER THE FILE NAME (? TO STOP) ----->'
    @ 1,40 GET NAME
    READ
    IF NAME='?'
        STORE .F. TO CONT
        LOOP
    ENDIF
    STORE NAME+'.DBF' TO FNAME
    IF .NOT. FILE (FNAME) THEN
        @ 20,1 SAY 'FILE NAME DOES NOT EXIST, PLEASE RE-
ENTER.....'
        WAIT
        CLEAR
        LOOP
    ENDIF
    SELE 2
    USE & NAME
    LOCATE FOR AGE = 28
    DO WHILE .NOT. EOF()
        SELE 1

```

```

APPEND BLANK
REPLACE TESTDATE WITH B->TESTDATE
REPLACE STR WITH B-?STR
REPLACE LOTNO WITH UPPER(LOTNO)
SELE 2
CONTINUE
ENDDO
ENDDO
CLOSE ALL
*-----*
* FOLLOWING LOOP WILL ASK THE USER IF HE WISHES TO CREATE AN *
* ASCII FILE FROM THE COMBINED DATA SET. IF 'YES' A FILE *
* CALLED 'JOIN.TXT' WILL BE CREATED *
*-----*
CLEAR
USE JOIN
STORE .T. TO CONT
IF .NOT. EOF()
DO WHILE CONT
STORE ' ' TO ANS
@ 1,1 SAY 'Do you wish to create a ASCII file? (Y/N) --->'
@ 1,49 GET ANS
READ
IF UPPER (ANS)='Y' .OR. UPPER(ANS)='N'
STORE .F. TO CONT
LOOP
ENDIF
ENDDO
IF UPPER(ANS) ='Y'
IF FILE(JOIN.TXT) THEN
DELETE FILE JOIN.TXT
ENDIF
COPY TO JOIN.TXT SDF DELIMITTED WITH BLANK
ENDIF
ENDIF

```

Once the data base has been created, the data is manipulated and statistically analyzed to provide the information based on which the initial choice for values of AQL and UQL is made. Following is a listing of the program which uses the data base and invokes SAS to analyze the data. Also, a sample of the output from the program that has used the P-501 Concrete flexural strength information is given and discussed.

5.2.2 Program Description 'SAS P-501'

The SAS program in this section illustrates how the P-501 Concrete flexural strength data was screened and how the remaining admissible data was used to determine values for AQL and UQL. The SAS program given herein can be easily modified to meet the specific format of the input ASCII data set. As mentioned in the previous subsection, only 28-day strength data was present in the ASCII data set and, therefore, only this type of data was in the input file P-501.DAT. If this would happen not to be the case, SAS can easily subset the data as needed based on an additional input variable, e.g., AGE.

The SAS program in file P501.SAS can be run in the batch mode by typing the following:

```
SAS P501
or
SAS P501.SAS
```

This will create two output files - P501.LOG (contains SAS input statements from P501.SAS with any error messages) and P501.LST that contains the desired output. After this batch SAS job has been completed, print P501.LST. The output should be examined carefully to determine the screening criteria (if different than what is specified in P501.SAS). If different screening criteria are desired, modify P501.SAS accordingly and run the SAS P501 program a second time using the above commands, e.g., SAS P501.

The SAS program can be run interactively using the SAS Display Manager. To do this, enter SAS at the DOS prompt. SAS will then show the Display Manager on the terminal screen. In the Program Editor portion of the 3 window screen Display Manager, enter the following at the Command line prompt:

```
INCLUDE "P501.SAS"
```

To execute the program, press Function Key F10. This will submit the program. The program output will be displayed in the OUTPUT window. To save this output for future viewing and printing, enter the following at the command line prompt within the OUTPUT window:

```
FILE "P501.LST"
```

This creates the ASCII file "P501.LST" that can then be printed out with the DOS command PRINT. For example, enter the following at the DOS prompt once you have exited from SAS:

```
PRINT P501.LST
```

Below is a listing of the contents of P501.SAS. The items highlighted with an asterisk are those that one may need to modify or adapt this program to meet his specific needs.

The names that follow, with underlines as spaces, such as LOT_NO, MEAN_STR, N_STR, STD_STR, and Q_STR are variable string file names and can also be found in Tables 5.1, 5.2, 5.3, and 5.4 and Figures 5.1 and 5.2.

```
TITLE "Determination of AQL and UQL using P-501 data";
TITLE2 "Performed on lots of 28 day strength";
TITLE3 "Lots with >= 4 samples";
OPTIONS PAGESIZE=62;
* INPUT FILE SHOULD CONTAIN THE 3 VARIABLES BELOW;
* ADDITIONAL VARIABLES MAY BE ADDED AS NEEDED;
DATA ONE;
    INFILE "P501.DAT";
    INPUT TESTDATE 1-8 STRENGTH 10-12 LOT_NO $ 14-20;
PROC SORT;
    BY TESTDATE LOT_NO;
*BELOW PROC MEANS CREATES DATASET WITH LOT MEANS;
PROC MEANS NOPRINT MEAN STD N;
    OUTPUT OUT = TWO MEAN = MEAN_STR N = N_STR STD = STD_STR;
    VAR STRENGTH; BY TESTDATE LOT_NO;
* BELOW SELECTS ONLY LOTS WITH >= 4 SAMPLES;
DATA THREE; SET TWO; IF N_STR >= 4;
* IF THE ACCEPTANCE CRITERIA CHANGE, 650 BELOW MAY NEED TO BE
MODIFIED;
    Q_STR = (MEAN_STR - 650)/STD_STR;
PROC SORT; BY MEAN_STR;
PROC PRINT;
    VAR TESTDATE LOT_NO N_STR MEAN_STR STD_STR Q_STR;
/* USE THIS PRINTOUT TO SCREEN DATA BASED ON MEAN */;
*BELOW ARE SAMPLE SCREENING CRITERIA FOR MEAN;
DATA FOUR; SET THREE; IF MEAN_STR > 500 AND MEAN_STR <1200;
PROC SORT; BY Q_STR;
PROC PRINT;
    VAR TESTDATE LOT_NO N_STR MEAN_STR STD_STR Q_STR;
/* USE THIS PRINTOUT TO SCREEN DATA BASED ON Q_STR */;
* BELOW ARE SAMPLE SCREENING CRITERIA FOR Q;
DATA FIVE; SET FOUR ; IF Q_STR > -3 AND Q_STR < 10;
*STATEMENTS BELOW SUMMARIZE SELECTED DATA;
* THIS OUTPUT SHOULD BE CLOSELY EXAMINED TO PICK THE AQL AND UQL;
PROC UNIVARIATE; VAR MEAN_STR Q_STR;
PROC CHART; HBAR MEAN_STR / MIDPOINTS = 550 TO 1000 BY 25;
PROC CHART; HBAR Q_STR / MIDPOINTS = 01 TO 05 BY .5;
RUN;
```

5.2.3 Sample Output

Shown in Tables 5.1, 5.2, 5.3, and 5.4 are sample outputs from running the program listed above. Table 5.1 displays the data arranged so that the calculated values of mean per lot are in ascending order. A lot is defined in this example as consisting of data from the same date and same project location. Also in these output samples, if the number of test values for a lot is less than 4, the lot was not admitted.

The data records recieved during the data collection had not made any distinction between the number of tests that constitute a lot, so it was determined to assign samples to a specific lot number for the same day. This is only for the previously collected data and should not apply to techniques in general and of future data. Hopefully, future test samples per lot will be somewhere between three and six. As such, the minimum number of tests in Column 4 of Table 5.1 is 4 and, as it turns out, the maximum number of test values is 28. Thus, the mean value for flexural strength per lot range from a minimum value of 105.2 psi to maximum value of 934.5 psi is as shown in Table 5.1.

The values for quality index, (Q), are listed in Table 5.2 in ascending order. The same restriction on minimum number of test values per lot (4), of course, is applied to the listing in Table 5.2. As can be seen in the program listing, the lower specification limit of 650 psi has been used in the calculation of Q listed in Table 5.2. This lower limit value may need to be modified for other/later applications. The values of Q listed in Table 5.2 are also restricted to values of the mean calculated and listed in Table 5.1 to be between 500 psi and 1200 psi. Correspondingly, the values of Q in Table 5.2 range from -2.927 to 59.273.

Table 5.3 lists the results of applying a univariate procedure to the values of the mean per lot between the limits of 500 psi and 1200 psi. Therein are the values for the parameters calculated from this procedure. The mean value and standard deviation for the population of test values for flexural strength, as determined from applying the above mentioned restrictions to the data base, are easily obtained from the listing in Table 5.3, as are other useful items such as 50% percentile, range, etc.

Similarly, Table 5.4 lists the results of applying a univariant procedure to values of Q listed per lot in Table 5.2.

Finally, shown in Figures 5.1 and 5.2 are the histograms for mean value of flexural strength and quality index, (Q), respectively. The histogram for mean value, Figure 5.1, indicates that the distribution of mean value is insignificantly different from normal. Therein about 50% of the values for mean value are above 750 psi.

TABLE 5.1
MEAN VALUES OF FLEXURAL STRENGTH FOR P-501 CONCRETE
FROM PROJECT TEST SPECIMENS

| OBS | TESTDATE | LOT_NO | N_STR | MEAN_STR | STD_STR | Q_STR |
|-----|----------|---------|-------|----------|---------|----------|
| 1 | 19860925 | BUF501 | 5 | 105.200 | 4.550 | -119.743 |
| 2 | 19860909 | BUF501 | 4 | 107.250 | 2.217 | -244.774 |
| 3 | 19850915 | SBY501 | 6 | 109.333 | 6.282 | -86.063 |
| 4 | 19850917 | SBY501 | 9 | 109.333 | 5.244 | -103.101 |
| 5 | 19860716 | BUF501 | 8 | 116.125 | 12.194 | -43.781 |
| 6 | 19860729 | BUF501 | 6 | 117.667 | 9.180 | -57.990 |
| 7 | 19850914 | SBY501 | 4 | 126.750 | 9.912 | -52.789 |
| 8 | 19851001 | ACY501A | 10 | 542.800 | 149.999 | -0.715 |
| 9 | 19850930 | ACY501A | 8 | 552.750 | 33.225 | -2.927 |
| 10 | 19850924 | ACY501A | 6 | 591.167 | 43.116 | -1.365 |
| 11 | 19850730 | PHL501A | 6 | 600.500 | 74.675 | -0.663 |
| 12 | 19850722 | PHL501A | 8 | 622.875 | 63.623 | -0.426 |
| 13 | 19850807 | PHL501A | 8 | 637.500 | 56.609 | -0.221 |
| 14 | 19860725 | IAD501A | 6 | 637.500 | 49.066 | -0.255 |
| 15 | 19860808 | BUF501A | 16 | 645.312 | 35.752 | -0.131 |
| 16 | 19800802 | SYR501A | 4 | 646.500 | 24.826 | -0.141 |
| 17 | 19860815 | BUF501A | 4 | 648.750 | 57.355 | -0.022 |
| 18 | 19860607 | IAD501A | 4 | 656.250 | 26.575 | 0.235 |
| 19 | 19860627 | IAD501A | 24 | 657.917 | 36.083 | 0.219 |
| 20 | 19860722 | IAD501A | 6 | 661.667 | 35.166 | 0.332 |
| 21 | 19800703 | SYR501A | 4 | 667.000 | 0.000 | . |
| 22 | 19800502 | SYR501A | 4 | 668.750 | 6.292 | 2.980 |
| 23 | 19860819 | BUF501A | 12 | 668.750 | 67.086 | 0.279 |
| 24 | 19851002 | ACY501A | 9 | 669.111 | 97.303 | 0.196 |
| 25 | 19840706 | ORF501B | 4 | 670.000 | 97.211 | 0.206 |
| 26 | 19800711 | SYR501A | 4 | 676.500 | 21.000 | 1.262 |
| 27 | 19850802 | PHL501A | 6 | 680.333 | 72.152 | 0.420 |
| 28 | 19860605 | IAD501A | 10 | 680.500 | 46.335 | 0.658 |
| 29 | 19860623 | IAD501A | 26 | 681.038 | 34.106 | 0.910 |
| 30 | 19860625 | IAD501A | 23 | 681.304 | 62.599 | 0.500 |
| 31 | 19860626 | IAD501A | 24 | 682.292 | 50.021 | 0.646 |
| 32 | 19800422 | SYR501A | 4 | 685.000 | 19.149 | 1.828 |
| 33 | 19850717 | PHL501A | 12 | 685.167 | 42.861 | 0.820 |
| 34 | 19840714 | ORF501B | 4 | 686.250 | 161.729 | 0.224 |
| 35 | 19850723 | PHL501A | 8 | 686.250 | 77.076 | 0.470 |
| 36 | 19850925 | ACY501A | 11 | 686.818 | 72.057 | 0.511 |
| 37 | 19800709 | SYR501A | 4 | 687.500 | 23.671 | 1.584 |
| 38 | 19860731 | BUF501A | 14 | 687.500 | 101.787 | 0.368 |
| 39 | 19850806 | PHL501A | 8 | 688.375 | 46.965 | 0.817 |
| 40 | 19850815 | PHL501A | 8 | 689.375 | 71.496 | 0.551 |
| 41 | 19001008 | PIT501A | 6 | 694.500 | 108.614 | 0.410 |
| 42 | 19860718 | PIT501C | 6 | 698.500 | 51.458 | 0.943 |
| 43 | 19800424 | SYR501A | 4 | 701.250 | 37.500 | 1.367 |
| 44 | 19850809 | PHL501A | 8 | 701.625 | 56.840 | 0.908 |
| 45 | 19860606 | IAD501A | 12 | 702.083 | 69.685 | 0.745 |
| 46 | 19860825 | BUF501A | 8 | 702.500 | 57.321 | 0.916 |
| 47 | 19850719 | PHL501A | 6 | 703.500 | 74.167 | 0.721 |
| 48 | 19860804 | BUF501A | 12 | 703.750 | 95.134 | 0.565 |
| 49 | 19850801 | PHL501A | 8 | 705.375 | 104.125 | 0.532 |
| 50 | 19840711 | ORF501B | 4 | 707.500 | 68.860 | 0.835 |
| 51 | 19860725 | BUF501A | 15 | 710.133 | 120.997 | 0.497 |
| 52 | 19800529 | SYR501A | 4 | 710.250 | 10.532 | 5.721 |
| 53 | 19860610 | IAD501A | 28 | 710.536 | 47.324 | 1.279 |
| 54 | 19860812 | BUF501A | 16 | 712.187 | 57.095 | 1.089 |
| 55 | 19860905 | PIT501C | 8 | 714.500 | 64.398 | 1.002 |

TABLE 5.1 (CONTINUED)
MEAN VALUES OF FLEXURAL STRENGTH FOR F-501 CONCRETE
FROM PROJECT TEST SPECIMENS

| CBS | TESTDATE | LOT_ID | N_STR | MEAN_STR | STD_STR | Q_STR |
|-----|----------|---------|-------|----------|---------|---------|
| 55 | 19860926 | BUF501A | 6 | 716.667 | 28.225 | 2.36195 |
| 57 | 19800203 | SYR501A | 4 | 718.750 | 52.519 | 1.30905 |
| 58 | 19800430 | SYR501A | 4 | 720.000 | 60.000 | 1.16667 |
| 59 | 19840712 | ORF501B | 4 | 721.250 | 56.624 | 1.25831 |
| 60 | 19860903 | BUF501A | 5 | 723.000 | 55.969 | 1.30430 |
| 61 | 19850627 | PHL501A | 6 | 723.167 | 44.638 | 1.63911 |
| 62 | 19850718 | PHL501A | 8 | 724.250 | 78.640 | 0.94419 |
| 63 | 19850815 | ACY501A | 6 | 724.500 | 150.488 | 0.49506 |
| 64 | 19860904 | BUF501A | 18 | 726.389 | 92.495 | 0.82587 |
| 65 | 19860902 | BUF501A | 24 | 726.458 | 98.063 | 0.77969 |
| 66 | 19800702 | SYR501A | 4 | 729.000 | 24.249 | 3.25791 |
| 67 | 19860829 | BUF501A | 8 | 733.125 | 46.209 | 1.79889 |
| 68 | 19860820 | BUF501A | 12 | 733.333 | 78.432 | 1.06250 |
| 69 | 19850724 | PHL501A | 8 | 733.500 | 64.029 | 1.30410 |
| 70 | 19840625 | ORF501B | 4 | 735.000 | 27.988 | 3.03701 |
| 71 | 19000922 | PIT501A | 4 | 737.500 | 30.838 | 2.83739 |
| 72 | 19800605 | SYR501A | 4 | 739.000 | 39.345 | 2.26206 |
| 73 | 19800602 | SYR501A | 4 | 739.500 | 21.000 | 4.26190 |
| 74 | 19800703 | SYR501A | 4 | 739.500 | 21.000 | 4.26190 |
| 75 | 19800905 | SYR501A | 4 | 739.750 | 62.612 | 1.43343 |
| 76 | 19850731 | PHL501A | 8 | 740.250 | 22.977 | 3.92789 |
| 77 | 19860723 | BUF501A | 13 | 743.077 | 113.294 | 0.82155 |
| 78 | 19850916 | ACY501A | 4 | 747.750 | 68.515 | 1.42670 |
| 79 | 19850821 | ACY501A | 5 | 749.800 | 61.329 | 1.62730 |
| 80 | 19860828 | BUF501A | 15 | 750.333 | 76.262 | 1.31563 |
| 81 | 19860917 | BUF501A | 11 | 754.545 | 113.720 | 0.91932 |
| 82 | 19840703 | ORF501B | 4 | 760.000 | 41.433 | 2.65491 |
| 83 | 19800827 | SYR501A | 4 | 760.250 | 62.612 | 1.76085 |
| 84 | 19860729 | BUF501A | 10 | 760.500 | 102.671 | 1.07625 |
| 85 | 19850725 | PHL501A | 8 | 761.125 | 56.453 | 1.96844 |
| 86 | 19860806 | BUF501A | 15 | 761.733 | 95.619 | 1.16853 |
| 87 | 19000927 | PIT501A | 7 | 764.286 | 72.200 | 1.58289 |
| 88 | 19860731 | PIT501C | 8 | 765.500 | 89.822 | 1.28588 |
| 89 | 19850910 | ACY501A | 4 | 768.250 | 42.161 | 2.80470 |
| 90 | 19850919 | ACY501A | 8 | 768.375 | 70.470 | 1.67980 |
| 91 | 19860826 | BUF501A | 4 | 768.750 | 62.899 | 1.88796 |
| 92 | 19860930 | BUF501A | 10 | 769.000 | 105.720 | 1.12562 |
| 93 | 19860815 | PIT501C | 8 | 771.750 | 71.250 | 1.70878 |
| 94 | 19850926 | ACY501A | 8 | 772.375 | 79.859 | 1.53239 |
| 95 | 19850909 | ACY501A | 8 | 772.625 | 83.671 | 1.46556 |
| 96 | 19850826 | ACY501A | 9 | 772.667 | 69.660 | 1.76094 |
| 97 | 19850809 | ACY501A | 7 | 773.857 | 55.769 | 2.22091 |
| 98 | 19860818 | PIT501C | 8 | 774.875 | 89.558 | 1.39434 |
| 99 | 19001009 | PIT501A | 8 | 776.125 | 53.116 | 2.37454 |
| 100 | 19001002 | PIT501A | 7 | 776.429 | 63.916 | 1.97804 |
| 101 | 19850822 | ACY501A | 9 | 778.444 | 99.638 | 1.28911 |
| 102 | 19850923 | ACY501A | 7 | 779.429 | 50.731 | 2.55128 |
| 103 | 19860725 | PIT501C | 8 | 780.125 | 91.940 | 1.41532 |
| 104 | 19850729 | PHL501A | 8 | 780.500 | 50.265 | 2.59624 |
| 105 | 19840626 | ORF501B | 4 | 781.250 | 63.031 | 2.08231 |
| 106 | 19860912 | ACY501A | 8 | 782.875 | 41.824 | 3.17698 |
| 107 | 19840628 | ORF501B | 4 | 785.000 | 54.772 | 2.46475 |
| 108 | 19860905 | BUF501A | 23 | 785.000 | 85.918 | 1.57127 |
| 109 | 19850828 | ACY501A | 10 | 785.500 | 104.602 | 1.29538 |
| 110 | 19860721 | BUF501A | 13 | 788.077 | 141.871 | 0.97326 |

TABLE 5.1 (CONTINUED)
MEAN VALUES OF FLEXURAL STRENGTH FOR P-501 CONCRETE
FROM PROJECT TEST SPECIMENS

| OES | TESTDATE | LOT_NO | N_STR | MEAN_STR | STD_STR | Q_STR |
|-----|----------|---------|-------|----------|---------|---------|
| 111 | 19850812 | ACY501A | 6 | 788.933 | 57.825 | 2.4009 |
| 112 | 19860814 | BUF501A | 4 | 790.000 | 197.146 | 0.7101 |
| 113 | 19000925 | PIT501A | 6 | 791.667 | 156.340 | 0.9061 |
| 114 | 19850823 | ACY501A | 8 | 792.375 | 70.385 | 2.0223 |
| 115 | 19860724 | PIT501C | 8 | 797.875 | 99.919 | 1.4799 |
| 116 | 19860305 | PIT501C | 8 | 799.875 | 58.973 | 2.5414 |
| 117 | 19840720 | ORF501B | 4 | 800.000 | 61.914 | 2.4227 |
| 118 | 19850918 | ACY501A | 9 | 801.556 | 36.049 | 4.2042 |
| 119 | 19860319 | BUF501A | 6 | 801.667 | 92.340 | 1.6425 |
| 120 | 19850913 | ACY501A | 9 | 807.111 | 79.186 | 1.9841 |
| 121 | 19840822 | ORF501B | 4 | 807.500 | 99.121 | 1.5890 |
| 122 | 19860910 | BUF501A | 17 | 807.941 | 96.583 | 1.6353 |
| 123 | 19860908 | BUF501A | 25 | 808.800 | 122.273 | 1.2987 |
| 124 | 19850814 | ACY501A | 8 | 810.750 | 84.825 | 1.8951 |
| 125 | 19860918 | BUF501A | 17 | 813.529 | 81.120 | 2.0159 |
| 126 | 19850813 | ACY501A | 7 | 815.288 | 37.196 | 4.4436 |
| 127 | 19840830 | ORF501B | 4 | 818.750 | 64.080 | 2.6334 |
| 128 | 19860902 | PIT501C | 6 | 820.833 | 82.891 | 2.0609 |
| 129 | 19860716 | BUF501A | 8 | 821.875 | 157.819 | 1.0891 |
| 130 | 19860806 | PIT501C | 7 | 827.143 | 106.490 | 1.6635 |
| 131 | 19860811 | PIT501C | 4 | 827.250 | 78.704 | 2.2521 |
| 132 | 19860903 | PIT501C | 8 | 829.250 | 44.784 | 4.0025 |
| 133 | 19840824 | ORF501B | 4 | 830.000 | 14.720 | 12.2286 |
| 134 | 19860717 | PIT501C | 4 | 832.750 | 78.987 | 2.3137 |
| 135 | 19860925 | BUF501A | 13 | 833.462 | 109.209 | 1.6799 |
| 136 | 19850920 | ACY501A | 9 | 835.000 | 82.271 | 2.2487 |
| 137 | 19850827 | ACY501A | 10 | 842.000 | 106.298 | 1.8062 |
| 138 | 19861006 | PIT501C | 6 | 844.333 | 10.132 | 19.1793 |
| 139 | 19860716 | PIT501C | 6 | 848.167 | 75.656 | 2.6193 |
| 140 | 19860904 | PIT501C | 6 | 849.833 | 87.605 | 2.2811 |
| 141 | 19850816 | ACY501A | 7 | 851.000 | 53.276 | 3.7728 |
| 142 | 19850911 | ACY501A | 8 | 851.625 | 81.477 | 2.4746 |
| 143 | 19860825 | PIT501C | 7 | 853.571 | 72.415 | 2.8112 |
| 144 | 19831023 | ROC501A | 4 | 857.500 | 66.521 | 3.1193 |
| 145 | 19860814 | PIT501C | 8 | 858.375 | 31.409 | 6.6341 |
| 146 | 19850819 | ACY501A | 4 | 860.000 | 38.410 | 5.4673 |
| 147 | 19850905 | ACY501A | 8 | 862.125 | 37.813 | 5.6098 |
| 148 | 19860808 | PIT501C | 8 | 864.625 | 87.106 | 2.4640 |
| 149 | 19860812 | PIT501C | 7 | 866.571 | 40.070 | 5.4048 |
| 150 | 19860826 | PIT501C | 8 | 866.625 | 66.982 | 3.2341 |
| 151 | 19860829 | PIT501C | 8 | 869.625 | 70.587 | 3.1114 |
| 152 | 19860912 | BUF501A | 4 | 870.000 | 63.770 | 3.4499 |
| 153 | 19800903 | SYR501A | 4 | 874.750 | 58.926 | 3.8141 |
| 154 | 19831010 | ROC501A | 4 | 875.000 | 47.958 | 4.6916 |
| 155 | 19850906 | ACY501A | 8 | 876.625 | 50.242 | 4.5107 |
| 156 | 19851016 | SBY501A | 4 | 877.000 | 41.960 | 5.4099 |
| 157 | 19840723 | ORF501B | 4 | 887.500 | 46.458 | 5.1122 |
| 158 | 19860822 | PIT501C | 7 | 890.571 | 74.231 | 3.2408 |
| 159 | 19870203 | ORF501A | 4 | 891.250 | 24.622 | 9.7981 |
| 160 | 19831021 | ROC501A | 4 | 895.000 | 54.467 | 4.4981 |
| 161 | 19850807 | ACY501A | 5 | 911.200 | 42.044 | 6.2125 |
| 162 | 19831019 | ROC501A | 5 | 921.000 | 37.483 | 7.2299 |
| 163 | 19851014 | SBY501A | 7 | 925.429 | 49.490 | 5.5653 |
| 164 | 19870101 | ORF501A | 4 | 933.750 | 4.787 | 59.2734 |
| 165 | 19851017 | SBY501A | 4 | 934.500 | 37.599 | 7.5667 |

TABLE 5.2
VALUES OF QUALITY INDEX, Q, FOR P-501 CONCRETE

| OES | TESTDATE | LOT_NO | N_STR | MEAN_STR | STD_STR | Q_STR |
|-----|----------|---------|-------|----------|---------|----------|
| 1 | 19800708 | SYR501A | 4 | 667.000 | 0.000 | . |
| 2 | 19850933 | ACY501A | 8 | 552.750 | 33.225 | -2.92693 |
| 3 | 19850924 | ACY501A | 6 | 591.167 | 43.115 | -1.36454 |
| 4 | 19851001 | ACY501A | 10 | 542.800 | 149.999 | -0.71467 |
| 5 | 19850730 | PHL501A | 6 | 600.500 | 74.675 | -0.66289 |
| 6 | 19850722 | PHL501A | 8 | 622.875 | 63.623 | -0.42634 |
| 7 | 19860725 | IAD501A | 6 | 637.500 | 49.066 | -0.25476 |
| 8 | 19850807 | PHL501A | 8 | 637.500 | 56.609 | -0.22081 |
| 9 | 19800802 | SYR501A | 4 | 646.500 | 24.826 | -0.14099 |
| 10 | 19860803 | BUF501A | 16 | 645.312 | 35.752 | -0.13111 |
| 11 | 19860815 | BUF501A | 4 | 648.750 | 57.355 | -0.02179 |
| 12 | 19851002 | ACY501A | 9 | 669.111 | 97.308 | 0.19640 |
| 13 | 19840706 | ORF501B | 4 | 670.000 | 97.211 | 0.20574 |
| 14 | 19860627 | IAD501A | 24 | 657.917 | 36.083 | 0.21940 |
| 15 | 19840714 | ORF501B | 4 | 686.250 | 161.729 | 0.22414 |
| 16 | 19860607 | IAD501A | 4 | 656.250 | 26.575 | 0.23518 |
| 17 | 19860819 | BUF501A | 12 | 668.750 | 67.086 | 0.27949 |
| 18 | 19860722 | IAD501A | 6 | 661.667 | 35.166 | 0.33176 |
| 19 | 19860731 | BUF501A | 14 | 687.500 | 101.787 | 0.36842 |
| 20 | 19001008 | PIT501A | 6 | 694.500 | 108.614 | 0.40971 |
| 21 | 19850802 | PHL501A | 6 | 680.333 | 72.152 | 0.42041 |
| 22 | 19850723 | PHL501A | 8 | 686.250 | 77.076 | 0.47031 |
| 23 | 19850815 | ACY501A | 6 | 724.500 | 150.488 | 0.49503 |
| 24 | 19860725 | BUF501A | 15 | 710.133 | 120.997 | 0.49698 |
| 25 | 19860625 | IAD501A | 23 | 681.304 | 62.599 | 0.50007 |
| 26 | 19850925 | ACY501A | 11 | 686.818 | 72.057 | 0.51096 |
| 27 | 19850801 | PHL501A | 8 | 705.375 | 104.125 | 0.53181 |
| 28 | 19850815 | PHL501A | 8 | 689.375 | 71.496 | 0.55073 |
| 29 | 19860804 | BUF501A | 12 | 703.750 | 95.134 | 0.56499 |
| 30 | 19860626 | IAD501A | 24 | 682.292 | 50.021 | 0.64556 |
| 31 | 19860605 | IAD501A | 10 | 680.500 | 46.335 | 0.65825 |
| 32 | 19860814 | BUF501A | 4 | 790.000 | 197.146 | 0.71013 |
| 33 | 19850719 | PHL501A | 6 | 703.500 | 74.167 | 0.72135 |
| 34 | 19860606 | IAD501A | 12 | 702.083 | 69.885 | 0.74527 |
| 35 | 19860902 | BUF501A | 24 | 726.458 | 98.063 | 0.77969 |
| 36 | 19850806 | PHL501A | 8 | 688.375 | 46.965 | 0.81710 |
| 37 | 19850717 | PHL501A | 12 | 685.167 | 42.861 | 0.82048 |
| 38 | 19860723 | BUF501A | 13 | 743.077 | 113.294 | 0.82155 |
| 39 | 19860904 | BUF501A | 18 | 726.389 | 92.495 | 0.82587 |
| 40 | 19840711 | ORF501B | 4 | 707.500 | 68.860 | 0.83503 |
| 41 | 19000925 | PIT501A | 6 | 791.667 | 156.340 | 0.90614 |
| 42 | 19850809 | PHL501A | 8 | 701.625 | 56.840 | 0.90824 |
| 43 | 19860623 | IAD501A | 26 | 681.038 | 34.106 | 0.91005 |
| 44 | 19860825 | BUF501A | 8 | 702.500 | 57.321 | 0.91589 |
| 45 | 19860917 | BUF501A | 11 | 754.545 | 113.720 | 0.91932 |
| 46 | 19860718 | PIT501C | 6 | 698.500 | 51.458 | 0.94252 |
| 47 | 19850718 | PHL501A | 8 | 724.250 | 78.640 | 0.94418 |
| 48 | 19860721 | BUF501A | 13 | 788.077 | 141.871 | 0.97326 |
| 49 | 19860905 | PIT501C | 8 | 714.500 | 64.398 | 1.00158 |
| 50 | 19860820 | BUF501A | 12 | 733.333 | 78.432 | 1.06250 |
| 51 | 19860729 | BUF501A | 10 | 760.500 | 102.671 | 1.07625 |
| 52 | 19860716 | BUF501A | 8 | 821.875 | 157.819 | 1.08907 |
| 53 | 19860812 | BUF501A | 16 | 712.187 | 57.095 | 1.08918 |
| 54 | 19860930 | BUF501A | 10 | 769.000 | 105.720 | 1.12562 |
| 55 | 19800430 | SYR501A | 4 | 720.000 | 60.000 | 1.16667 |

TABLE 5.2 (CONTINUED)
VALUES OF QUALITY INDEX, Q, FOR P-501 CONCRETE

| OSS | TESTDATE | LCT_NO | N_STR | MEAN_STR | STD_STR | Q_STR |
|-----|----------|---------|-------|----------|---------|---------|
| 55 | 19860305 | BUF501A | 15 | 761.733 | 95.619 | 1.16853 |
| 57 | 19840712 | ORF501B | 4 | 721.250 | 56.624 | 1.25831 |
| 58 | 19800711 | SYR501A | 4 | 676.500 | 21.000 | 1.26190 |
| 59 | 19860610 | IAD501A | 28 | 710.536 | 47.324 | 1.27919 |
| 60 | 19860731 | PIT501C | 8 | 765.500 | 89.822 | 1.28528 |
| 61 | 19850822 | ACY501A | 9 | 778.444 | 99.638 | 1.28911 |
| 62 | 19850828 | ACY501A | 10 | 785.500 | 104.602 | 1.29539 |
| 63 | 19860908 | BUF501A | 25 | 808.800 | 122.273 | 1.29874 |
| 64 | 19850724 | PHL501A | 8 | 733.500 | 64.029 | 1.30410 |
| 65 | 19860909 | BUF501A | 5 | 723.000 | 55.969 | 1.30430 |
| 66 | 19800808 | SYR501A | 4 | 718.750 | 52.519 | 1.30905 |
| 67 | 19860828 | BUF501A | 15 | 750.333 | 76.262 | 1.31563 |
| 68 | 19800424 | SYR501A | 4 | 701.250 | 37.500 | 1.36667 |
| 69 | 19860818 | PIT501C | 8 | 774.875 | 89.558 | 1.39434 |
| 70 | 19860725 | PIT501C | 8 | 780.125 | 91.940 | 1.41532 |
| 71 | 19850916 | ACY501A | 4 | 747.750 | 68.515 | 1.42670 |
| 72 | 19800905 | SYR501A | 4 | 739.750 | 62.612 | 1.43343 |
| 73 | 19850909 | ACY501A | 8 | 772.625 | 83.671 | 1.46556 |
| 74 | 19860724 | PIT501C | 8 | 797.875 | 99.919 | 1.47995 |
| 75 | 19850926 | ACY501A | 8 | 772.375 | 79.859 | 1.53239 |
| 76 | 19860905 | BUF501A | 23 | 785.000 | 85.918 | 1.57127 |
| 77 | 19000927 | PIT501A | 7 | 764.286 | 72.200 | 1.58289 |
| 78 | 19800709 | SYR501A | 4 | 687.500 | 23.671 | 1.58419 |
| 79 | 19840822 | ORF501B | 4 | 807.500 | 99.121 | 1.58896 |
| 80 | 19850821 | ACY501A | 5 | 749.800 | 61.329 | 1.62730 |
| 81 | 19860910 | BUF501A | 17 | 807.941 | 96.583 | 1.63529 |
| 82 | 19850627 | PHL501A | 6 | 723.167 | 44.638 | 1.63911 |
| 83 | 19860919 | BUF501A | 6 | 801.667 | 92.340 | 1.64248 |
| 84 | 19860806 | PIT501C | 7 | 827.143 | 106.490 | 1.66347 |
| 85 | 19850919 | ACY501A | 8 | 768.375 | 70.470 | 1.67980 |
| 86 | 19860925 | BUF501A | 13 | 833.462 | 109.209 | 1.67991 |
| 87 | 19860815 | PIT501C | 8 | 771.750 | 71.250 | 1.70878 |
| 88 | 19800827 | SYR501A | 4 | 760.250 | 62.612 | 1.76085 |
| 89 | 19850826 | ACY501A | 9 | 772.667 | 69.660 | 1.76094 |
| 90 | 19860829 | BUF501A | 8 | 733.125 | 46.209 | 1.79889 |
| 91 | 19850827 | ACY501A | 10 | 842.000 | 106.298 | 1.80624 |
| 92 | 19800422 | SYR501A | 4 | 685.000 | 19.149 | 1.82782 |
| 93 | 19860826 | BUF501A | 4 | 768.750 | 62.899 | 1.88796 |
| 94 | 19850814 | ACY501A | 8 | 810.750 | 84.825 | 1.89507 |
| 95 | 19850725 | PHL501A | 8 | 761.125 | 56.453 | 1.96844 |
| 96 | 19001002 | PIT501A | 7 | 776.429 | 83.916 | 1.97804 |
| 97 | 19850913 | ACY501A | 9 | 807.111 | 79.186 | 1.98409 |
| 98 | 19860918 | BUF501A | 17 | 813.529 | 81.120 | 2.01589 |
| 99 | 19850823 | ACY501A | 8 | 792.375 | 70.385 | 2.02282 |
| 100 | 19860902 | PIT501C | 6 | 820.833 | 82.891 | 2.06093 |
| 101 | 19840626 | ORF501B | 4 | 781.250 | 63.031 | 2.08231 |
| 102 | 19850809 | ACY501A | 7 | 773.857 | 55.769 | 2.22091 |
| 103 | 19850920 | ACY501A | 9 | 835.000 | 82.271 | 2.24867 |
| 104 | 19860811 | PIT501C | 4 | 827.250 | 78.704 | 2.25212 |
| 105 | 19800605 | SYR501A | 4 | 739.000 | 39.345 | 2.26208 |
| 106 | 19860904 | PIT501C | 6 | 849.833 | 87.605 | 2.28108 |
| 107 | 19860717 | PIT501C | 4 | 832.750 | 78.987 | 2.31368 |
| 108 | 19860926 | BUF501A | 6 | 716.667 | 28.225 | 2.36195 |
| 109 | 19001009 | PIT501A | 8 | 776.125 | 53.116 | 2.37454 |
| 110 | 19850812 | ACY501A | 6 | 788.833 | 57.825 | 2.40091 |

TABLE 5.2 (CONTINUED)
VALUES OF QUALITY INDEX, Q, FOR P-501 CONCRETE

| OBS | TESTDATE | LOT_NO | N_STR | MEAN_STR | STD_STR | Q_STR |
|-----|----------|---------|-------|----------|---------|---------|
| 111 | 19840720 | ORF501B | 4 | 800.000 | 61.9133 | 2.4227 |
| 112 | 19860803 | PIT501C | 8 | 864.625 | 87.1057 | 2.4640 |
| 113 | 19840628 | ORF501B | 4 | 785.000 | 54.7723 | 2.4648 |
| 114 | 19850311 | ACY501A | 8 | 851.625 | 81.4773 | 2.4746 |
| 115 | 19860805 | PIT501C | 8 | 799.975 | 59.9732 | 2.5414 |
| 116 | 19850923 | ACY501A | 7 | 779.429 | 50.7308 | 2.5513 |
| 117 | 19850729 | PHL501A | 8 | 780.500 | 50.2650 | 2.5562 |
| 118 | 19860716 | PIT501C | 6 | 848.167 | 75.6556 | 2.6193 |
| 119 | 19840830 | ORF501B | 4 | 818.750 | 64.0800 | 2.6334 |
| 120 | 19840703 | ORF501B | 4 | 760.000 | 41.4327 | 2.6549 |
| 121 | 19850910 | ACY501A | 4 | 768.250 | 42.1614 | 2.8047 |
| 122 | 19860825 | PIT501C | 7 | 853.571 | 72.4151 | 2.8112 |
| 123 | 19000922 | PIT501A | 4 | 737.500 | 30.8383 | 2.8374 |
| 124 | 19800502 | SYR501A | 4 | 668.750 | 6.2915 | 2.9802 |
| 125 | 19840625 | ORF501B | 4 | 735.000 | 27.9881 | 3.0370 |
| 126 | 19860829 | PIT501C | 8 | 869.625 | 70.5872 | 3.1114 |
| 127 | 19831028 | ROC501A | 4 | 857.500 | 66.5207 | 3.1193 |
| 128 | 19860912 | ACY501A | 8 | 782.875 | 41.8242 | 3.1770 |
| 129 | 19860826 | PIT501C | 8 | 866.625 | 66.9817 | 3.2341 |
| 130 | 19860822 | PIT501C | 7 | 890.571 | 74.2313 | 3.2408 |
| 131 | 19800702 | SYR501A | 4 | 729.000 | 24.2487 | 3.2579 |
| 132 | 19860912 | BUF501A | 4 | 870.000 | 63.7704 | 3.4499 |
| 133 | 19850816 | ACY501A | 7 | 851.000 | 53.2760 | 3.7728 |
| 134 | 19800903 | SYR501A | 4 | 874.750 | 58.9258 | 3.8141 |
| 135 | 19850731 | PHL501A | 8 | 740.250 | 22.9767 | 3.9279 |
| 136 | 19860903 | PIT501C | 8 | 829.250 | 44.7844 | 4.0025 |
| 137 | 19850918 | ACY501A | 9 | 801.556 | 36.0490 | 4.2042 |
| 138 | 19800602 | SYR501A | 4 | 739.500 | 21.0000 | 4.2619 |
| 139 | 19800703 | SYR501A | 4 | 739.500 | 21.0000 | 4.2619 |
| 140 | 19850813 | ACY501A | 7 | 815.286 | 37.1964 | 4.4436 |
| 141 | 19831021 | ROC501A | 4 | 895.000 | 54.4671 | 4.4981 |
| 142 | 19850906 | ACY501A | 8 | 876.625 | 50.2421 | 4.5107 |
| 143 | 19831010 | ROC501A | 4 | 875.000 | 47.9583 | 4.6916 |
| 144 | 19840723 | ORF501B | 4 | 887.500 | 48.4579 | 5.1122 |
| 145 | 19860812 | PIT501C | 7 | 866.571 | 40.0702 | 5.4048 |
| 146 | 19851016 | SBY501A | 4 | 877.000 | 41.9603 | 5.4099 |
| 147 | 19850819 | ACY501A | 4 | 860.000 | 38.4101 | 5.4673 |
| 148 | 19851014 | SBY501A | 7 | 925.429 | 49.4903 | 5.5653 |
| 149 | 19850905 | ACY501A | 8 | 862.125 | 37.8132 | 5.6098 |
| 150 | 19800529 | SYR501A | 4 | 710.250 | 10.5317 | 5.7208 |
| 151 | 19850807 | ACY501A | 5 | 911.200 | 42.0440 | 6.2125 |
| 152 | 19860814 | PIT501C | 8 | 858.375 | 31.4095 | 6.6341 |
| 153 | 19831019 | ROC501A | 5 | 921.000 | 37.4833 | 7.2299 |
| 154 | 19851017 | SBY501A | 4 | 934.500 | 37.5988 | 7.5667 |
| 155 | 19870203 | ORF501A | 4 | 891.250 | 24.6221 | 9.7981 |
| 156 | 19840824 | ORF501B | 4 | 830.000 | 14.7196 | 12.2286 |
| 157 | 19861006 | PIT501C | 6 | 844.333 | 10.1325 | 19.1793 |
| 158 | 19870101 | ORF501A | 4 | 933.750 | 4.7871 | 59.2734 |

TABLE 5.3
UNIVARIATE ANALYSIS FOR MEAN VALUE OF FLEXURAL STRENGTH
FOR P-501 CONCRETE

UNIVARIATE PROCEDURE

Variable=MEAN_STR

Moments

| | | | |
|----------|----------|----------|----------|
| N | 154 | Sum Wgts | 154 |
| Mean | 759.9162 | Sum | 117027.1 |
| Std Dev | 76.70439 | Variance | 5883.564 |
| Skewness | -0.04201 | Kurtosis | -0.19977 |
| USS | 89830982 | CSS | 900185.3 |
| CV | 10.0938 | Std Mean | 6.181016 |
| T:Mean=0 | 122.9436 | Prob> T | 0.0001 |
| Sgn Rank | 5967.5 | Prob> S | 0.0001 |
| Num ^= 0 | 154 | | |

Quantiles(Def=5)

| | | | |
|----------|----------|-----|----------|
| 100% Max | 934.5 | 99% | 925.4286 |
| 75% Q3 | 810.75 | 95% | 887.5 |
| 50% Med | 761.4292 | 90% | 866.5714 |
| 25% Q1 | 703.5 | 10% | 669.1111 |
| 0% Min | 542.8 | 5% | 645.3125 |
| | | 1% | 552.75 |
| Range | 391.7 | | |
| Q3-Q1 | 107.25 | | |
| Mode | 637.5 | | |

Extremes

| Lowest | Obs | Highest | Obs |
|-----------|-----|-----------|------|
| 542.8(| 3) | 895(| 140) |
| 552.75(| 1) | 911.2(| 150) |
| 591.1667(| 2) | 921(| 152) |
| 600.5(| 4) | 925.4286(| 147) |
| 622.875(| 5) | 934.5(| 153) |

TABLE 5.4
UNIVARIATE ANALYSIS FOR QUALITY INDEX, (Q),
FOR P-501 CONCRETE

UNIVARIATE PROCEDURE

Variable=Q_STR

Moments

| | | | |
|----------|----------|----------|----------|
| N | 154 | Sum Wgts | 154 |
| Mean | 1.96244 | Sum | 302.2158 |
| Std Dev | 1.780377 | Variance | 3.169741 |
| Skewness | 1.264815 | Kurtosis | 2.909319 |
| USS | 1078.051 | CSS | 484.9703 |
| CV | 90.72258 | Std Mean | 0.143467 |
| T:Mean=0 | 13.67871 | Prob> T | 0.0001 |
| Sgn Rank | 5685.5 | Prob> S | 0.0001 |
| Num ^= 0 | 154 | | |

Quantiles(Def=5)

| | | | |
|----------|----------|-----|----------|
| 100% Max | 9.79809 | 99% | 7.566739 |
| 75% Q3 | 2.596239 | 95% | 5.565309 |
| 50% Med | 1.586579 | 90% | 4.443596 |
| 25% Q1 | 0.83503 | 10% | 0.279491 |
| 0% Min | -2.92698 | 5% | -0.14098 |
| | | 1% | -1.36454 |
| Range | 12.72507 | | |
| Q3-Q1 | 1.761209 | | |
| Mode | 4.261905 | | |

Extremes

| Lowest | Obs | Highest | Obs |
|-----------|-----|-----------|------|
| -2.92698(| 1) | 6.212536(| 150) |
| -1.36454(| 2) | 6.63415(| 151) |
| -0.71467(| 3) | 7.229881(| 152) |
| -0.66288(| 4) | 7.566739(| 153) |
| -0.42634(| 5) | 9.79809(| 154) |

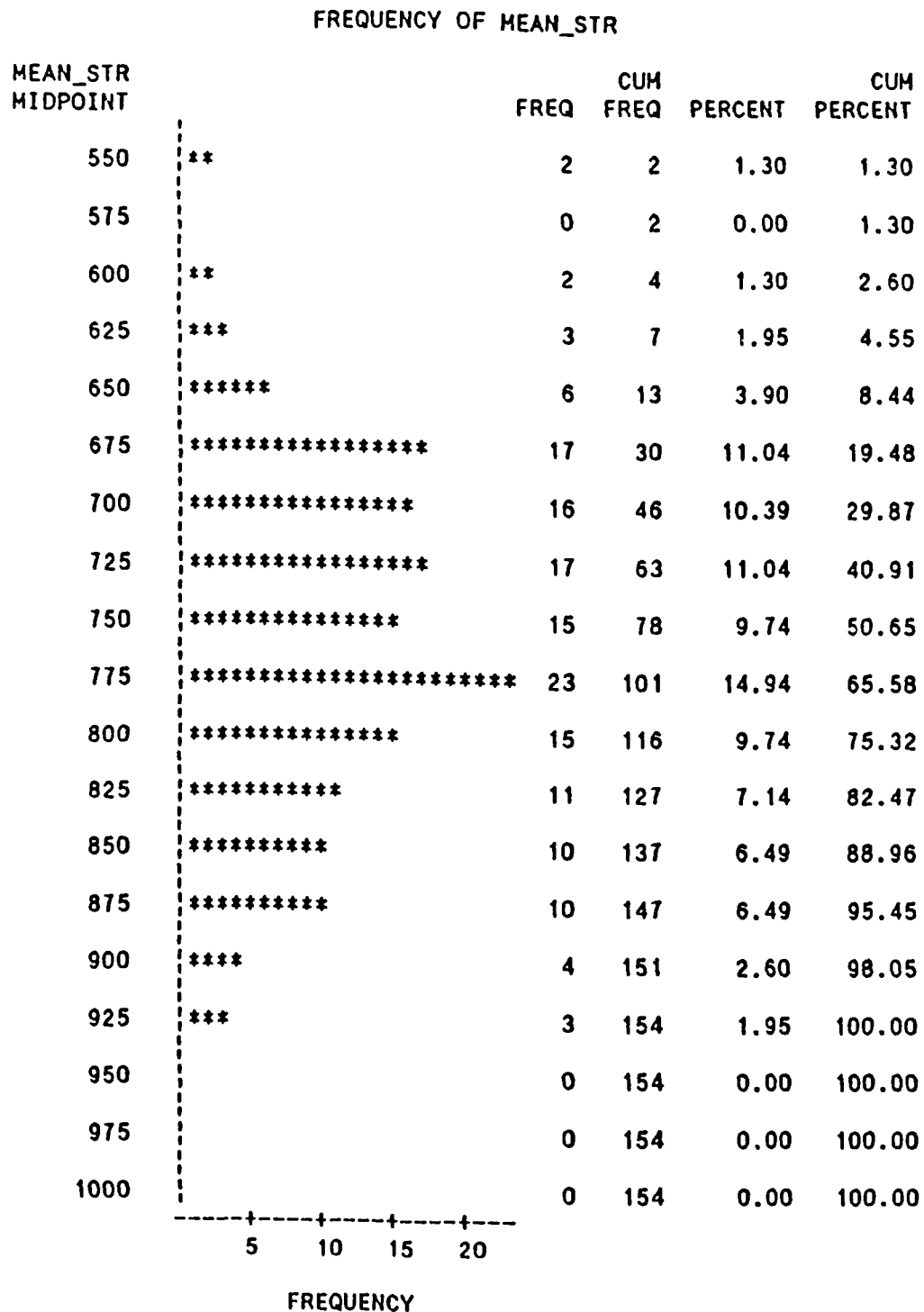


FIGURE 5.1. HISTOGRAM FOR MEAN VALUE OF FLEXURAL STRENGTH FOR P-501 CONCRETE

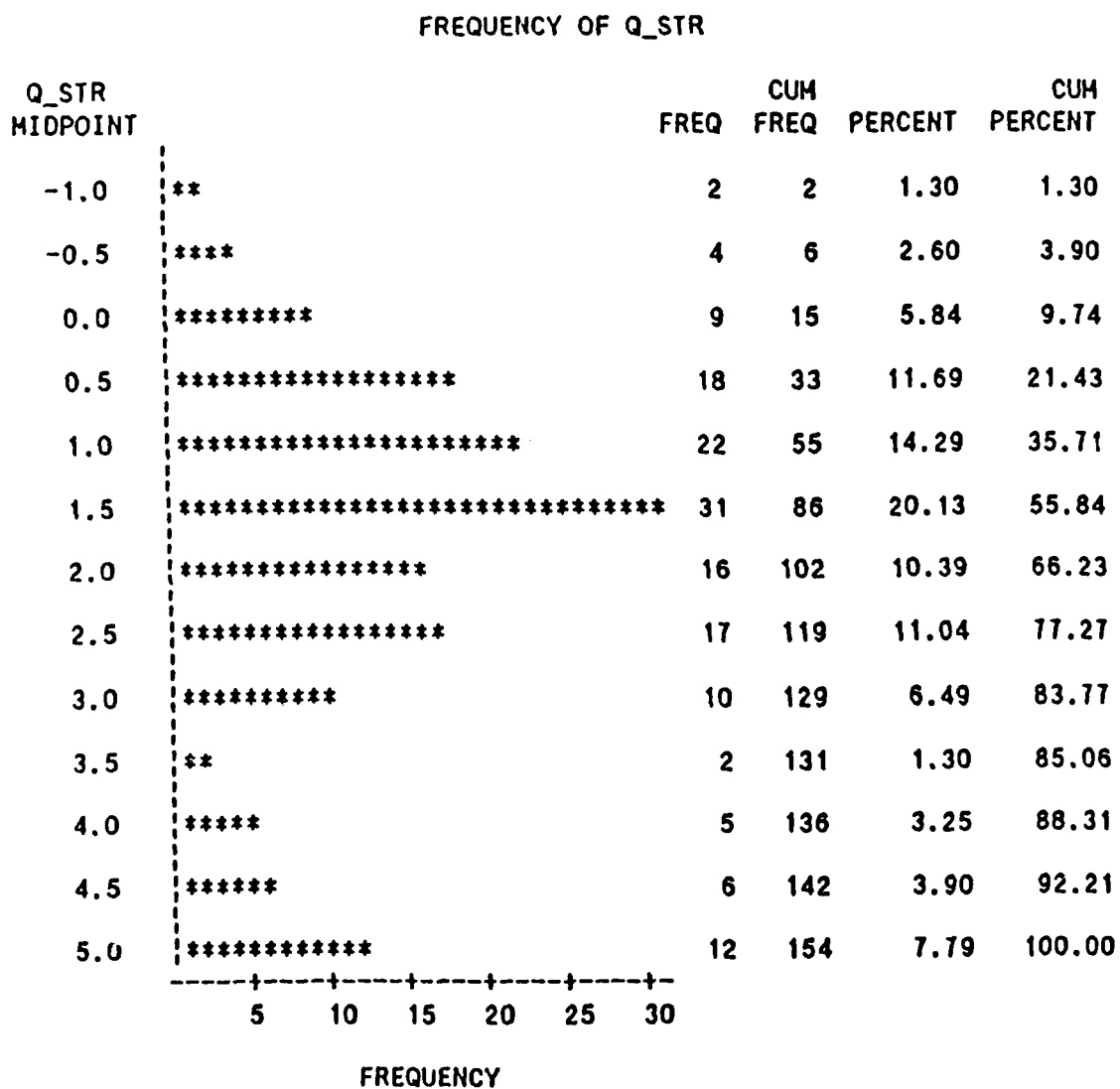


FIGURE 5.2. HISTOGRAM FOR QUALITY INDEX, (Q)
FOR P-501 CONCRETE

The histogram for Q, Figure 5.2, is the primary ingredient in the selection of values for AQL and UQL. Figure 5.2 reveals that the 50th percentile has a value of Q between 1.0 and 1.5. If we pick a value for Q within this range, we could use one of the formulas in Chapter 4 to calculate EPAL and this would yield an initial choice for AQL. Unfortunately, the listings in Tables 5.1 through 5.4 are not for consistent sample size.

Recall the restriction on lot size. Lot size was determined in this example for number of test values greater than or equal to four per date and location. As such, the values of Q calculated from these data are based on sample sizes ranging from 4 units to 28 units. Thus, which of the formulas to use from Chapter 4 is unclear in this example.

When the data is arranged so that lot size is (fairly) consistent, calculation of AQL from the appropriate formula of Chapter 4 follows without difficulty. Again, the reason for the choice of value of Q around the 50th percentile is that this value reflects, in the main, what the industry typically produces without undue hardship.

In a similar manner, an initial choice for UQL is made. Again return to the histogram for Q, Figure 5.2. Therein at least 90% of the population is able to produce at a quality level of 0.0 or stated oppositely, only 10% of the population is producing at a value of Q less than 0.0. This can serve as the value of Q from which the value of UQL is calculated. Use one of the formulae in Chapter 4 with the value of $Q = 0$ and calculate the value for EPAL. This will serve as the initial choice for UQL. A calculation of EPAL to find UQL will not be correct in this example for the reasons cited above. However, this situation notwithstanding, the procedure for calculating QAL and UQL is clear.

It is reminded here that this procedure provides the initial choice for AQL and UQL. It is the responsibility of the agency to determine if these values are indeed reasonable and implementable. To this end, the values of AQL and UQL should be bridged by the procedure outlined in Chapter 4 and the resulting pay factors should be applied to the lots in the data base of question. If the resulting pay factors are either too harsh or too lenient, an iterative procedure should be exercised until the appropriate values for AQL and UQL and pay factors are determined.

For the sake of demonstrating the procedure in detail, ignore the fact that the histogram of Figure 5.11 is not based on lots of same sample size. Suppose it is assumed that the number of samples per lot is 4. Additionally, assume that the 50th percentile for quality index, (Q), is around 1.25 - midway between Q equal to 1.0 and 1.5. Use Equation (4-6), Chapter 4, and calculate EPAL.

That is:

$$EPAL_q = 100(1-A) \quad \text{where}$$

$$A = \max[0, \frac{1}{2} - \frac{1}{2} * Q * (n^k / n - 1)].$$

$$\text{For } n = 4 \text{ and } Q = 1.25$$

$$A = \max [0, \frac{1}{2} - \frac{1}{2} * 1.25 * 2/3]$$

$$A = .08333 \quad \text{whereupon}$$

$$EPAL_q = 91.7 \approx 92$$

Therefore, choose AQL = 91 PAL. In a similar manner, use the value of Q from Figure 5.2 that only 10% of the population are testing below. This turns out to be $Q = .2$. Again, use Equation (4-6) to calculate EPAL. To this end,

$$A = \max [0, \frac{1}{2} - \frac{1}{2} * .2 * 2/3]$$

$$A = .41 \quad \text{whereupon}$$

$$EPAL_q = 59.$$

Therefore choose UQL = 59 PAL. These values are (practically) the same as those listed in Chapter 4 and as such, the values for the coefficients required for the quadratic expression that spans the gap between AQL and UQL will be almost the same and so will be the resulting pay factor expression for values of EPAL between $EPAL \approx 90$ and $EPAL \approx 60$. That is, the expression would turn out to be

$$\text{Pay Factor} = (-3.2120 * EPAL^2) + (6.4847 * EPAL) + (-2.2345)$$

as before. This uses a scaling factor (SF) of 0.6.

6. PAYMENT ADJUSTMENT PLAN (PAP) DISKETTE SYSTEM

6.1 Introduction

This effort is supported on an IBM-compatible floppy data disks in amounts and contents, as required to technically administer a computerized program, default files, and source program listing.

The payment formulas, defaults, payment schedules, acceptance and rejection quality limits, payment factors, and/or other items developed to collect field information are written into an IBM-compatible floppy disk(s) computer program(s) capable of accepting new information and test data to produce payment factor(s).

Hereafter, this software will be referred to as the Payment Adjustment Plan (PAP) diskette system and will consist of several individual computer programs.

This chapter describes the steps used to develop the Payment Adjustment Plan (PAP) diskette system. Throughout the text of this chapter, letters and words within square brackets, [], indicate computer keys and/or keyboard keystrokes required to be performed by the computer operator. The square brackets, [], are not to be typed as part of the required keystroke input.

6.2 Criteria for Payment Adjustment Plan (PAP) Diskette System

The Payment Adjustment Plan (PAP) diskette system has been developed to provide FAA personnel with a computer program, incorporating payment adjustment schedules/factors, for pavement test results that are below a desirable level. This PAP diskette system may be used by FAA office personnel, FAA field personnel, construction contractors, consultants/engineers, other government agencies, or others as the FAA so elects.

The criteria listed below were developed to produce this PAP diskette system.

Criteria established by definition of the effort are to be as follows:

- o Must be operable on an IBM compatible computer.
- o Must use floppy data disks.
- o Must have contents to technically administer a Payment Adjustment Plan (PAP) computerized program.

- o Must contain necessary default files.
- o The source program listing must be provided.

Criteria established by the FAA are as follows:

- o The program is to be free of proprietary rights.
- o The basic keyboard functions are to be similar to the program being written by Engineering Economics Research, Inc. (It was concluded this program was not sufficiently similar to the PAP program to warrant having similar key strokes.)
- o To provide FAA office personnel the ability to add/change formula defaults before providing the PAP disk to field personnel.
- o To allow field personnel to input new test data and calculate a payment factor based on this new test data.

Additional criteria established by the Contractor to provide a complete, easy to operate, quality program are as follows:

- o The floppy disks are to be 5-1/4 inch double-sided, double-density and operable in a computer's Drive A. This size of disk is selected because it is the most common size used on computers. Also, all IBM compatible computers will have a Drive A.
- o The program being delivered to field personnel is to be compiled or protected in such a manner as to prohibit field personnel from listing the source code, modifying the program, or changing the FAA input data/formula defaults.
- o The PAP programs are to be similar to other programs a computer operator may be familiar with.
- o The PAP program is to be "User Friendly", that is, to be operable by field personnel inexperienced in computer operation. Field personnel must have, at least, the ability to boot a computer and load DOS and the PAP program.
- o The PAP program is to be "Menu Driven", that is, progress through the program, step-by-step, providing direction to the computer operator as to his next choice or entry.
- o The PAP program is to have the [CONTROL-BREAK] key disabled, requiring field personnel to use the Menu Driven program.
- o An introduction screen is to provide a basic description of the program. This screen is to include the version date the program was issued.

- o One field disk is to contain the following:
 - Airport, Contractor and FAA project information.
 - PAP programs for five specifications.
 - FAA assigned curve defaults.
 - The ability to save data for all included specifications from six projects.
 - Printing ability of data for all specifications and projects.
- o The PAP program is to have the ability to input new data, calculate this data into a payment factor based on FAA defaults, and store/file this data and calculations for future recall and FAA use.
- o The PAP program is to have the ability to perform quick PAP calculations without saving the test data. This is for "WHAT IF" calculations.
- o The PAP program is to contain specific information, such as, the airport, the Contractor, the FAA project, and testing methods.
- o The PAP program is to contain specific test information and data, such as, lot numbers, sample locations, test dates, test results and PAP calculations.
- o The PAP program is to have the ability to print out (hard copy) test data and PAP calculations.

6.3 Development of the PAP Diskette System

Step One was to develop the P-501 PAP formula into a simple 5-1/4 inch diskette computer program, written in GWBASIC, to input new test data, calculate the sample average, sample standard deviation, estimated Q or QL, estimated PAL and the payment factor. This original program had built in PAL cut-off points and curve slope that resulted in a fixed pay factor formula. Also, this program had the ability to use only four test data entries for each lot for its calculations. No data or calculations of this original program could be saved for future usage.

The built in PAL cut-off points were set as follows:

- o Upper PAL = 90 percent (above receives 100 percent payment).

- o Lower PAL = 60 percent established at 50 percent payment (below 60 percent PAL received no payment).
- o Points between 60 and 90 percent PAL represent a quadratic curve which resulted in payment factor of between 50 to 100 percent payment.

During Step Two, the PAP program was expanded to include an introduction screen, the menu driven ability, six project data files, airport information input, data file saving and printing (hard copy) of data. This expanded program was presented for FAA review.

The FAA requested the four test samples input for each lot be changed to accept from three to six samples for each lot before performing the PAP calculations. This was included as requested.

Step Three was to develop a program that could be used by FAA office personnel to change PAL cut-off default points and the quadratic curve equation and save these default points and equation in a file named "CURVEPAP.FAA." To identify a field disk for a specific airport, the airport and FAA project description information are saved to a file named "CURVINFO.FAA."

The curve calculation program, "FAACURVE.EXE," does not have to be provided on the field PAP disk; however, files "CURVEPAP.FAA" and "CURVEINFO.FAA" are required.

Step Four was to expand the computer PAP diskette system to include several programs and files as follows:

- o A quick calculation program.
- o A curve modification program.
- o A printing (hard copy) program.
- o A start (general airport information) program.
- o Airport information files.
- o Six project files for test data (for each of the five specifications).
- o Several FAA default files.
- o Several field information files.

During this program expansion, most of the criteria previously established were included successfully.

Step Five was to rewrite these programs into a compiled version of BASIC.

The PAP programs were first rewritten in TurboBasic. A problem of disabling the [CONTROL-BREAK] key was solved; however, the separate programs compiled in .EXE & .TBC files would not "chain" from program to program. Borland International was unable to assist with solving this problem.

The PAP programs were then rewritten in QuickBASIC. The problems of disabling the [CONTROL-BREAK] key and the "chaining" from program to program were solved and overall, the programs functioned satisfactorily.

Other problems that were being encountered were also minimized and will be discussed later.

The problem of insufficient disk space for the operation of the PAP programs was solved by having the pavement test data transferred to a data storage disk in Drive B whenever the field PAP disk in Drive A became full. This process worked successfully; however, (1) Using Drive B was not in the original criteria and (2) The process may be too complex for a novice computer operator to follow.

The disk storage space problem prompted the Contractor to investigate having one PAP diskette for each different material specification. This proved to be a good choice as several separate programs could be condensed into the main program. This was due to the increased operation speed of QuickBASIC over GWBasic. QuickBASIC compiled programs operate on a machine language level, permitting faster operational speed. Combining these programs saved disk space.

Also, using QuickBASIC permitted using "tools" not permitted by GWBasic, such as eliminating line number and using "CALL-SUB" programs. These tools permitted further reducing the disk storage space required.

It was also concluded that providing the field PAP diskette in a compiled QuickBASIC program would solve the problem of computer operators having difficulty in loading the PAP program.

The problem most operators were encountering, using programs written in GWBasic, was that they would load GWBasic from their Drive C and were then unable to load the PAP program from their Drive A. A batch file program was written to solve this problem; however, when this batch file program was tested on several different computers, success was experienced only 85 percent of the time.

As previously mentioned, a program written in compiled QuickBASIC permits an easy and quick way of loading the field PAP program, because it can be loaded directly from the MS-DOS A> prompt, eliminating any need of loading a GWBasic or any other program. The steps required to load the QuickBASIC compiled field PAP program is as follows:

1. The computer must be properly installed with a monitor (preferably a color monitor) and a printer.
2. Start the computer system and boot MS-DOS, as per computer instructions.
3. Insert the FAA Payment Adjustment Plan (PAP) computer program FAA-PAP field disk into the computer's Drive A.
4. Type [A:] and press the [ENTER] key to transfer computer control to the Drive A.
5. From the A> Prompt, load the Payment Adjustment Plan (PAP) data input and pay factor calculation computer program by typing, in capital letters [FAASTART] and pressing the [ENTER] key.

A file name of "FAASTART" was chosen to assist experienced computer operators who will go directly to the computer and do a directory [DIR] of the disk and choose the most likely file to load, which normally will contain a clue in the file name such as "START."

Other criteria areas that deserve an explanation are the "User Friendly" and "Menu Driven" abilities of the PAP programs. These two items are closely associated. A "Menu Driven" program only permits the operator few and logical choices to progress, screen-by-screen, through the program. The [CONTROL-BREAK] key being disabled is vital to a "Menu Driven" program.

A "User Friendly" program is one that communicates, in an understandable language, with the computer operator. This is normally achieved by displaying several tools and statements on each screen, in an easy and understandable language, prompting the operator to take the next step, and even suggesting his next operation, choice or default.

The best and most common example of a "User Friendly" and "Menu Driven" program is the LOTUS 1-2-3 program. A computer operator familiar with programs, such as LOTUS 1-2-3, will not have any difficulty using these PAP programs.

The "User Friendly" and "Menu Driven" tools incorporated in the PAP programs are as follows:

- o Each screen has general characteristics and placements of screen tools to assist the operator during a program session.
- o Each screen of these programs displays 25 horizontal lines (left to right) with each line having up to 80 characters. A character can either be a letter, number or symbol. Vertical (up and down) characters are called columns. Many screens group words or numbers together in columns.
- o The placement of screen tools are as follows:

Lines 1 and 2: A screen title is displayed to explain the general purpose of the particular information/data required.

Lines 3 through 20: These lines are the heart of the program and are used for displaying, entering and editing information and data. The required information and data are grouped together in a logical order and each general category of required information has a number to assist the operator to select inputting/editing of information. The computer cursor is located in the active CELL. The active CELL is highlighted in reverse color and the cursor position is indicated by a blinking underline.

Line 21: This line is not used.

Lines 22 and 23: During the Response Request Mode, prompts are displayed to instruct the operator for screen approval/corrections and requests information/data required during program flow.

Line 24: Indicates current program mode the program is in. The Insert Mode is also highlighted on this line.

Line 25: Indicates the function keys the program has access to. Not all function keys are active at all times.

- o Modes of Operation:

Response Request Mode: The Response Request Mode requires an operator response. A selection request is displayed on Lines 22 and 23 of the screen. The operator must respond for the program to continue. Only the keys required to continue are active.

Input Mode: The Input Mode permits the operator to input information and data into the program and its files. When in the Input Mode, the CELL that is actively receiving the information/data is highlighted in reverse color. The TYPEWRITER

KEYBOARD, [ARROWS], [BACKSPACE], [INSERT], [ESCAPE], [DELETE], and [END] keys are active. The [LEFT and RIGHT ARROW] keys move the cursor left or right within the CELL. The [UP and DOWN ARROW] keys will [ENTER] the information into the CELL and move input/edit to the CELL before or after it, or respond with an [ENTER] and return the program to the Response Request Mode.

Calculation Mode: After necessary data has been entered into the program, the program will calculate the data and return the results and the pavement adjustment payment factor. No input keys are active during the Calculation Mode.

File Processing Mode: The File Processing Mode includes loading of additional program subroutines, transferring programs to other screen inputs, and loading and storing data/information into its files. No input keys are active during the File Processing Mode.

Printing Transfer Mode: The Printing Transfer Mode is used only to transfer information and data from the diskette files to the printer in the printing program.

During developing and testing of the PAP computer program it became apparent, when program errors were encountered, that it was necessary to have a method of communicating between the computer operator and the computer programmer.

A program subroutine was written to analyze error messages. The standard BASIC error number codes were chosen. Common program errors will be handled within the program and the computer operator will not be aware of any problem. Unusual program errors will display a message on Lines 22 and 23, which instructs the computer operator to record the message error and press any key to continue with the program. This message will list an error code number, a line number of the program, and a screen number. If the same error continues, the computer operator should notify FAA personnel with this information, so that, the problem can be resolved. See Table J-1 of Appendix J.

Several persons assisted in testing the "Menu Driven" and "User Friendly" abilities of these programs. Their computer experience ranged from that of an eleven-year-old without any computer experience, to a college graduate with extensive computer science skills. The persons without any knowledge of FAA pavement and test information, required a briefing in this area. These exercises proved quite useful in pointing out shortcomings in the programs and the Operator's Manual that had been developed. Revisions were made to accommodate these shortcomings.

6.4 QuickBASIC Programing

Computer program packages, such as QuickBASIC, have been developed to provide a method for computer programmers to write specialized programs and issue these programs to other computer operators. The FAA field PAP programs are an excellent example of where Quick BASIC compiled programs can be used.

The program writer can program within the QuickBASIC environment, similar to when using GWBasic. After the newly written program is completed and debugged from within the QuickBASIC environment, the QuickBASIC program will compile the new program into an .EXE file that can be run independently of any other program, except MS-DOS.

The compiled .EXE programs require a run module (BRUN45.EXE in this case) that is copyrighted by Microsoft Corporation. However, a registered license of a QuickBASIC program is permitted to generate these compiled .EXE programs and include the run module (BRUN45.EXE) as part of the disk that is provided to other computer operators.

The only disadvantage is that the run module, BRUN45.EXE, uses 77,000 bytes of disk space, which could be used for data storage. For additional details on the Microsoft License Agreement and usage privileges, see Appendix F.

6.5 PAP File Data Transfer to dBASE III

Previous test data collected during Task C were screened and the data that were found to be acceptable were entered into the dBASE III data files for analyzing during Task D, Development of Payment Adjustment Plans. This chapter will not review the methods used in analyzing this data or operation of the dBASE III program.

A study was conducted to make the test data entered into the PAP diskette system files transferable to dBASE III files. A program named "PAPDBASE", was written to accept a PAP data file, evaluate its data, make minor alterations to the storage sequence, and save that PAP data to another file that could be read and loaded by the dBASE III program.

After analyzing that program, it was concluded that by making minor changes in the PAP programs "FAASTART" and "FAAPRINT", PAP test data could be read directly, by a dBASE III program, and stored with the previously collected data in dBASE III files. The data would have to be evaluated using the dBASE III program.

The minor changes required in the PAP programs were: (1) Store data as ASCII characters, (2) Change the data file name extension from .DAT to .TXT, and (3) Add a carriage return and a line feed at the end of each lot. This will result in a data file that can be

retrieved by a dBASE III program.

It is recommended that future dBASE III data files follow the dBASE III data "filename" description previously used during Task C data entry. See Appendix G for example. Format should be as follows:

- o The first three or four digits of the "filename" is to be the FAA assigned airport designation, such as for Dulles International Airport being IAD.
- o The next three digits is to be the FAA assigned number of the specification, such as for P-501, Portland Cement Concrete Pavement being 501.
- o The last digit is to be a sequential designation, using alphabetical letters A through Z.

Therefore, the third project on file for P-501 at Washington Dulles International Airport would have a "filename" of "IAD501C".

The following will explain one method for transferring PAP data to a dBASE III file. The directions are for use with a computer having both A and B drives. The "filename" will refer to the newly established file name of a dBASE III file described above.

- Step 1: Insert the field PAP data diskette returned from the field with the newly added data into Drive A. Insert a newly formatted disk into Drive B.
- Step 2: From the DOS A> prompt, perform a [COPY A:*.TXT B:] and press the [Enter] key.
- Step 3: Leaving the disk in Drive B, replace the disk in Drive A with the office PAP disk.
- Step 4: From the DOS A> prompt, perform a [COPY A:MASTER.DBF B:filename.DBF] and press the [Enter] key.
- Step 5: Repeat Step 4 for each of the files to be transferred to dBASE III.
- Step 6: Insert the dBASE III system disks into Drive A and load the dBASE III operating program into the computer.
- Step 7: From the ASSIST screen/menu, position the highlight to the Setup/Database file and press the [Enter] key. This will display drive choices.
- Step 8: Position the highlight to Drive B and press the [Enter] key. This will display the name of the files currently on the selected drive.

Step 9: Position the highlight to the "filename" you wish to work with and press the [Enter] key.

Step 10: This will display the question "Is the file indexed? [Y/N]". Respond with pressing the [N] key and the [Enter] key. This will transfer dBASE III program control to the selected file.

Note the drive and the "filename" appears on the highlighted line at the bottom of the screen, as the second and third entry, respectively.

Step 11: Press the escape [ESC] key, transferring the program control to the command line, which is the fourth line from the bottom of the screen.

Step 12: From the command line, type [APPEND FROM PAP-AA.TXT SDF] and press the [Enter] key. In lieu of the file PAP-AA.TXT, you may use the name of another file as required.

This program will display the number of records that were transferred into the dBASE III files.

Step 13: From the command line, type [ASSIST] and press the [Enter] key. This will transfer program control back to the ASSIST screen/menu.

At this point, the data transferred to the dBASE III files can be viewed and edited by positioning the highlight to the Update/Browse position and pressing the [Enter] key. To view data to the right of the screen, hold down the control [CTRL] key and press the [right arrow] key.

Or, transfer additional files from the PAP files to the dBASE III files, repeat Steps 7 through 13.

Step 14: Exit dBASE III from the ASSIST screen/menu by positioning the highlight to Set Up/Quit dBASE III and pressing the [Enter] key. This will transfer computer control to MS-DOS.

Step 15: Leaving the disk in Drive B, insert the proper Task C dBASE data disk in Drive A, perform a directory [DIR/W A:] to verify there is not any duplication of file names with the newly created files, otherwise, the older files will be destroyed.

Step 16: Type [COPY B:*.DBF A:] and press [Enter] key.

This concludes one method of transferring PAP field collected data into the dBASE III data base files.

Usage and analysis of this dBASE III data is described in another chapter.

6.6 Payment Adjustment Plan (PAP) Computer Program

The Payment Adjustment Plan (PAP) diskette system was designed to provide acceptance/rejection and payment adjustment schedules for Federal Aviation Administration (FAA) airport pavement projects.

The PAP diskette system computer programs developed will function on an IBM compatible computer with MS-DOS (Disk Operating System) (Microsoft) using a 5-1/4" double-sided, double-density floppy disk. For optimum screen response, a color monitor should be used.

The PAP diskette system is to be used in Drive A of the computer hardware. Using other drives is the responsibility of the user.

There are three main PAP computer programs that make up the PAP diskette system. These programs are as follows:

- | | |
|-------------------|---|
| FAASTART.BAS/.EXE | For field personnel use. This program contains all project information and test data input, PAP formulas, calculation of the PAP, and saving input and calculations for future recall and FAA use. This program uses the PAP defaults that were established by FAA office personnel using the FAACURVE program. |
| FAAPRINT.BAS/.EXE | For producing a printout (hardcopy) of the project information, pavement test data, and the PAP calculations. |
| FAACURVE.BAS/.EXE | For use by FAA office personnel only, to change PAP defaults. This program is not required for field personnel. |

Information files that are required for successful operation of the PAP programs are as follows:

- | | |
|--------------|--|
| CURVINFO.FAA | Airport information to identify the disk with input by FAA office personnel. |
| CURVEPAP.FAA | PAP formula defaults established by FAA office personnel. |
| INFO-GEN.FAA | Airport information with input by field personnel. |
| INFO-PAP.FAA | PAP testing information with input by field personnel. |

DRIVE.MAP

The computer program uses this file to keep track of the project files.

Test data files that are generated by the computer program to save the test data for five projects are as follows:

PAP-AA.TXT
PAP-BB.TXT
PAP-CC.TXT
PAP-DD.TXT
PAP-EE.TXT

A run module required for operation of the PAP diskette system is as follows:

BRUN45.EXE

This file/program is a run module that is required for proper operation of the FAACURVE, FAASTART and FAAPRINT programs. This program is copyrighted by Microsoft Corporation and requires a statement to this effect on each disk and program introduction screen that is provided to field personnel.

These aforementioned files constitute the PAP computer diskette system. All files/programs, except FAACURVE, are required for the successful operation of the field PAP computer programs.

The field PAP computer programs can be loaded into a properly installed IBM compatible computer by: (1) Inserting the Field PAP diskette into the computer's Drive A, (2) Typing [A:] and pressing the [ENTER] key, and (3) Typing [FAASTART] and pressing the [ENTER] key.

The PAP computer programs are Menu Driven and the program flow proceeds from screen to screen throughout the program. There is one menu screen to permit selecting airport information input, printer and exiting to MS-DOS. The program flow diagram is shown in Figure 1 of the Operator's Manual, Volume II, of this report.

The program flow is as follows:

Introduction Screen: The Introduction Screen provides a brief description of the project and includes the version date of the program. Press the [Y] or [ENTER] key to continue.

General Information Screen: The General Information Screen is for Airport, Consultant, Contractor, and Test Laboratory information input.

Pavement and Project Screen: The Pavement and Project Screen requests a specific pavement material specification and a specific project name (location) within the overall construction contract

to enable the PAP program to group data into their proper category and file.

A project is defined as work being performed that must be grouped together to allow for a proper pay adjustment. The airport design consultant or engineer should indicate what constitutes a project and a project name. One contractor can be constructing several projects at once throughout the same airport. Caution must be taken to keep and enter the test laboratory results in the proper project.

Data and Information Screens: After the material specifications and project name are properly selected, the PAP program continues to the testing information screen which permits entering the Methods of Testing and the required target specification, such as for P-501 (Flex Strength), 700 psi.

After entering the Target Specifications and Methods of Testing Screen, the program continues permitting entering lot numbers, exact test location, sample/test dates and the Laboratory test results. The program will then calculate the acceptance and the pay adjustment of the entered tests.

The PAP program will save the entered airport information, testing information, pavement test date, and the pay adjustment in the program diskette files.

Menu Screen: At several points in the PAP program, selecting the [F2] function key will display the Main Menu. The Main Menu permits returning to previously displayed screens, selecting HELP screens, selecting printing of a hardcopy, selecting a QUICK CHECK screen, and exiting to MS-DOS.

Help Screen: At several points in the PAP program, selecting the [F1] function key will display several HELP screens as follows:

- HELP Screen 1, Program Flow.
- HELP Screen 2, Key Description.
- HELP Screen 3, Function Keys.

Printer Screen: Used to select files and to produce a printed hardcopy of data in the computer files. A sample of the P-501 Concrete test data printout is included herein as Appendix G.

QUICK CHECK Screen: The QUICK CHECK screen will permit an easy and quick method to input pavement test data and calculate the payment adjustment factors. This input data or the calculated payment adjustment factors will not be saved, nor can it be sent to a printer.

EXIT: EXIT will cancel the program and return the computer command to MS-DOS.

6.7 PAP Computer Program Operator's Manual

An operator's manual was written to assist persons in understanding the programs and the required inputs. Experienced computer operators may not need to refer to the manual as the PAP programs are "User Friendly" and "Menu Driven." Operators familiar with Lotus 1-2-3 will find keystrokes similar and will not have any difficulty using this program.

The PAP Computer Program Operator's Manual is published as Volume II of this report.

6.8 FAA Office Procedures

There are two levels of FAA office procedures which are as follows:

- o Generating a disk containing the field PAP computer programs from a master PAP computer program disk that contains .EXE files. Appendix J, Curve Default Program, is an Operator's Manual for this program.
- o Changing/modifying the source code of the programs and compiling these changes/modifications into a master PAP computer program disk.

The source code programs will have an extension of .BAS and the compiled master PAP computer programs will have an extension of .EXE.

The first procedure generating a field PAP disk has simple and easy steps.

A master PAP computer program disk must exist containing the following files:

FAASTART.EXE
FAAPRINT.EXE
FAACURVE.EXE
BRUN45.EXE
CURVINFO.FAA
CURVEPAP.FAA
INFO-GEN.FAA
INFO-PAP.FAA

The computer operator should do a directory [DIR] to verify these files are available on the master disk.

All files should not have any information or data stored in them except the CURVEPAP.FAA file.

To generate the field PAP computer disk, proceed as follows:

- o Insert the aforementioned master PAP computer disk into Drive A and a blank formatted disk in Drive B of an IBM compatible computer.
- o From the DOS level prompt, type [A:] and press the [ENTER] key.
- o From the A> prompt, type [DISKCOPY A: B:] and press the [ENTER] key.
- o Follow instructions from your computer.
- o Remove the master PAP computer disk from Drive A and return to storage.
- o Remove the field PAP computer disk from Drive B and insert in Drive A.
- o With the field PAP computer disk in Drive A and from the A> prompt on the screen, type [FAASTART] and press the [ENTER] key.
- o The program FAASTART will load into the computer's memory.
- o From the Introduction Screen, type [CURVE] and the program FAACURVE will automatically load into the computer's memory.
- o The FAA office computer operator can move from screen-to-screen making desired changes to the PAP defaults and airport information.
- o After all desired changes are made, the FAA office computer operator must save [S] these defaults to the proper CURVINFO.FAA and CURVEPAP.FAA files. The save process has been designed to be an easy process for the operator. After evoking the save process, the computer will do most of the work.
- o After properly saving the defaults, the operator can choose to return to the MS-DOS level or reload the FAASTART program.
- o From the MS-DOS level A> prompt, type [DEL FAACURVE.EXE] and press the [ENTER] key. This step removes the curve default program FAACURVE from the field PAP disk. If deleting this program is neglected, field personnel will still be unable to load this program into the computer's memory without knowing the password. If the FAA office personnel wants to modify the defaults after deleting the FAACURVE program, a [COPY FAACURVE.EXE A: B:] of the file FAACURVE.EXE from the master disk, it is recommended that the file be removed from the

disk, since this allows more disk storage space for data.

- o Label the field PAP disk with the following information:
 - Field PAP Calculation Program.
 - For (airport and city/state).
 - Date: (Use date field program was made).
 - Portions (c) 1982-1988 Microsoft Corporation. All Rights Reserved.
 - Enter FAASTART to run program.
- o If a record/backup of the field PAP disk issued is desired, generate a [DISKCOPY] as described above. Label the record/backup copy and store.

The above listed steps do not require FAA office personnel to work within the QuickBASIC environment; however, a field PAP computer program disk can be made from within the QuickBASIC environment.

The other procedure, changing/modifying the source code, requires a knowledge of programming in a BASIC language and familiarity of the QuickBASIC programming tools. The FAA computer program source code is written in a BASIC language, has a file extension of .BAS, saved in a ASCII format, and can best be changed/modified within the QuickBASIC environment.

The advantages of programming within a QuickBASIC environment and utilizing the many QuickBASIC tools are too numerous to list within this report. These advantages and tools can be studied in the texts: "Microsoft QuickBASIC Programming in BASIC" and "Microsoft QuickBASIC Learning to Use Microsoft QuickBASIC."

Programs written within the QuickBASIC environment uses all the commands available in BASIC, plus additional commands that simplify and improve programming. When the program is completed, run and debugged, the QuickBASIC environment will generate a compiled .EXE program from the source code .BAS program. This compiled .EXE program can then be run without requiring any other program, except MS-DOS.

Programming within the QuickBASIC environment can be done on a computer without a fixed Drive C; however, because the QuickBASIC program package contains five disks, programming speed is increased if the computer Drive C is used.

6.9 Recommendations

The advantages of providing the field PAP diskette system in QuickBASIC compiled programs are as follows:

- o Simplicity of loading the FAA field PAP computer programs.
- o A QuickBASIC compiled program is more compatible with an "IBM compatible computer," than a program written in Basic, Basica, or GWBasic.
- o The [CONTROL-BREAK] key is disabled permitting "Menu Driven" programs.
- o A field based computer operator cannot make a listing of the source code of the programs or change/modify the program.
- o Another program, such as Basic, Basica, or GWBasic, is not required for the PAP programs to operate. The work normally performed by a BASIC program will be done by the run modules BRUN45.EXE, which is included on the field disk.
- o Line numbers are not required when writing programs in QuickBASIC. This saves disk space and time.
- o The calculation and processing speed is greatly increased over a GWBasic written program; because compiled programs operate on a machine language level.
- o There are many programming tools QuickBASIC has that are not available in GWBasic. These tools are detailed in the QuickBASIC manuals.

The disadvantages of programming in a QuickBASIC compiled program are as follows:

- o The run module, BRUN45.EXE, uses 77,000 bytes of disk space, which could be used for data storage.
- o A statement "Portions (C) 1982-1988 MICROSOFT Corporation. All rights reserved" must appear on (1) the disk label and (2) the program's first introduction screen. This is to be in accordance with the license agreement of MICROSOFT Corporation.

Comparing the advantages and disadvantages of programming in a QuickBASIC compiled program, it is the Contractor's recommendation that the FAA field PAP programs be provided to field personnel in a compiled QuickBASIC version.

7. RANK AND SELECT THREE AIRPORT PAVEMENT PROJECTS

7.1 General

The study required testing of the pavement adjustment system developed during Task F with pavement test data from three airports having applicable new pavement construction. This chapter explains the process used for the selection of the three airports.

7.2 Development of Airport Pavement Construction Project Criteria

Criteria were established to assist in the selection of the best applicable airport projects for testing the payment adjustment system during Task F. The criteria used for selecting the airport construction projects are as follows:

- o The airport should be located in the FAA Eastern Region.
- o Airports should have as many of the required five specifications as possible.
- o The construction project should comply with the latest FAA specification.
- o Each project must have at least 20 test points.
- o The contractor must be a "Competent Contractor".
- o Density tests must be performed by the sand-cone method.
- o P-501 Concrete to be tested by the flexural strength beam testing method.

7.3 Selection of Three Airport Construction Projects

Meetings with airport managers, consultants, and engineers during the Task C, Data Collection phase, did not generate a positive list of airports that were having applicable pavement construction for the 1988 and 1989 seasons. Consequently, a list of airports having construction projects was generated from FAA records. Investigation of these airports revealed that few were having pavement type construction of the required specifications. Further pursuit of applicable data from the airports noted on this list was discontinued.

A meeting with personnel of the FAA Eastern Region's Falls Church District office indicated very little airport construction was being performed during the 1988 and 1989 seasons on the applicable specifications except P-152, Excavation and Embankment. The

parties agreed to provide pavement test data from the Dulles International Airport, Washington D.C., as the data become available. Expected data were for P-152, P-209, and P-501.

Meetings were conducted with other airport managers and consultants that were anticipating pavement construction, with only one consultant positively having applicable airport construction during the 1988 and 1989 season. This consultant was R. Kenneth Weeks, Engineers, of Norfolk, VA. The project was for a Terminal Apron expansion at the Norfolk International Airport, Norfolk, VA, using P-501 Concrete pavement.

Personnel from the Greater Pittsburgh International Airport, Pittsburgh, PA were contacted for possible projects. The airport personnel referred the Contractor to the airports Construction Manager, Mellon Stuart Company, Dick Enterprises. The Mellon Stuart Company, Dick Enterprises indicated there was a Midfield Terminal project at the Greater Pittsburgh International Airport, Pittsburgh, PA being constructed and they would provide pavement test data for Items P-152, Excavation and Embankment and P-501, Portland Cement Concrete Pavement.

The Greiner Engineering Services, Inc., Baltimore, MD provided P-501, Portland Cement Concrete Pavement test data for the Baltimore/Washington International Airport, Baltimore, MD for a Pier D/Y Headstand project. The test data were received too late to be used by the Contractor during Task F, Analyzing of Collected Data.

A meeting was held with representatives of the National Ready Mixed Concrete Association and the American Concrete Pavement Association. They indicated that they did not have P-501 Concrete test data from the FAA Eastern Region. However, they did have, and offered to provide, P-501 Concrete test data from the Wichita Mid-Continent Airport, Wichita, Kansas for review and use.

As a result of Task C, Data Collection interviews between the Contractors' personnel and FAA field personnel, airport personnel, and consulting engineers, it was apparent that most engineering monitors preferred a construction contractor to continue to rework compactible type material until a "pass" was obtained from the "pass/fail" tests, rather than offer a payment adjustment for the section for which the tests failed. This situation was consistent with that discovered by the FAA Operation personnel in interviews with pavement industry personnel and field engineers.

Pavement materials currently under density testing consideration are as follows:

- P-152, Excavation and Embankment, Density.
- P-209, Crushed Aggregate Base Course, Density.
- P-304, Concrete Treated Base Course, Density.
- P-306, Econocrete Subbase Course, Density.

The Contractor did not review and has not made recommendations for any other density testing materials beyond the four aforementioned materials.

The Contractor was unable to locate any airport pavement projects in the FAA Eastern Region being constructed using P-306, Econocrete Subbase Course, for the 1988 and 1989 seasons.

Based on the above listed recommendations, the only material specification to require testing of the developed methodology, formulation and diskette system was P-501, Portland Cement Concrete Pavement (flexural strength). Of the above listed five airports, the three that received the highest rating for the previously established criteria were as follows:

1. Greater Pittsburgh International Airport, Pittsburgh, PA.
2. Norfolk International Airport, Norfolk, VA.
3. Dulles International Airport, Washington D.C.

The FAA approved using these three airports as the P-501 Concrete projects for field testing of the newly developed PAP system.

8. FIELD EVALUATION OF AIRPORT PAVEMENT CONSTRUCTION PROJECTS

8.1 General

To verify the payment adjustment (PAP) system developed, the PAP system was tested with three airport pavement construction projects. This chapter explains the airport pavement construction projects used for this process.

As indicated in Chapter 2, the only material specification that was to be monitored during Task F was P-501, Portland Cement Concrete Pavement.

During the development of the payment adjustment methodology, system analysis of data and development of the PAP formulation, Task D, frequent panel discussions were held concerning quality control. The objective of payment adjustment quality control is to encourage maintaining and improving on a good quality of materials, and if below an acceptable quality limit (AQL), to offer an adjusted payment, dependent on lower quality, until an Unacceptable Quality (UQL) is reached. It is at this Unacceptable Quality (UQL) point that the material is rejected.

8.2 Airport Pavement Construction Test Data Used for Verification

The three airport pavement projects listed in Chapter 7, Greater Pittsburgh, Norfolk, and Dulles, were the primary projects that were considered; however, two additional airport pavement projects (Baltimore/Washington and Wichita Mid-Continent) were also reviewed.

The original P-501 Concrete flexural strength test data (approximately 50 Lots) received for Norfolk International Airport was used by the computer programmer during the development of the PAP computer program system, Task D. The remainder of the Norfolk test data and the other four projects were used at various times to verify and debug the PAP computer program system.

Details of the P-501 Concrete test data received and the payment adjustment results are as follows:

1. Greater Pittsburgh International Airport, Pittsburgh, PA

The pavement test data were provided by the Mellon Stuart Company, Dick Enterprises and are of a Midfield Terminal project constructed in 1989. The material specification was for P-501, Portland Cement Concrete Pavement (flexural strength).

Flexural strength tests were conducted by Mellon Stuart Company, Dick Enterprises. Their record keeping and test result data sheets were excellent.

Sufficient testing of the concrete was performed each day to facilitate grouping tests into lots of 28-day tests. This resulted in 113 lots.

The design target was established at 750 PSI for the flexural strength beam tests. Basing the PAP formula defaults of AQL equal to 90 percent, UQL equal to 60 percent and a scaling factor of 0.6, the payment schedule results for each lot are shown in Appendix J.

Analysis of these results is as follows:

- o Data entry personnel did not experience any problems with the information/data entry ability of the computer program.
- o All data for the 113 lots of the P-501 Concrete for the Pittsburgh project were analyzed with the computer program, and provided satisfactory results without difficulty. Pay factors produced were within expected projections.

2. Norfolk International Airport, Norfolk, Virginia

The pavement test data were provided by R. Kenneth Weeks, Engineers of Norfolk, Virginia and are of a Terminal Apron Expansion, constructed in late 1987 and 1988. The material specification was for P-501, Portland Cement Concrete Pavement (flexural strength).

Flexural strength tests were conducted by ATEC Associates of Virginia, Inc. of Norfolk, Virginia. Their record keeping and data sheets were very good. As they had required only two passing beam tests for each lot, the data was entered into the PAP computer programs in two arrangements and under different project files. The first entry was by lots, as originally designated, using both 14-day and 28-day tests. It should be noted, some lots (17, 18, 19, 20, and 31) had only 14-day tests performed on the flexural strength beams. This resulted in 99 lots and is shown in Appendix K. The second entry combined reasonable tests on the same day, to form new lots of 28-days only. This resulted in 44 lots and is shown in Appendix L.

The design target was established at 700 PSI for flexural strength beam tests. Basing the PAP formula defaults of AQL equal to 90 percent, UQL equal to 60 percent, and a scaling factor of 0.6, the payment schedule results for each lot are shown in Appendix K and L.

Analysis of these results is follows:

- o The first series of test data received were used to assist the computer programmer during the writing of the program. The remainder permitted the computer programmer to verify and debug the program. This provided vital hands-on experience for the computer programmer to evaluate and incorporate typical test data and information that are expected to be available during pavement construction. As would be expected during the debugging of any new computer program, considerable problems were encountered; however, all problems were isolated and the program was corrected, so as to avoid similar problems in the future.
- o The later data entry of the 28-day tests only resulted in few problems with the computer program.
- o During the transfer of the data from the PAP files to dBase III files, there was a problem encountered with the lots that followed those lots that did not have any data assigned to them. The problem was isolated and corrected.
- o All data for the 44 (28-day) lots of the P-501 Concrete for the Norfolk project were analyzed with the computer program and provided satisfactory results without difficulty. Pay factors produced were within expected projections.

3. Dulles International Airport, Washington D.C.

Pavement test data were provided by the FAA Falls Church District of Falls Church, Virginia and are for a Runway No. 30 Concrete Pavement at Dulles International Airport. This construction was between June 1988 and October 1988. The material specification was for P-501, Portland Cement Concrete Pavement (flexural strength).

Flexural strength tests were conducted by ATEC Associates of Virginia, Inc. of Chantilly, Virginia.

As they had required only two passing tests at either 14 days or 28 days, most were accepted at 14-days; therefore, data would enter into the PAP computer program in two arrangements in different files. The first entry was by lots, as originally designated, using the latest four tests of 7-day, 14-day, or 28-day tests. This resulted in 51 lots and is shown in Appendix M. The second data entry was by combining reasonable tests on the same day into new lots of the best four tests from two lots. This resulted in 25 lots and is shown in Appendix N.

The design target was established as 650 PSI for the flexural strength beam tests by the airport design engineers. Basing the PAP formula defaults as AQL equal to 90 percent, UQL equal to 60 percent, and a scaling factor of 0.6, the payment schedule results for each lot are shown in Appendices M and N.

Analysis of these results is as follows:

- o Few data entry problems were encountered as the program was already debugged. Any problems encountered were isolated and corrected.
- o A problem was encountered while transferring data from the PAP data files to the dBase III files. This problem could not be solved, so the data were reentered into the PAP program under another project file. The data base was correctly transferred from the PAP data files into the dBase III files.
- o All data for the 25 lots of the P-501 Concrete for the Dulles project were analyzed with the computer program, and provided satisfactory results without difficulty. Pay factors produced were within expected projections.

The above three airport projects were selected for testing of the payment adjustment system. P-501 Concrete test data from two additional airport projects were available and were tested. Results are as follows:

4. Baltimore/Washington International, Baltimore, Maryland

Pavement test data were provided by the Greiner Engineering Services, Inc. of Baltimore, Maryland and were for a Pier D/Y Headstand concrete pavement. This construction occurred between August and November of 1987. The material specification was for P-501, Portland Cement Concrete Pavement (flexural strength).

Flexural strength tests were conducted by Penniman and Browne, Inc. of Baltimore, Maryland. Their data sheets are a combination of flexural strength test results and core thickness test results.

Most lots had at least three flexural strength tests. In the cases when only one or two were performed, the tests were combined with an adjacent day's lots and entered into the PAP computer files. This was for Lots 1, 11 and 17. This resulted in the data entry of 20 lots and is shown in Appendix O.

The design target was established at 700 PSI for flexural strength beam tests. By using the PAP formula defaults of AQL equal to 90 percent, UQL equal to 60 percent, and a scaling factor of 0.6, the payment schedule results for each lot are shown in Appendix O.

Analysis of these results is as follows:

- o There were no major problems encountered during the data entry with the FAA computer program, or when transferring this data to the dBase III files.
- o All data for the 20 lots of the P-501 Concrete for the Baltimore/Washington International project were analyzed with the computer program and provided satisfactory results without difficulty. Pay factors produced were within expected projections.

5. Wichita Mid-Continent Airport, Wichita, Kansas

The pavement test data were provided by the National Ready Mixed Concrete Association/National Aggregates Association of Silver Spring, Maryland, and are for a Runway 1L-19R reconstruction concrete pavement project. This construction was between July and October 1987. The material specification was for P-501, Portland Cement Concrete Pavement (flexural strength).

Flexural strength tests were conducted by Professional Engineering Consultants, Wichita, Kansas. During pavement construction, a comparison test was conducted between flexural strength, compressive strength, and splitting tensile strength tests. 28-day flexural strength tests were performed in groups, either four or eight tests per lot. For entering this data into the PAP computer program, the lots having eight tests were divided into two lots of four consecutive tests each. This resulted in 65 lots.

The design target was established by the airport design engineer at 650 PSI for the flexural strength beam tests. Basing the PAP formula defaults on AQL equal to 90 percent, UQL equal to 60 percent, and a scaling factor of 0.6, the payment schedule results for each lot are shown in Appendix P.

This project is included for informational purposes. It cannot be reviewed in conjunction with the data from the FAA Eastern Region, as the projects utilized in this study must all be from the same FAA region.

Analysis of these results is as follows:

- o There was no major problems encountered during the data entry with the FAA computer program, or when transferring this data to the dBase III files.
- o All data for the 65 lots of the P-501 Concrete for the Wichita Mid-Continent project were analyzed with the computer program, and provided satisfactory results without difficulty. Pay factors produced were within expected projections.

9. RESULTS OF APPLYING PAYMENT ADJUSTMENT PLAN TO AIRPORT CONSTRUCTION PROJECTS

9.1 Preliminary Remarks

As discussed in Chapter 8, data from airport construction projects were used to verify the payment adjustment plan that was developed during Task D. The rationale for choice of values for AQL and UQL was also previously discussed in Chapter 5, and emphasis was placed on the fact that those values were based on historical data for the construction items of interest, which in this effort was P-501 Concrete flexural strength. The historical data were obtained from airport projects that dated from 1974 through 1986. What will be discussed in this chapter are the results that occurred from applying the PAP to recent airport construction projects, that included P-501 Concrete as one of the construction materials.

9.2 Application of the PAP to Recent Airport Construction Projects

9.2.1 Greater Pittsburgh International Airport

Data from this project for P-501 Concrete flexural strength involved the time period from August through December 1989. As pointed out in Chapter 8, these data resulted in one hundred thirteen (113) lots that were subjected to the PAP. The PAP was based on AQL, UQL, scale factor (SF), and minimum pay values of 90%, 60%, 0.60, and 50%, respectively. This means that all values of $EPAL \geq 90\%$ received full pay; values of $EPAL = 60\%$ received 50% of full pay; all values of $EPAL < 60\%$ received zero pay; and all values of $EPAL$ for which $60\% < EPAL < 90\%$ received an adjusted pay according to the form

$$PAY\ FACTOR = -3.21*EPAL^2 + 6.48*EPAL - 2.234$$

This is the same expression that was developed in Chapter 4 and justified in Chapter 5.

The values of adjusted pay for the 113 lots are listed in Appendix J. From that listing, 60 lots received full pay; 21 lots received between 99% and 90% of full pay; 13 lots received between 89% and 80% of full pay; 5 lots received between 79% and 70% of full pay; 8 lots received between 69% and 50% of full pay, and 6 lots received zero pay, the minimum.

If these data are subjected to the pay factor that is currently in use by FAA for P-501 Concrete (see Chapter 4), an entirely different and much more lenient pay factor results. All lots except those whose $EPAL$ is less than 60% would receive full pay. This translates to 107 lots receiving full pay, 3 lots receiving

between 99% and 90% of full pay and 3 lots receiving between 89% and 80% of full pay. The reason for this is obvious from Figure 9.1, wherein the graphical representation of pay factor versus EPAL is shown. Both curves in Figure 9.1 were taken from Chapter 4. In Figure 9.1, the curve representing the pay factor that resulted from the current work provides for zero pay at the same point (EPAL = 60%), wherein the pay factor from the currently FAA used adjustment curve begins to decrease from full pay.

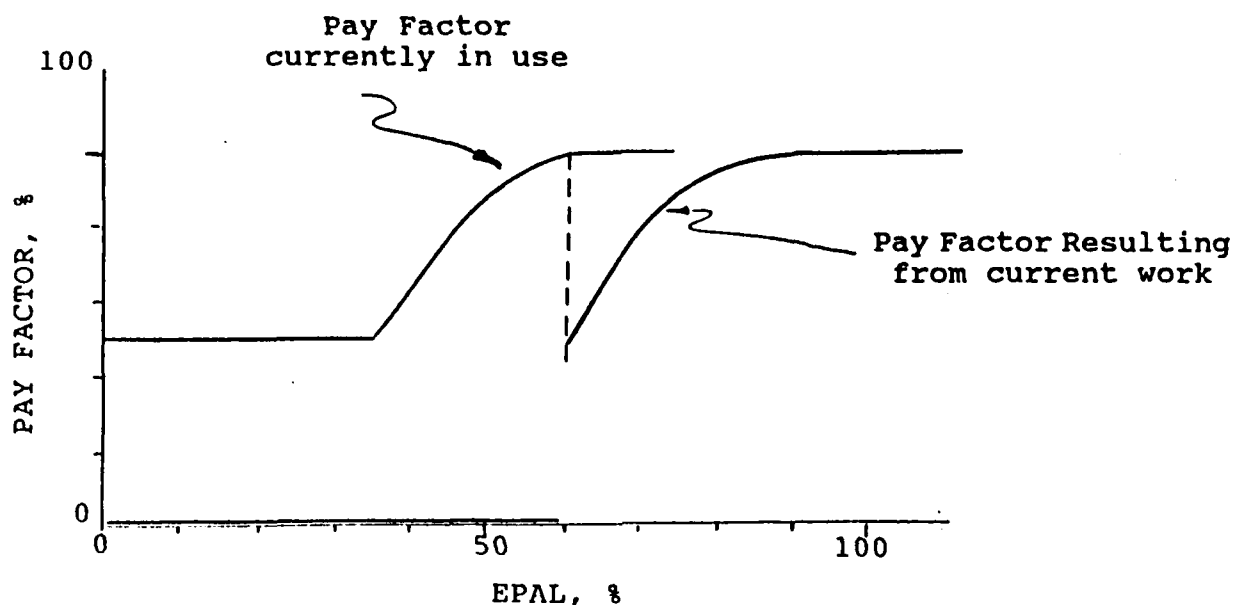


FIGURE 9.1 EPAL VS. PAY FACTOR

An interesting facet associated with the pay factor that resulted from this current work is the influence that the standard deviation (S) has on the pay factor for a particular lot. Look at the listing in Appendix D and specifically at the results for lots 5 and 6. Recall that the lower specification limit for flexural strength for this project was 750 psi. Lot 5 has an average value for stress = 763 psi, an EPAL = .82 and a pay factor of about 92%. Lot 6 has an average value for stress = 760, only 3 psi different from the value of stress for lot 5. However, the pay factor for lot 6 is zero (since EPAL = .56 which is <.60, the limiting value for pay factor different from zero).

The difference between pay factors for lots 5 and 6 lies in the difference in standard deviation for the two lots. Note for lot 5, $S = 13.3$, while for lot 6, $S = 54.7$. Standard deviation is a good measure of the spread or variation from the mean value that the values from the sample possess. Note from the members of the sample from lot 5, that the maximum difference between individual

values for stress and the average sample value is 23 psi. The sample values for stress in lot 5 are tightly nested about the mean value. Just the opposite is true for the values of stress from the samples for lot 6. Thus, S is a good measure of test result variability and plays a strong role in estimating the impact of this variability on the pay factor. Large variability in quality should be penalized and the formulation from this work provides for that aspect. A cursory look through the remaining elements in the listing of Appendix J supports this finding.

9.2.2 Norfolk International Airport

Data for this project for P-501 Concrete flexural strength involved the time period from November 1987 to October 1988. As noted previously, an arrangement of this data provided for forty-five lots to be subjected to the pay adjustment scheme (see Chapter 8). For consistency with the previous work, the PAP was based on AQL = 90%, UQL = 60%, SF = .60, and pay (at EPAL = 60%) = 50%.

This is the same as before, that is,

Pay factor = 1.00 for EPAL \geq 90%

Pay factor = 0.50 for EPAL = 60%

Pay factor = 0 for EPAL < 60%

and Pay factor (for 60% < EPAL < 90%) is calculated according to

$$\text{PAY FACTOR} = -3.21 \cdot \text{EPAL}^2 + 6.48 \cdot \text{EPAL} - 2.234$$

The values for pay factor for the 45 lots from the Norfolk project are listed in Appendix L. Therein all lots except four received full pay. Three of those four lots received pay factors between 90% to 95% of full pay and the remaining lot received 89% of full pay. The reason for the lack of significant reductions in pay factor is due to the fact that the lower specification value for flexural stress was 700 psi for this project (compared to a specification value of 750 psi for the Pittsburgh project). This, and also the sample average stress values were not only appreciably above the specification value of 700 psi, but generally the standard deviation values were not large compared to the level of lot average value of stress.

9.2.3 Dulles International Airport

Data for the Dulles project were received and manipulated, as discussed in Chapter 8, to provide data for 25 lots. These data were obtained from tests conducted during the July to September 1988 timeframe. Again, the same values for AQL, UQL, SF, and minimum pay were used in the model for pay factors as used for estimating pay factors for the Pittsburgh and Norfolk projects.

The values for pay factor for the 25 lots (as arranged per the discussion in Chapter 8) for the Dulles project are listed in Appendix N. From the listing in Appendix N, all lots received full pay. Simply stated, all average values for flexural stress for the 25 lots were well above the lower specification value of 650 psi. In fact, there were no values of flexural stress from the individual sample values less than the 650 psi lower limit. Thus, it would be difficult to generate a pay factor less than one unless a large variation in stress values occurred within a lot which is measured by the standard deviation.

Also, as mentioned in Chapter 8, data were made available from two additional airport projects, Wichita and Baltimore/Washington. As such, these two projects were subjected to the pay adjustment model and, therefore, these results will also be discussed.

9.2.4 Baltimore/Washington International Airport

Data for this project resulted from tests conducted during the August to November 1987 time period. The data were arranged per the discussion in Chapter 8 and resulted in 20 lots for analysis. The same values for AQL, UQL, SF and minimum pay as used before were used in the estimation for pay factor for this project. The values for pay factor are listed in Appendix O.

Therein, 18 of 20 lots received full pay and the remaining two lots received pay factors of 98% and 88% of full pay. The 88% of full pay (lot 15) value was due to the relatively large value (95 psi) of standard deviation relative to the average value (783 psi) of flexural stress for this lot.

9.2.5 Wichita Mid-Continent Airport

Although this data can not be judged/reviewed in reality, according to data from the FAA Eastern Region, nonetheless it was subjected to the pay factor model. Data were available for the time period covering July 1987 through October 1987. Sixty-five (65) lots resulted from the flexural strength tests conducted during this time period and are listed in Appendix P.

The same parametric values were used to estimate pay factors for the 65 lots of this project, as were used in the previous projects. That is, AQL = 90%, UQL = 60%, SF = .60 and minimum pay (@EPAL = 60%) = 50%.

The results of subjecting the data from this project to the pay adjustment factor model are also listed in Appendix P. Therein, 55 lots received full pay; 2 lots received between 99% and 90% of full pay; 3 lots received between 89% and 80% of full pay; 1 lot received 73% of full pay; 1 lot received 57% of full pay; and 3

lots received no pay. The lower specification value for flexural stress for this project was 650 psi.

In Subsection 9.2.1, reference was made to the fact that the pay factor that results from the work of this program is more stringent than that currently in use by the FAA. However, it must be kept in mind that the central point of this project is to determine if the method generally employed in determining pay factors for P-401 Asphalt is applicable to other airport construction materials. That point has definitely been proven to be true. Additionally, a rational approach was needed for choice of the parametric values in the pay factor model.

The approach taken in this project was based on actual data taken from the field for the particular construction item of interest. As such, the resulting pay adjustment model reflects in reality what industry is able to achieve, quality wise, without undue hardship or expense. Therefore, if the resulting pay factor model appears to be more stringent than that currently in use by the FAA, then this difference should be couched in the context of an attempt to improve the overall quality of the end item product (P-501 Concrete), but under the conditions that this is what the industry is able to achieve in a reasonable manner.

In order to bring this issue into perspective, the results from applying the pay factor model to the five projects discussed in this chapter have been lumped together and are listed in Table 9.1.

TABLE 9.1
DISTRIBUTION OF PAY FACTORS FOR FIVE AIRPORT PROJECTS

| Project | Pay Factor, % | | | | | | TOTAL |
|---------|---------------|----------|----------|----------|----------|----------|-----------|
| | 100 | 99-90 | 89-80 | 79-70 | 69-50 | 0 | |
| Pitt | 60 | 21 | 13 | 5 | 8 | 6 | 113 |
| Norfolk | 41 | 3 | 1 | - | - | - | 45 |
| Dulles | 25 | - | - | - | - | - | 25 |
| BWI | 18 | 1 | 1 | - | - | - | 20 |
| Wichita | <u>55</u> | <u>2</u> | <u>3</u> | <u>1</u> | <u>1</u> | <u>3</u> | <u>65</u> |
| TOTALS | 199 | 27 | 18 | 6 | 9 | 9 | 268 |

Therein, altogether 268 lots were examined by the pay factor model and 199 of these lots (or 74% of the total number of lots for these five projects) received 100% of full pay. Twenty-seven lots received between 99% and 90% of full pay; eighteen lots received between 89% and 80% of full pay; six lots received between 79% and 70% of full pay; nine lots received between 69% and 50% of full pay and only nine lots received no pay. This says that over 93% of all the lots received at least 70% of full pay, and only about 3%

received no pay. It should also be noted here that these values could be improved to a better level, by a tighter control over product variability, herein measured by standard deviation.

As was seen in an earlier discussion, reduction in the standard deviation for the samples in a lot can have a dramatic effect on estimated quality and, subsequently, on estimated pay factor. But this is precisely the point regarding an attempt at product quality improvement. Reduce product variability and improve product quality. Reduction in standard deviation per sample is the key to quality improvement and is the statistical monitor of quality for this model.

10. ADAPTATION OF PAYMENT ADJUSTMENT PLAN TO OTHER MATERIALS

10.1 Application of Methodology to Other Materials in General

In Chapter 4, (Subsections 4.3.3 through 4.3.7) the applicability of the methodology to other material specifications P-152, Excavation and Embankment, Density; P-209, Crushed Aggregate Base Course, Density; P-304, Cement Treated Base Course, Density; P-306, Econocrete Subbase Course, Density; and P-501, Portland Cement Concrete Pavement, Thickness was discussed. For the reasons stated therein, the applicability of the methodology to these specific construction items was deemed inappropriate. However, since the current FAA specification for P-306 Econocrete involves pay adjustment based on thickness with limitations placed on slump, air content and compressive strength and since compressive strength for P-306 Econocrete is monitored in almost the same manner as that for P-501 Concrete flexural strength, a pay factor for P-306 Econocrete, based on compressive strength, could be accomplished. What follows in the next subsections are the results of applying the methodology to this item.

10.2 Application of Methodology to P-306 Econocrete Compressive Strength

Data for P-306, Econocrete Subbase Course (compressive strength) were received from two project sites, Pittsburgh International Airport and Harrisburg International Airport. The time period for which test data were taken spanned from July 1986 through September 1986 for the Pittsburgh Airport and from November 1983 up to May 1986 for the Harrisburg Airport. The data were screened for admissible lots under the restrictions that the reported values for compressive strength were from 28-day cure batches and a minimum of 3 samples per lot. This screening criteria resulted in 19 admissible lots from the Pittsburgh Airport and 26 admissible lots from the Harrisburg Airport for a total of 45 lots. These lots are listed in Table 10.1.

TABLE 10.1
DETERMINATION OF AQL AND UQL USING P-306 DATA
Performed on lots of 28-day strength
Lots with ≥ 3 samples

| OBS | TESTDATE | LOT_NO | N_STR | MEAN_STR | STD_STR | Q_STR |
|-----|----------|---------|-------|----------|---------|---------|
| 1 | 19860509 | MDT306A | 3 | 753.33 | 11.547 | 0.2887 |
| 2 | 19860408 | MDT306A | 6 | 881.67 | 73.052 | 1.8024 |
| 3 | 19860410 | MDT306A | 6 | 888.33 | 24.014 | 5.7606 |
| 4 | 19860401 | MDT306A | 3 | 893.33 | 23.094 | 6.2065 |
| 5 | 19860728 | PIT306A | 4 | 946.25 | 114.150 | 1.7192 |
| 6 | 19860730 | PIT306A | 4 | 968.00 | 192.227 | 1.1341 |
| 7 | 19860402 | MDT306A | 3 | 976.67 | 11.547 | 19.6299 |
| 8 | 19860729 | PIT306A | 4 | 977.00 | 39.387 | 5.7633 |
| 9 | 19860409 | MDT306A | 6 | 993.33 | 150.953 | 1.6120 |
| 10 | 19860425 | MDT306A | 3 | 1010.00 | 20.000 | 13.0000 |
| 11 | 19860328 | MDT306A | 3 | 1026.67 | 35.119 | 7.8780 |
| 12 | 19860331 | MDT306A | 3 | 1026.67 | 15.275 | 18.1121 |
| 13 | 19860827 | PIT306A | 4 | 1039.00 | 72.778 | 3.9710 |
| 14 | 19860912 | PIT306A | 4 | 1078.75 | 114.596 | 2.8688 |
| 15 | 19860725 | PIT306A | 4 | 1083.50 | 199.321 | 1.6732 |
| 16 | 19860415 | MDT306A | 3 | 1085.00 | 8.660 | 38.6825 |
| 17 | 19860421 | MDT306A | 6 | 1088.33 | 359.968 | 0.9399 |
| 18 | 19860404 | MDT306D | 4 | 1092.25 | 169.683 | 2.0170 |
| 19 | 19860828 | PIT306A | 3 | 1126.00 | 87.069 | 4.3184 |
| 20 | 19860807 | PIT306A | 4 | 1154.00 | 120.036 | 3.3657 |
| 21 | 19860411 | MDT306A | 3 | 1163.33 | 11.547 | 35.7957 |
| 22 | 19860403 | MDT306A | 3 | 1170.00 | 20.000 | 21.0000 |
| 23 | 19860804 | PIT306A | 4 | 1171.50 | 181.118 | 2.3272 |
| 24 | 19860407 | MDT306A | 6 | 1173.33 | 237.795 | 1.7802 |
| 25 | 19860911 | PIT306A | 4 | 1180.25 | 46.421 | 9.2684 |
| 26 | 19860404 | MDT306A | 6 | 1186.67 | 79.162 | 5.5161 |
| 27 | 19860910 | PIT306A | 4 | 1246.75 | 41.939 | 11.8445 |
| 28 | 19860714 | PIT306A | 4 | 1255.75 | 72.016 | 7.0228 |
| 29 | 19860908 | PIT306A | 4 | 1291.00 | 38.114 | 14.1943 |
| 30 | 19831122 | MDT306C | 4 | 1300.50 | 490.745 | 1.1218 |
| 31 | 19860326 | MDT306A | 3 | 1320.00 | 36.056 | 15.8090 |
| 32 | 19860424 | MDT306A | 3 | 1326.67 | 15.275 | 37.7517 |
| 33 | 19860718 | PIT306A | 4 | 1339.50 | 201.875 | 2.9201 |
| 34 | 19860701 | PIT306A | 4 | 1410.50 | 199.862 | 3.3048 |
| 35 | 19851211 | MDT306D | 4 | 1419.50 | 128.648 | 5.2041 |
| 36 | 19851210 | MDT306D | 4 | 1432.75 | 51.745 | 13.1944 |
| 37 | 19831116 | MDT306C | 4 | 1458.75 | 89.712 | 7.9003 |
| 38 | 19860707 | PIT306A | 4 | 1490.00 | 106.464 | 6.9507 |
| 39 | 19860723 | PIT306A | 4 | 1494.50 | 144.975 | 5.1354 |
| 40 | 19860702 | PIT306A | 4 | 1498.50 | 311.279 | 2.4046 |
| 41 | 19831115 | MDT306C | 4 | 1733.00 | 128.898 | 7.6262 |
| 42 | 19831118 | MDT306C | 4 | 1741.75 | 116.903 | 8.4835 |
| 43 | 19860719 | PIT306A | 4 | 1750.50 | 442.180 | 2.2627 |
| 44 | 19831121 | MDT306C | 4 | 1777.50 | 139.115 | 7.3860 |
| 45 | 19831117 | MDT306C | 4 | 2020.25 | 22.187 | 57.2527 |

10.2.1 PAP When Only the Lower Limit for Compressive Strength is Specified

The lower target value for compressive strength for P-306 Econocrete was 750 psi for each of the 45 lots. There was no upper limit (apparently) specified for the compressive strength for these lots. From the listing in Table 10.1, there is only one value for compressive strength that would possibly not receive full pay, if only the lower limit of 750 psi is required for acceptance of this material item. That value is from the Harrisburg International Airport and the test date was May 9, 1986 for three samples whose average value for compressive strength was 753.3 psi, with a standard deviation of 14 and Quality Index $Q = .289$.

Further calculations show EPAL = 58% for this lot. Use of the technique outlined in Chapter 5 for choice of AQL and UQL emphasizes the ability of the remaining 44 lots from these two projects to each receive almost full pay.

However, this technique must be applied within all the elements of the specification for the material item. These items include the fact that average value of 28-day compressive strength needs to be at least 750 psi, and no more than 20% of the specimens tested have a strength value less than 750 psi. Thus, if the suggested method for choices of AQL and UQL, as outlined in Chapter 5, are followed blindly, the 50th percentile choice for AQL (based on a mean value of compressive strength = 117 psi, the 50th percentile) would result in $Q = 5.7$ (see Table 10.2), which corresponds to a EPAL = 100%. On the other hand, the 10th percentile choice for UQL (based on the 10th percentile mean value of compressive strength = 946.25 psi) would result in $Q = 1.6$ (see Table 10.2), which also corresponds to an EPAL = 100%. If taken literally, this would say that all values of compressive strength, whose average value is less than 946 psi and corresponding Q is less than 1.6, may receive a significant adjustment in pay. This, of course, is incorrect because when the items of the specifications are considered (average lot compressive strength = 750 psi and no more than 20% of the samples are less than 750 psi for the lot), practically all lots except the one mentioned above should receive close to full pay. As such, a choice of UQL may not be able to be based on only the project data available and on mechanical use of the technique of Chapter 5. Further scrutiny of the data is required, until additional (project) data are available to supplement that on hand for choice of UQL.

TABLE 10.2
 DETERMINATION OF AQL AND UQL USING P-306 DATA
 Performed on lots of 28-day strength
 Lots with ≥ 3 samples

UNIVARIATE PROCEDURE

Variable=Q_STR

Moments

| | | | |
|----------|----------|----------|----------|
| N | 45 | Sum Wgts | 45 |
| Mean | 9.648894 | Sum | 434.2002 |
| Std Dev | 11.84554 | Variance | 140.3168 |
| Skewness | 2.391665 | Kurtosis | 6.095318 |
| USS | 10363.49 | CSS | 6173.939 |
| CV | 122.7658 | Std Mean | 1.765829 |
| T:Mean=0 | 5.46423 | Prob> T | 0.0001 |
| Sgn Rank | 517.5 | Prob> S | 0.0001 |
| Num ^= 0 | 45 | | |

Quantiles(Def=5)

| | | | |
|----------|----------|-----|----------|
| 100% Max | 57.25275 | 99% | 57.25275 |
| 75% Q3 | 11.84446 | 95% | 37.7517 |
| 50% Med | 5.760556 | 90% | 21 |
| 25% Q1 | 2.327214 | 10% | 1.611986 |
| 0% Min | 0.288675 | 5% | 1.121765 |
| | | 1% | 0.288675 |
| Range | 56.96407 | | |
| Q3-Q1 | 9.517245 | | |
| Mode | 0.288675 | | |

Extremes

| | | | |
|-----------|-----|-----------|-----|
| Lowest | Obs | Highest | Obs |
| 0.288675(| 1) | 21(| 22) |
| 0.939899(| 17) | 35.79572(| 21) |
| 1.121765(| 30) | 37.7517(| 32) |
| 1.134074(| 6) | 38.68247(| 16) |
| 1.611986(| 9) | 57.25275(| 45) |

An alternative for choice of UQL may consist of a guess of value for UQL that would seem to be reasonable and consistent with the data that are available. As an example, consider a choice of UQL = 70 EPAL and suppose this corresponds for lots of sample size of 4. The formulas of Chapter 4 can provide the means to aid in judgement for the choice of UQL. That is

$$\text{EPAL}_L = [1-A]*100 \text{ and here EPAL}_L \text{ was chosen} = 70. \text{ That is,}$$

$$70 = 100*[1-A] \text{ which implies } A = .3$$

Further use of the formulas from Chapter 4 allows

$$A = \text{Max. } [0; 1/2 - 1/2*Q*(n^{1/2}/n-1)] \text{ or}$$

$$.3 = 1/2 - 1/2*Q*2/3 \quad \text{for } 0 < A. \text{ Whereupon}$$

$$Q = 0.6$$

That is, if $Q \geq 6$, this corresponds to a UQL = 70 EPAL, which probably suits the P-306 Econocrete compressive strength data fairly well since all lots, except the lot from May 9, 1986, would receive almost full pay. Only the lot where $Q = .289$ (see Table 10.1) would receive zero pay, while lots for Observations 2, 3, and 4 would receive slightly less than full pay.

The results of the foregoing analysis are illustrated in Figure 10.1. Therein, AQL = 100%, UQL = 70%, the SF = 0.60, and the pay factor is determined from the equation when $70\% < \text{EPAL} < 100$

$$\text{PAY FACTOR} = -3.212*\text{EPAL}^2 + 7.127*\text{EPAL} - 2.915$$

and

$$\begin{aligned} \text{PAY FACTOR} &= 1.00 \text{ for EPAL} \geq 100 \\ &= 0.50 \text{ for EPAL} = 70 \\ &= 0 \quad \text{for EPAL} < 70 \end{aligned}$$

According to this model, Observation 1 would receive zero pay; Observation 2 would receive 77% of full pay; Observation 3 would receive 91% of full pay; Observation 4 would receive 95% of full pay; and all other observations would receive full pay.

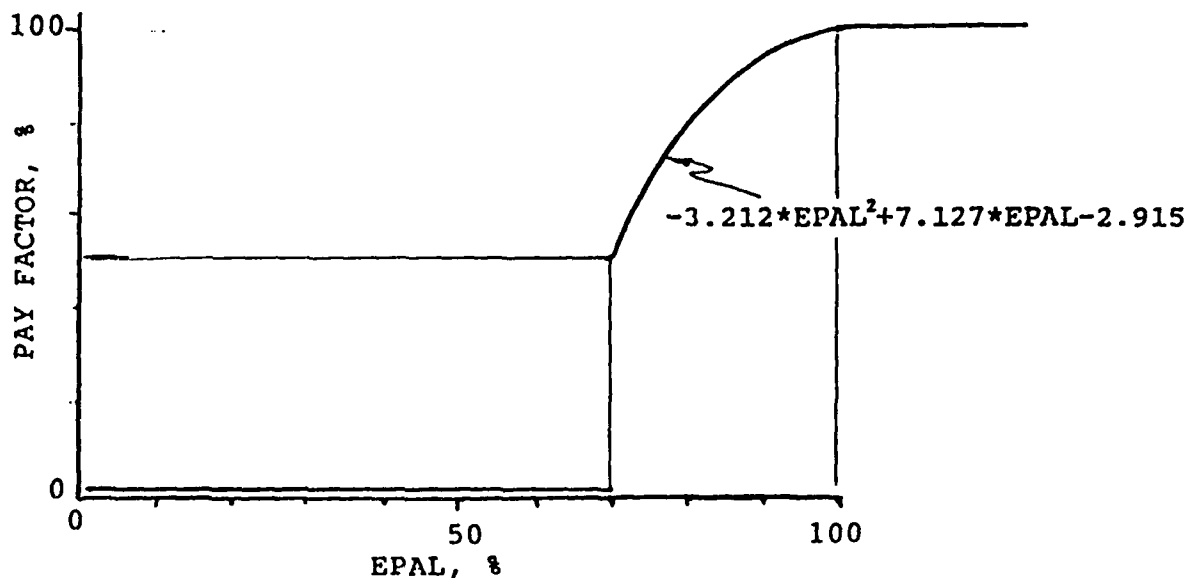


FIGURE 10.1 PAY FACTOR VERSUS EPAL

10.2.2 PAP When Lower and Upper Limits for Compressive Strength are Specified.

In the previous paragraphs, the discussion centered on the PAP when only a lower limit for compressive strength was specified under the constraints of average lot compressive strength and percentage of lot members allowed below the lower strength value. There should also be consideration for the situation when both upper and lower limits for compressive strength are specified for the material item, in this case P-306, Econocrete. In fact, one of the elements within the specifications for acceptance of P-306 Econocrete, based on compressive strength, is that the engineer may specify an upper limit of 1200 psi. What follows is a discussion that addresses the issue when both upper and lower limits are specified for the material item.

In most of the previous discussion, the reference has been made to percent above limit (PAL or EPAL) which was appropriate for the case when only a lower value was specified for the material item. However, when lower and upper limits are specified, reference should be made to percent within limit (PWL or EPWL), since for acceptance the value of the attribute (compressive strength) must on the average (and within the remaining requirements of the elements specified for acceptance) be at least equal to the lower limit. Additionally, the average value must not exceed the upper limit; that is, lower limit \leq compressive strength \leq upper limit. Thus, this attribute actually must satisfy the requirement of a

PWL. In order to accommodate the PWL (or EPWL), the following considerations were included in the PAP.

The data from the Pittsburgh and Harrisburg airports were analyzed and subjected to the same requirements (average 28-day strength \geq 750 psi) as before, with the added requirement that in the main, the lot compressive strength must not exceed 1200 psi. The results of doing this are presented in Table 10.3, wherein the last column represents the probability that the lot would lie between the 750 psi and 1200 psi limits. Thus, increasing values of EPWL are shown in the last column of Table 10.3 and it is clear that out of the 45 candidate lots for acceptance, only 33 lots have values of EPWL > 0 . The univariate analyses for the probability (EPWL) is shown in Table 10.4, wherein the 50th percentile has an EPWL = 55.6% and a 10th percentile EPWL = 0%. Thus, if these two values are selected for AQL and UQL, an expression for the pay factor can be written using the quadratic expression from Chapter 4 for $0 \leq \text{EPWL} \leq 55$ as

$$\text{PAY FACTOR} = -1.911 \cdot \text{EPWL}^2 + 2.869 \cdot \text{EPWL}$$

For EPWL > 55 , PAY FACTOR = 1.0

The pay factor versus EPWL is graphically illustrated in Figure 10.2.

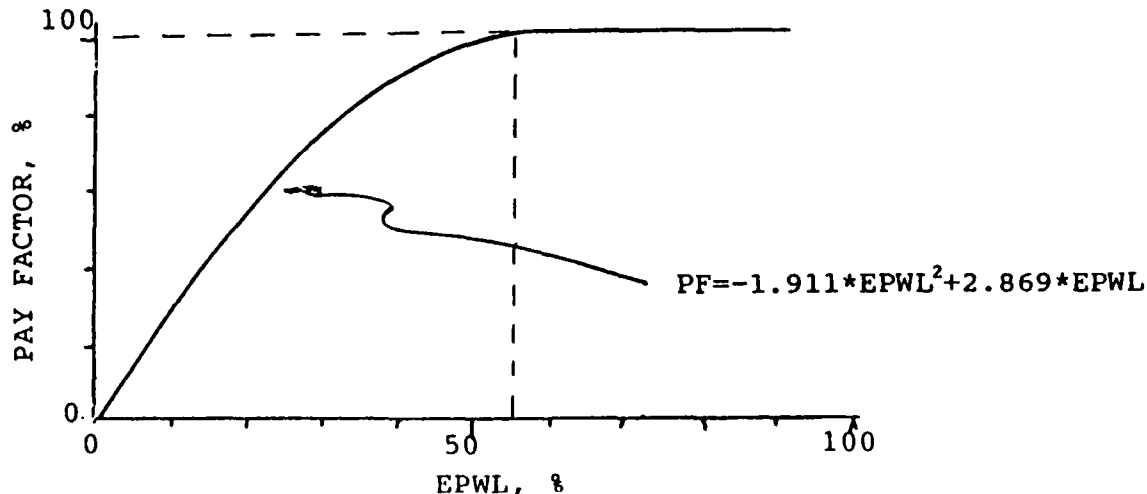


FIGURE 10.2 PAY FACTOR VERSUS EPWL

In all likelihood, the reference data for compressive strength from the Pittsburgh and Harrisburg projects were not subjected to the upper limit value and, as such, the curve of Figure 10.2 is biased significantly to the left. In other words, if future data is collected for P-306 Econocrete compressive strength, under the restrictions of lower and upper strength limits, the curve will shift to the right, which will be more in line with the functional form between Pay Factor and P-501 Concrete flexural strength.

TABLE 10.3
DETERMINATION OF AQL AND UQL USING P-306 DATA
Performed on lots of 28-day strength
Lots with ≥ 3 samples

| OBS | TESTDATE | LOT_NO | N_STR | MEAN_STR | STD_STR | P1 | P2 | PROB |
|-----|----------|---------|-------|----------|---------|---------|---------|---------|
| 1 | 19831117 | MDT306C | 4 | 2020.25 | 22.187 | 0.00000 | 1.00000 | 0.00000 |
| 2 | 19860424 | MDT306A | 3 | 1326.67 | 15.275 | 0.00000 | 1.00000 | 0.00000 |
| 3 | 19831118 | MDT306C | 4 | 1741.75 | 116.903 | 0.00000 | 1.00000 | 0.00000 |
| 4 | 19851210 | MDT306D | 4 | 1432.75 | 51.745 | 0.00000 | 1.00000 | 0.00000 |
| 5 | 19831121 | MDT306C | 4 | 1777.50 | 139.115 | 0.00000 | 1.00000 | 0.00000 |
| 6 | 19831115 | MDT306C | 4 | 1733.00 | 128.898 | 0.00000 | 1.00000 | 0.00000 |
| 7 | 19860326 | MDT306A | 3 | 1320.00 | 36.056 | 0.00000 | 1.00000 | 0.00000 |
| 8 | 19831116 | MDT306C | 4 | 1458.75 | 89.712 | 0.00000 | 1.00000 | 0.00000 |
| 9 | 19860707 | PIT306A | 4 | 1490.00 | 106.464 | 0.00000 | 1.00000 | 0.00000 |
| 10 | 19860908 | PIT306A | 4 | 1291.00 | 38.114 | 0.00000 | 1.00000 | 0.00000 |
| 11 | 19860723 | PIT306A | 4 | 1494.50 | 144.975 | 0.00000 | 1.00000 | 0.00000 |
| 12 | 19851211 | MDT306D | 4 | 1419.50 | 128.648 | 0.00000 | 1.00000 | 0.00000 |
| 13 | 19860719 | PIT306A | 4 | 1750.50 | 442.180 | 0.00000 | 0.91499 | 0.08501 |
| 14 | 19860910 | PIT306A | 4 | 1246.75 | 41.939 | 0.00000 | 0.87157 | 0.12843 |
| 15 | 19860701 | PIT306A | 4 | 1410.50 | 199.862 | 0.00000 | 0.85107 | 0.14893 |
| 16 | 19860702 | PIT306A | 4 | 1498.50 | 311.279 | 0.00000 | 0.81965 | 0.18035 |
| 17 | 19860714 | PIT306A | 4 | 1255.75 | 72.016 | 0.00000 | 0.75805 | 0.24195 |
| 18 | 19860718 | PIT306A | 4 | 1339.50 | 201.875 | 0.00000 | 0.73034 | 0.26966 |
| 19 | 19831122 | MDT306C | 4 | 1300.50 | 490.745 | 0.12608 | 0.56826 | 0.30566 |
| 20 | 19860421 | MDT306A | 6 | 1088.33 | 359.968 | 0.18670 | 0.39660 | 0.41670 |
| 21 | 19860407 | MDT306A | 6 | 1173.33 | 237.795 | 0.00000 | 0.46262 | 0.53738 |
| 22 | 19860804 | PIT306A | 4 | 1171.50 | 181.118 | 0.00000 | 0.44755 | 0.55245 |
| 23 | 19860404 | MDT306A | 6 | 1186.67 | 79.162 | 0.00000 | 0.44386 | 0.55614 |
| 24 | 19860509 | MDT306A | 3 | 753.33 | 11.547 | 0.40377 | 0.00000 | 0.59623 |
| 25 | 19860807 | PIT306A | 4 | 1154.00 | 120.036 | 0.00000 | 0.37226 | 0.62774 |
| 26 | 19860911 | PIT306A | 4 | 1180.25 | 46.421 | 0.00000 | 0.35818 | 0.64182 |
| 27 | 19860725 | PIT306A | 4 | 1083.50 | 199.321 | 0.00000 | 0.30517 | 0.69483 |
| 28 | 19860404 | MDT306D | 4 | 1092.25 | 169.683 | 0.00000 | 0.28833 | 0.71167 |
| 29 | 19860730 | PIT306A | 4 | 968.00 | 192.227 | 0.12198 | 0.09770 | 0.78033 |
| 30 | 19860828 | PIT306A | 3 | 1126.00 | 87.069 | 0.00000 | 0.21670 | 0.78330 |
| 31 | 19860912 | PIT306A | 4 | 1078.75 | 114.596 | 0.00000 | 0.14731 | 0.85269 |
| 32 | 19860409 | MDT306A | 6 | 993.33 | 150.953 | 0.00000 | 0.04364 | 0.95636 |
| 33 | 19860328 | MDT306A | 3 | 1026.67 | 35.119 | 0.00000 | 0.00000 | 1.00000 |
| 34 | 19860331 | MDT306A | 3 | 1026.67 | 15.275 | 0.00000 | 0.00000 | 1.00000 |
| 35 | 19860401 | MDT306A | 3 | 893.33 | 23.094 | 0.00000 | 0.00000 | 1.00000 |
| 36 | 19860402 | MDT306A | 3 | 976.67 | 11.547 | 0.00000 | 0.00000 | 1.00000 |
| 37 | 19860403 | MDT306A | 3 | 1170.00 | 20.000 | 0.00000 | 0.00000 | 1.00000 |
| 38 | 19860408 | MDT306A | 6 | 881.67 | 73.052 | 0.00000 | 0.00000 | 1.00000 |
| 39 | 19860410 | MDT306A | 6 | 888.33 | 24.014 | 0.00000 | 0.00000 | 1.00000 |
| 40 | 19860411 | MDT306A | 3 | 1163.33 | 11.547 | 0.00000 | 0.00000 | 1.00000 |
| 41 | 19860415 | MDT306A | 3 | 1085.00 | 8.660 | 0.00000 | 0.00000 | 1.00000 |
| 42 | 19860425 | MDT306A | 3 | 1010.00 | 20.000 | 0.00000 | 0.00000 | 1.00000 |
| 43 | 19860728 | PIT306A | 4 | 946.25 | 114.150 | 0.00000 | 0.00000 | 1.00000 |
| 44 | 19860729 | PIT306A | 4 | 977.00 | 39.387 | 0.00000 | 0.00000 | 1.00000 |
| 45 | 19860827 | PIT306A | 4 | 1039.00 | 72.778 | 0.00000 | 0.00000 | 1.00000 |

TABLE 10.4
 DETERMINATION OF AQL AND UQL USING P-306 DATA
 Performed on lots of 28-day strength
 Lots with ≥ 3 samples

UNIVARIATE PROCEDURE

Variable=PROB

Moments

| | | | |
|----------|----------|----------|----------|
| N | 45 | Sum Wgts | 45 |
| Mean | 0.512614 | Sum | 23.06763 |
| Std Dev | 0.414788 | Variance | 0.172049 |
| Skewness | -0.0636 | Kurtosis | -1.69908 |
| USS | 19.39493 | CSS | 7.570147 |
| CV | 80.91619 | Std Mean | 0.061833 |
| T:Mean=0 | 8.290311 | Prob> T | 0.0001 |
| Sgn Rank | 280.5 | Prob> S | 0.0001 |
| Num ^= 0 | 33 | | |

Quantiles(Def=5)

| | | | |
|----------|----------|-----|---|
| 100% Max | 1 | 99% | 1 |
| 75% Q3 | 1 | 95% | 1 |
| 50% Med | 0.556143 | 90% | 1 |
| 25% Q1 | 0 | 10% | 0 |
| 0% Min | 0 | 5% | 0 |
| | | 1% | 0 |
| Range | 1 | | |
| Q3-Q1 | 1 | | |
| Mode | 1 | | |

Extremes

| Lowest | Obs | Highest | Obs |
|--------|-----|---------|-----|
| 0(| 12) | 1(| 41) |
| 0(| 11) | 1(| 42) |
| 0(| 10) | 1(| 43) |
| 0(| 9) | 1(| 44) |
| 0(| 8) | 1(| 45) |

11.0 QUALITY CONTROL SPECIFICATIONS FOR P-501, CONCRETE

11.1 Background

One of the main factors for implementation of the technology from this project lies in the impact of this work on the specifications for airport construction material items of interest. Since the focus of this work rests primarily with P-501 Concrete flexural strength for the reasons stated in Subsections 4.3.3 through 4.3.7 and later in Section 10.1, the following discussion pertains solely to the impact of this work on the specification for P-501 Concrete flexural strength. Reference is made to a Draft Specification for P-501 Concrete that was issued for review by the Federal Aviation Administration. Specifically, the discussion that follows is primarily concerned with Paragraph 501-4.21, Acceptance Sampling and Testing, from that Draft Specification for P-501 Concrete.

11.2 Comments Pertaining to the Federal Aviation Administration Draft Specification for P-501 Concrete

There may be some concern over the method outlined in the specification, that is suggested to determine lot quality, because of the manner in which sample values for lots are determined. In Paragraph 501-4.21b., Pavement Strength, the following is quoted:

"Each lot (a lot is defined as one day's production) shall be divided into four equal sublots. One sample shall be taken, for each subplot, from the plastic concrete delivered to the job site. [For flexural strength determination, two specimens shall be made from each sample and the average of the two shall be the strength for that subplot.] Random sampling locations shall be determined by the Engineer in accordance with procedures contained in ASTM-D3665."

The question has been raised for the case of determining strength of the lot by using the average value for each subplot. It has been suggested that all eight values of strength (2 values per subplot and 4 sublots), taken together, be used to determine the average value of strength for the lot. The resulting quality estimate for the lot would be based on the average value of strength for the lot and the standard deviation of lot, when all values from the sublots are used individually in the calculation of the standard deviation. If this is done, it would tend to mask the impact of subplot importance on estimation of quality for the lot. If, in fact, the purpose of the subplot is to capture the influence of production throughout the day, this aspect is clouded when all values are taken together. On the other hand, if the average value for two specimens is used per subplot, then the influence of each subplot will be present in the estimation for lot quality, and variability

throughout the production day can be monitored. Additionally, because of the very nature of testing (for flexural strength) there is always the possibility that one of the specimens in the subplot would not be admissible for testing, due to damage or improper care during the 28-day cure period. If this happens, then the surviving specimen can be tested and the resulting value used to represent the strength of the subject. In the event that both specimens are rendered not useable for testing, then the number of sublots that make up the lot is reduced by one, but this does not destroy the influence of variability from subplot to subplot for the lot.

Having said the foregoing, it would seem that the method that is suggested for estimating pavement strength per Paragraph 501.21b. is completely in order and should remain as is.

A second concern is involved with the expression that is used to estimate unit price, in the event that the lot strength value or PWL is below 85%. The expression quoted in Paragraph 501-4.21d. for this purpose is:

$$PAP = -5.3333 * PWL + 9.7334 * PWL - 3.4200$$

It may be a better choice to leave the expression in the more general form:

$$PAP = A * PWL + B * PWL + C$$

where A, B, and C are values that shall be specified by the Federal Aviation Administration Regional Office, or on a per project basis, whichever is most appropriate. In this way, proper reflection of the past history for the attribute can be incorporated into the formulation by the procedures outlined in Chapters 4 and 5. Also, the percentage of 85% should not be "hard wired" in the specification for minimum PWL for which pay factor is full price. Instead, AQL should be specified as the value at and above which values of PWL receive full pay and below which an adjustment in price paid is made. The value of AQL should also be determined by the Federal Aviation Administration Regional Office, or on a per project basis, using historical information (data base) and the methods outlined in Chapters 4 and 5.

12. SUMMARY, CONCLUSIONS, AND RECOMMENDATIONS

12.1 Summary

The objective of this study was to develop a statistically based acceptance plan and a payment adjustment schedule applicable for five specification items. These are:

- P-152, Excavation and Embankment.
- P-209, Crushed Aggregate Base Course.
- P-304, Cement Treated Base Course.
- P-306, Econocrete Subbase Course.
- P-501, Portland Cement Concrete Pavement.

The study was divided into three work elements.

- o Work Element No. 1 included literature review and collection of historical construction data.
- o Work Element No. 2 included statistical analysis of the collected data and development of the pay adjustment plan.
- o Work Element No. 3 included field verification, at three airport construction sites, of plans developed in Work Element No. 2.

Quality Control between a supplier and a consumer is normally an acceptance/rejection of the product(s) being supplied. This means that a product(s) found to be below an acceptable quality limit (AQL) will be returned to the supplier. This is similar to what is currently being used for P-152, Excavation and Embankment, density; such as, when a test fails a specified limit, the work is rejected and the contractor reworks the area until the tests indicate a pass.

A variation of this acceptance/rejection quality control would be to have full payment above the acceptable quality limit, (AQL) a reject (zero payment) below a lower unacceptable quality limit (UAL) and a curved or straight line between these two points, indicating a progressive payment adjustment. This is currently similar to the P-401 Asphalt Concrete payment adjustment schedule.

The methodology of this quality control was the focus of Work Element No. 2, which consisted of reviewing current acceptable methodologies, statistically analyzing test data from previously constructed pavements, developing a Payment Adjustment Plan using this methodology, and statistically analyzing the data and incorporating this Payment Adjustment Plan into a computerized program.

In Work Element No. 3, the methodology and formulation that had been developed and implemented into the computer program during Work Element No. 2, was verified using data from recent airport construction projects for Item P-501, Portland Cement Concrete Pavement (flexural strength). Application of the method provides for a payment factor for the material item, that is consistent and fair, and is based on past pavement construction test data.

Additionally, the methodology and formulation system was extended to Item P-306, Econocrete (compressive strength), being based on the limited amount of available pavement construction test data for this use.

12.2 Conclusions

Based upon the results obtained in Work Element No. 2, the following conclusions can be drawn:

The technology that was used in the specification for P-401 Asphalt Concrete has been successfully expanded and improved upon to establish statistically based acceptance and pay adjustment plans for P-501 Concrete flexural strength. Application of this methodology to the five specifications listed in Section 6.1 for density is not practical or deemed implementable. However, use of the technology for P-306 Econocrete compressive strength, appears to be worthwhile.

The general consensus of persons interested in the quality control of density testing of pavements is that it can best be maintained by accept/ reject quality control (also known as pass/fail). These include P-152, Excavation and Embankment; P-209, Crushed Aggregate Base Course; and P-304, Cement Treated Base Course.

It has also been discovered that most engineers designing concrete pavements prefer to have thickness testing performed on the forms prior to pouring concrete, in lieu of core testing for thickness. These include P-306, Econocrete and P-501, Portland Cement Concrete Pavement.

12.3 Recommendations

During the data collection and entry tasks of this study, it was discovered that much test data was poorly documented, even to the point that some test data sheets did not identify what type material the tests were for, or for what airport or project they applied to. Also, many failed tests did not indicate retests. An example of highly organized and easily usable test records have been developed by The Construction Testing Division of ASW Environmental Consultants, Inc., Allentown, PA.

Recommendations are as follows:

- o It is recommended that the FAA develop and utilize a standard format for field and laboratory pavement test data sheets for all FAA pavement specifications. This should include the airport name, airport location, the FAA specification material and type, and all other pertinent information and test data. Entries for failed tests and retests should also be included.
- o It is recommended that a payment adjustment schedule not be made for materials such as:

P-152, Excavation and Embankment.
P-209, Crushed Aggregate Base Course.
P-304, Cement Treated Base Course.

- o Since many engineers are currently using nuclear testing for P-152, Excavation and Embankment, it is recommended that the FAA evaluate procedures for the acceptance of nuclear testing.
- o Since most engineers are currently measuring form depth in lieu of core testing for concrete, it is recommended that the FAA evaluate acceptable methods for these type inspections. This includes the materials of P-306, Econocrete and P-501, Portland Cement Concrete Pavement. Because of the lack of thickness test data, it is recommended that a thickness-based Payment Adjustment Schedule, on these two items, not be developed at this time.
- o Current practice for P-501 Concrete flexural strength is that beams will be broken at 7-days, and if these test results are above the 28-day specification the Contractor may be paid at 100% and the 28-day tests may/may not be performed. It is recommended that a partial payment, at most, be made based on the 7-day tests and a final payment be made after 28-day tests according to Payment Adjustment Schedule calculations.
- o Development of a payment adjustment schedule for Item P-501, Portland Cement Concrete Pavement is recommended because sufficient, acceptable test data have been collected and it is desirable to have such a payment adjustment program for this type material. This Payment Adjustment Schedule has been developed into an IBM Compatible computer program that can be used for field entry of test data results.

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APPENDIX A NORMAL DISTRIBUTION

The normal distribution is actually a family of distributions given by the following function of x ($-\infty < x < \infty$):

$$f(x|\mu, \sigma) = \frac{1}{\sigma(2\pi)^{1/2}} \exp \left[-\frac{(x-\mu)^2}{2\sigma^2} \right] \quad (\text{A-1})$$

where μ ($-\infty < \mu < \infty$) is the mean of the distribution and σ ($\sigma > 0$) is the standard deviation of the distribution; there is a unique normal distribution corresponding to each choice of μ and σ . The graph of $f(x)$ is symmetrical and bell-shaped, and centered at μ . The spread of the graph is determined by σ and widens as σ increases.

For a given μ and σ , the area under the graph of (A-1) and to the left of L is equal to

$$A = \int_{-\infty}^L f(x|\mu, \sigma) dx \quad (\text{A-2})$$

Due to a special property of the normal distribution, this area is equal to

$$A = \int_{-\infty}^{(L-\mu)/\sigma} f(x|0, 1) dx \quad (\text{A-3})$$

where $f(x|0, 1)$ is the standard normal distribution, the normal family member with $\mu = 0$ and $\sigma = 1$. The equality of the areas in (A-2) and (A-3) imply that the area under any normal distribution and to the left of a limit can be found by computing the area under a standard normal distribution and to the left of the original limit transformed.

Another way to refer to the area in (A-3) is $\Phi[(L-\mu)/\sigma]$, where the function $\Phi(\cdot)$ is the area under the standard normal curve and to the left of the argument. This integral is easily evaluated using numerical methods; tables of this integral appear in most

statistics books and an abbreviated table appears below as Table A.1. Note that $z = (L - \mu) / \sigma$ and $A = \Phi(z) = \Phi[(L - \mu) / \sigma]$. For example, if $L = 650$, $\mu = 600$, and $\sigma = 48$; $z = 1.04$ and according to Table A.1, the area to the left of 650 is about .85.

| z | A |
|--------|-----|
| 2.326 | .99 |
| 1.645 | .95 |
| 1.282 | .90 |
| 1.037 | .85 |
| .842 | .80 |
| .675 | .75 |
| .524 | .70 |
| .385 | .65 |
| .253 | .60 |
| .126 | .55 |
| 0 | .50 |
| - .126 | .45 |
| - .253 | .40 |
| - .385 | .35 |
| - .524 | .30 |
| - .675 | .25 |
| - .842 | .20 |
| -1.037 | .15 |
| -1.282 | .10 |
| -1.645 | .05 |
| -2.326 | .01 |

TABLE A.1.
STANDARD NORMAL DISTRIBUTION

If one is interested in the area under a normal curve and to the right (rather than left) of a limit, the computations are similar. First note that since the normal curve is symmetric, $\Phi(x) + \Phi(-x) = 1$. Since the area to the right of a limit, plus the area to the left of the same limit, must equal 1, $\Phi(x)$ being the area to the left implies that the area to the right is $\Phi(-x)$. Thus, the area under a normal curve and to the right of a limit is $\Phi[-(L - \mu) / \sigma] = \Phi[(\mu - L) / \sigma]$. For example, if $L = 650$, $\mu = 600$, and $\sigma = 48$; $z = -1.04$ and according to Table A.1, the area to the right of 650 is about .15.

APPENDIX B
DERIVATION OF FORMULAS FOR EPAL_n

In this appendix, Equations (B-5) through (B-14) are derived from Equation (3.4) from Page 9. Recall that:

$$\text{EPAL}_n = 100 \left\{ 1 - \int_0^A \text{beta} (X; n/2 - 1) dX \right\}, \quad (\text{B-1})$$

where $A = \max [0, 1/2 - 1/2 Q (n^{1/2}/n-1)]$ and $\text{beta} (X; n/2 - 1)$ is the beta density with $\alpha = \beta = n/2 - 1$. The beta density is defined for $\alpha, \beta > 0$ and is non-zero for $0 < X < 1$; it is [7]:

$$f(X) = \frac{\Gamma(\alpha+\beta)}{\Gamma(\alpha)\Gamma(\beta)} X^{\alpha-1} (1-X)^{\beta-1}. \quad (\text{B-2})$$

The following 2 equations are useful in analyzing the gamma function. Note that Equation (B-3) implies that for a positive integer Z , $\Gamma(Z) = (Z-1)!$.

$$\Gamma(Z+1) = Z \Gamma(Z) \text{ for } Z > 0 \quad (\text{B-3})$$

$$\Gamma(1/2) = \pi^{1/2} \quad (\text{B-4})$$

Substituting $\alpha = \beta = n/2 - 1$ into Equation (B-2), and substituting the result into Equation (B-1) produces, for a positive integer n ,

$$\text{EPAL}_n = 100 \left\{ 1 - \frac{\Gamma(n-2)}{[\Gamma(n/2 - 1)]^2} \int_0^A (X-X^2)^{n/2-2} dX \right\}. \quad (\text{B-5})$$

Since $\alpha, \beta > 0$, n must be greater than 2. For $n = 3$, from a table of integrals [8] it is found that:

$$\int_0^A (X-X^2)^{-1/2} dX = -\text{SIN}^{-1}(1-2A) + \pi/2. \quad (\text{B-6})$$

Using Equations (B-6) and (B-5) it is seen that:

$$EPAL_3 = 100 \{ .5 + (1/\pi) \sin^{-1}(1-2A) \} \quad (B-7)$$

which is Equation (4.5) from Page 9. Also from a table of integrals [8] it is found that, for a non-negative integer N,

$$\int_0^A (X-X^2)^{N+1/2} dX = \frac{(1-2A)(A-A^2)^{N+1/2}}{-4(N+1)} + \frac{(2N+1)}{8(N+1)} \int_0^A (X-X^2)^{N-1/2} dX. \quad (B-8)$$

Letting $N + 1/2 = n/2 - 2$ we see that $N = n/2 - 5/2$ is a non-negative integer for n odd and n greater than 3. Substituting the new expression for N into Equation (B-8):

$$\int_0^A (X-X^2)^{n/2-2} dX = \frac{(1-2A)(A-A^2)^{n/2-2}}{-2(n-3)} + \frac{(n-4)}{4(n-3)} \int_0^A (X-X^2)^{n/2-3} dX. \quad (B-9)$$

Note that the integral on the right hand side of Equation (B-9) can be written in terms of $EPAL_{n-2}$ by substituting $n-2$ for n in Equation (B-5) and solving:

$$\int_0^A (X-X^2)^{n/2-3} dX = \frac{[\Gamma(n/2 - 2)]^2}{\Gamma(n-4)} (1 - EPAL_{n-2} / 100). \quad (B-10)$$

Substituting the right hand side of Equation (B-10) into Equation (B-9), and substituting the result into Equation (B-5), it is found that, for n odd and n greater than 3,

$$EPAL_n =$$

$$100 \left\{ 1 - \frac{\Gamma(n-2)}{[\Gamma(n/2 - 1)]^2} \left[\frac{(1-2A)(A-A^2)^{n/2-2}}{2(n-3)} + \frac{(n-4)}{4(n-3)} \right. \right. \\ \left. \left. \frac{[\Gamma(n/2 - 2)]^2}{\Gamma(n-4)} (1 - EPAL_{n-2}/100) \right] \right\} \quad (B-11)$$

Note that:

$$\frac{\Gamma(n-2)}{[\Gamma(n/2 - 1)]^2} \frac{(n-4)}{4(n-3)} \frac{[\Gamma(n/2 - 2)]^2}{\Gamma(n-4)} = 1 \quad (B-12)$$

Using Equations (B-11) and (B-12) we get:

$$EPAL_n = 100 \left\{ \frac{\Gamma(n-2)}{[\Gamma(n/2 - 1)]^2} \frac{(1-2A)(A-A^2)^{n/2-2}}{2(3-n)} \right\} + EPAL_{n-2} \quad (B-13)$$

Equations (4-7), (4-9), (4-11), and (4-13) from Page 9 follow directly from Equation (B-13).

Using the binomial formula [8], it is found that, for a non-negative integer N,

$$(X-X^2)^N = \sum_{i=0}^N (-1)^i C(N,i) X^{N+i} \quad (B-14)$$

where C(N,i) equals the number of unique combinations of N items taken i at a time. Applying the integral to both sides of Equation (B-14):

$$\int_0^A (X-X^2)^N dx = \sum_{i=0}^N (-1)^i C(N,i) \frac{A^{N+i+1}}{N+i+1} \quad (B-15)$$

Letting $N = n/2 - 2$ it is seen that N is a non-negative integer for n even and n greater than 2. Substituting the new expression for N into Equation (B-15), and the result into Equation (B-5) produces, for n even and n greater than 2,

$EPAL_n =$

$$100 \left\{ 1 - \frac{\Gamma(n-2)}{[\Gamma(n/2 - 1)]^2} \sum_{i=0}^{n/2 - 2} (-1)^i C(N, i) \frac{A^{n/2 + i - 1}}{n/2 + i - 1} \right\} \quad (B-16)$$

Equations (4-6), (4-8), (4-10), (4-12), and (4-14) from Page 9 follow directly from Equation (B-16).

APPENDIX C CALCULATION OF THE OC

In this Appendix, a method for calculating the OC corresponding to a particular value of PAL will be presented. This value, OC_{100p} , can be written:

$$OC_{100p} = \Pr (EPAL_n < \text{Acceptance Limit} \mid PAL = 100p). \quad (C-1)$$

With respect to the acceptance plan for P-501 Concrete, Equation (C-2) is:

$$OC_{100p} = \Pr (EPAL_n < 73\% \mid PAL = 100p). \quad (C-2)$$

Using the fact that there is a one-to-one correspondence between $EPAL_n$ and Q [Equation (4.10)] Page 9, and the fact that $PAL = 100 \Phi[(\mu-L)/\sigma]$, an equivalent expression for Equation (C-2) is:

$$OC_{100p} = \Pr (Q < .6344 \mid (\mu-L)/\sigma = \Phi^{-1}(p)). \quad (C-3)$$

Using an elementary result in probability, all the terms on the right side of Equation (C-3) can be multiplied by a constant resulting in the equivalent expression:

$$OC_{100p} = \Pr (8^{1/2}Q < 1.794 \mid 8^{1/2}(\mu-L)/\sigma = 8^{1/2}\Phi^{-1}(p)). \quad (C-4)$$

The probability in Equation (C-4) can be computed using the fact that $n^{1/2}Q$ is distributed as a noncentral t random variable with $r = n-1$ degrees of freedom and noncentrality parameter $\delta = n^{1/2}(\mu-L)/\sigma$ [Appendix D]. To simplify the calculations use the fact that the probability that a noncentral t random variable with parameters r and δ is less than a constant, h , is approximately equal to $\Phi(z)$ where z is computed using Equation (C-5) [9]:

$$z = \frac{h(1 - 1/4r) - \delta}{(1 + h^2/2r)^{1/2}}. \quad (C-5)$$

For example, for $PAL = 80$, it is found from a standard normal table that $(\mu-L)/\sigma = 0.842$. This implies that $\delta = 2.382$. Using Equation (C-5) we find that $z = -.588$. Again, using a standard normal table, we find that $OC_{80} = .278$. The OC corresponding to various levels of PAL appear in Table C.1, along with the results of the intermediate calculations.

| PAL | $(\mu-L)/\sigma$ | δ | z | OC |
|-----|------------------|----------|--------|------|
| 95 | 1.645 | 4.653 | -2.636 | .004 |
| 90 | 1.282 | 3.626 | -1.710 | .044 |
| 85 | 1.036 | 2.930 | -1.082 | .140 |
| 80 | 0.842 | 2.382 | -0.588 | .278 |
| 75 | 0.674 | 1.906 | -0.159 | .437 |
| 70 | 0.524 | 1.482 | 0.224 | .589 |
| 65 | 0.385 | 1.089 | 0.578 | .718 |
| 60 | 0.253 | 0.716 | 0.914 | .820 |
| 55 | 0.126 | 0.356 | 1.239 | .892 |

TABLE C.1
OPERATING CHARACTERISTIC FOR GIVEN PAL AND QUALITY LEVELS

Also in this Appendix, a method for computing the overdesign ($\mu-L$) corresponding to a given probability (P) and lot standard deviation (σ) will be presented. This value can be computed using a rewritten form of Equation (C-5):

$$\delta = h(1 - 1/4\tau) - z(1 + h^2/2\tau)^{1/2}. \quad (C-6)$$

For example, consider the acceptance plan for P-501 Concrete. Recall that the acceptance value is 73%. Using Equation (4-10) Page 9, it is found that the corresponding Q is .6344. Since $h = n^{1/2}(Q)$, $h = 1.794$. Since $\tau = n-1$, $\tau = 7$. Now for $P = .90$, $z = -1.282$. Using Equation (4-17) it is found that $\delta = 3.152$. Since $\delta = n^{1/2}(\mu-L)/\sigma$, $(\mu-L)/\sigma = 1.114$. This relationship allows computing, for a given σ , the ($\mu-L$) needed to achieve a probability of .90 of acceptance, as in Table 4.4, Page 17. The same is done for $P = .95$ and $P = .99$ and the results are presented in Table C.2 along with the results of the intermediate calculations.

| P | z | δ | $(\mu-L)/\sigma$ |
|-----|--------|----------|------------------|
| .90 | -1.282 | 3.152 | 1.114 |
| .95 | -1.645 | 3.554 | 1.257 |
| .99 | -2.326 | 4.309 | 1.523 |

TABLE C.2
QUALITY REQUIRED TO ACHIEVE GIVEN PROBABILITY OF ACCEPTANCE

APPENDIX D
DERIVATION OF THE DISTRIBUTION OF $N^{1/2} Q$

In this appendix it will be shown that $n^{1/2}Q$ is distributed as a noncentral t random variable with $r = n-1$ degrees of freedom and noncentrality parameter $\delta = n^{1/2}(\mu-L)/\sigma$. Recall that:

$$Q = \frac{\bar{X}-L}{S} \quad (D-1)$$

A noncentral t random variable with r degrees of freedom and noncentrality parameter δ is defined as the ratio of a normal random variable with mean δ and standard deviation 1, and the square root of a chi-square random variable divided by its degrees of freedom r [4].

First note that [4]:

$$\frac{\bar{X}-\mu}{\sigma/n^{1/2}} \in N(0,1). \quad (D-2)$$

This implies that:

$$\frac{\bar{X}-\mu}{\sigma/n^{1/2}} + \frac{\mu-L}{\sigma/n^{1/2}} = \frac{\bar{X}-L}{\sigma/n^{1/2}} \in N(\delta,1), \quad (D-3)$$

where δ equals $n^{1/2}(\mu-L)/\sigma$. Also note that [4]:

$$\frac{(n-1)S^2}{\sigma^2} \in \text{Chi-square } (n-1). \quad (D-4)$$

Dividing the random variable by its degrees of freedom and taking the square root:

$$\left[\frac{(n-1)S^2}{\sigma(n-1)} \right]^{1/2} = \frac{S}{\sigma}. \quad (D-5)$$

Dividing the $N(\delta, 1)$ random variable in Equation (D-3) by the right hand side of Equation (D-5):

$$n^{1/2} \frac{\bar{X} - L}{S} \quad (D-6)$$

which, by definition, is a noncentral t random variable with $r = n-1$ degrees of freedom and noncentrality parameter $\delta = n^{1/2}(\mu - L)/\sigma$.

APPENDIX E ERROR CODES

TABLE E.1

| Code | Decsription | Code | Description |
|------|---------------------------------|------|----------------------------------|
| 2 | Syntax error | 53 | File not found |
| 3 | RETURN without GOSUB | 54 | Bad file mode |
| 4 | Out of DATA | 55 | File already open |
| 5 | Illegal function call active | 56 | FIELD statement |
| 6 | Overflow | 57 | Device I/O error |
| 7 | Out of memory | 58 | File already exists |
| 9 | Subscript out of range | 59 | Bad record length |
| 10 | Duplicate definition | 61 | Disk full |
| 11 | Division by zero | 62 | Input past end of file |
| 13 | Type mismatch | 63 | Bad record number |
| 14 | Out of string space | 64 | Bad file name |
| 16 | String formula too complex | 67 | Too many files |
| 19 | No RESUME | 68 | Device unavailable |
| 20 | RESUME without error | 69 | Communication-buffer overflow |
| 24 | Device Timeout | 70 | Permission denied |
| 25 | Device fault | 71 | Disk not ready |
| 27 | Out of paper | 72 | Disk-media error |
| 39 | CASE ELSE expected | 73 | Advanced feature unavailable |
| 40 | Variable required | 74 | Rename across disks |
| 50 | FIELD overflow error | 75 | Path/File access |
| 51 | Internal Error | 76 | Path not found |
| 52 | Bad file name or number | | |

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APPENDIX F
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July 21, 1989

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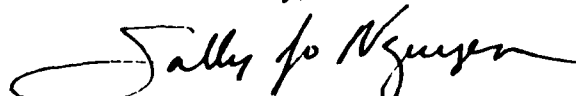
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APPENDIX G
SAMPLE OF dBASE III FILENAMES

P-501, PORTLAND CEMENT CONCRETE PAVEMENT
(FLEXURAL STRENGTH AND THICKNESS)

| | |
|---------|--|
| ACY501A | FAA TECH CENTER, FLEX '85 |
| ACY501B | FAA TECH CENTER, '85 (THICKNESS) |
| BUF501A | GREATER BUFFALO INTERNAT '86 |
| BUF501B | GREATER BUFFALO INTERNAT |
| BUF501C | GREATER BUFFALO INTERNAT '74-75 |
| BUF501D | GREATER BUFFALO INTERNAT '86 (THICKNESS) |
| BWI501A | BALTIMORE WASHINGTON INT '84-85 |
| CHO501A | CHARLOTTESVILLE-ALBERMARLE, VA. '84 |
| IAD501A | DULLES INTERNATIONAL '86 |
| IAG501A | NIAGARA FALLS INT. AIRPORT '85 |
| IAG501B | NIAGARA FALLS INT. AIRPORT |
| ORF501A | NORFOLK INTERNATIONAL '87 |
| ORF501B | NORFOLK INTERNATIONAL '84 |
| PHF501A | PATRICK HENRY AIRPORT '75 |
| PHL501A | PHILADELPHIA INTERNATIONAL '87 |
| PIT501A | GREATER PITTSBURGH |
| PIT501B | GREATER PITTSBURGH (THICKNESS) |
| PIT501C | GREATER PITTSBURGH '86 |
| PIT501D | GREATER PITTSBURGH '86 (THICKNESS) |
| ROC501A | ROCHESTER MONROE COUNTY '83 |
| SBY501A | WICOMICO COUNTY AIRPORT '85 |
| SYR501A | HANCOCK INT - SYRACUSE '80 |
| SYR501B | HANCOCK INT - SYRACUSE '82 |

APPENDIX H P-501 TEST DATA PRINTOUT SAMPLE

FAA ACCEPTANCE AND PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENTS P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 1

Airport: Norfolk International Airport
Norfolk, VA
ORF

Consultant/Engineer: R. Kenneth Weeks, Engineers
Norfolk, VA

Construction Contractor: Williams Corp. of Va.
Norfolk, VA

Pavement Testing Laboratory: ATEL Associates of Va., Inc.
Norfolk, VA

FAA Contract Number: AIP #3-51-0036-06
FAA Project Name: Terminal Apron Expansion
Work Area Project Name: Apron Expansion, 1988

Pavement Specification: P-501, PORTLAND CEMENT CONCRETE PAVEMENT
Design Target Specification in PSI: 700

Method of Testing: Flexural Strength Beams
ASTM Number: ASTM-C-78

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|---------------------------------|-------------|-----------|---------------|
| 1 | Lane #1, north end at 0+80 | 11/24/87 | 12/22/87 | 28 |
| 2 | Lane #1, north end | 11/24/87 | 12/22/87 | 28 |
| 3 | Lane #3, north end at 0+80 | 11/25/87 | 12/23/87 | 28 |
| 4 | Lane #3, north end at 0+330 | 11/25/87 | 12/23/87 | 28 |
| 5 | Lane #5, north end | 11/30/87 | 12/28/87 | 28 |
| 6 | 0+330 Ft | 11/30/87 | 12/28/87 | 28 |
| 7 | Lane #7, north end at 0+80 | 12/02/87 | 12/30/87 | 28 |
| 8 | north end at 0+240 | 12/03/87 | 01/05/88 | 33 |
| 9 | Lane #9, north end, 0+130 yards | 12/07/87 | 01/05/88 | 29 |
| 10 | Lane #9, north end 0+370 | 12/07/87 | 01/05/88 | 29 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR | |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|--------|---------|--------------|-------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 1 | 655 | 660 | 705 | 710 | 0 | 0 | 683 | 29.011 | -0.603 | 29.9 | 0.0 |
| 2 | 775 | 750 | 795 | 785 | 0 | 0 | 776 | 19.311 | 3.949 | 100.0 | 100.0 |
| 3 | 720 | 715 | 810 | 890 | 0 | 0 | 784 | 83.204 | 1.007 | 83.6 | 94.1 |
| 4 | 720 | 710 | 785 | 790 | 0 | 0 | 751 | 42.106 | 1.217 | 90.6 | 100.0 |
| 5 | 675 | 730 | 735 | 780 | 0 | 0 | 730 | 43.012 | 0.697 | 73.2 | 79.2 |
| 6 | 745 | 740 | 765 | 807 | 0 | 0 | 764 | 30.478 | 2.108 | 100.0 | 100.0 |
| 7 | 750 | 720 | 770 | 810 | 0 | 0 | 763 | 37.749 | 1.656 | 100.0 | 100.0 |
| 8 | 730 | 764 | 815 | 830 | 0 | 0 | 785 | 46.155 | 1.836 | 100.0 | 100.0 |
| 9 | 730 | 740 | 760 | 795 | 0 | 0 | 756 | 28.687 | 1.961 | 100.0 | 100.0 |
| 10 | 780 | 750 | 815 | 800 | 0 | 0 | 786 | 28.100 | 3.069 | 100.0 | 100.0 |

APPENDIX H (Continued)
P-501 TEST DATA PRINTOUT SAMPLE

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 2

Airport: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Apron Expansion, 1988

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--|-------------|-----------|---------------|
| 11 | 3rd slab from west, 66' from north to south | 12/08/87 | 01/05/88 | 28 |
| 12 | 3rd slab from west, 254' from north to south | 12/08/87 | 01/05/88 | 28 |
| 13 | Lane #11, North end 0+250 yds | 12/10/87 | 01/07/88 | 28 |
| 14 | Lane #11, north end, 0+410 ft | 12/10/87 | 01/07/88 | 28 |
| 15 | Lane #11, north end, 0+90 | 12/11/87 | 01/08/88 | 28 |
| 16 | Lane #11 | 12/11/87 | 01/08/88 | 28 |
| 17 | Lane #2, near runway, north end 0+100 | 12/12/87 | 12/26/87 | 14 |
| 18 | Lane #2, north end 0+320 | 12/12/87 | 12/26/87 | 14 |
| 19 | Lane #4, north end, 0+115 ft | 12/14/87 | 12/28/87 | 14 |
| 20 | Lane #4, north end 0+390 ft | 12/14/87 | 12/28/87 | 14 |
| 21 | Lane #6, north end 0+130 ft | 12/16/87 | 01/13/88 | 28 |
| 22 | Lane #6, 0+390 | 12/16/87 | 01/13/88 | 28 |
| 23 | Lane #8, north end, 0+95 ft | 12/17/87 | 01/14/88 | 28 |
| 24 | Lane #8, 0+245 ft | 12/18/87 | 01/15/88 | 28 |
| 25 | Lane #8, 0+366 ft | 12/18/87 | 01/15/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | |
| 11 | 695 | 680 | 735 | 755 | 0 | 0 | 716 | 34.731 | 0.468 | 63.7 |
| 12 | 725 | 700 | 810 | 850 | 0 | 0 | 771 | 70.519 | 1.010 | 94.3 |
| 13 | 735 | 716 | 790 | 830 | 0 | 0 | 768 | 52.028 | 1.302 | 100.0 |
| 14 | 695 | 695 | 750 | 720 | 0 | 0 | 715 | 26.141 | 0.574 | 71.3 |
| 15 | 725 | 669 | 780 | 760 | 0 | 0 | 734 | 48.638 | 0.689 | 78.7 |
| 16 | 675 | 750 | 730 | 810 | 0 | 0 | 741 | 55.734 | 0.740 | 81.7 |
| 17 | 585 | 620 | 670 | 670 | 0 | 0 | 636 | 41.508 | -1.536 | 0.0 |
| 18 | 660 | 640 | 720 | 725 | 0 | 0 | 686 | 42.696 | -0.322 | 0.0 |
| 19 | 640 | 620 | 715 | 684 | 0 | 0 | 665 | 42.859 | -0.822 | 0.0 |
| 20 | 675 | 655 | 745 | 700 | 0 | 0 | 694 | 38.810 | -0.161 | 0.0 |
| 21 | 670 | 720 | 760 | 790 | 0 | 0 | 735 | 51.962 | 0.674 | 77.8 |
| 22 | 670 | 712 | 790 | 710 | 0 | 0 | 721 | 50.210 | 0.408 | 59.1 |
| 23 | 775 | 745 | 760 | 770 | 0 | 0 | 763 | 13.229 | 4.725 | 100.0 |
| 24 | 710 | 740 | 795 | 780 | 0 | 0 | 756 | 38.595 | 1.457 | 100.0 |
| 25 | 830 | 880 | 940 | 955 | 0 | 0 | 901 | 57.500 | 3.500 | 100.0 |

APPENDIX H (Continued)
P-501 TEST DATA PRINTOUT SAMPLE

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 3

Airport: Norfolk International Airport, Norfolk, VA
FAA Project Name: Terminal Apron Expansion
Work Area Project Name: Apron Expansion, 1988

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--|-------------|-----------|---------------|
| 26 | Lane #8, north end 0+150 ft | 12/21/87 | 01/18/88 | 28 |
| 27 | Lane #10, north end, 3+35 | 01/04/88 | 02/01/88 | 28 |
| 28 | Lane #10, from 0+00 to 0+50 | 01/13/88 | 02/10/88 | 28 |
| 29 | Lane #12, north end 100+30 ft | 01/19/88 | 02/16/88 | 28 |
| 30 | Lane #12, north end, 3+10 ft | 01/19/88 | 02/16/88 | 28 |
| 31 | Lane #12, north end, 4+10 ft | 01/21/88 | 02/04/88 | 14 |
| 32 | Lane #14, east end, 1+10 ft | 01/22/88 | 02/19/88 | 28 |
| 33 | Area #2, center cross lane, seq. #2 | 02/01/88 | 02/29/88 | 28 |
| 34 | Lane #2, area #3, east end, 0+85 ft | 02/09/88 | 03/08/88 | 28 |
| 35 | Lane #2, area #3, east end, 1+95 ft | 02/09/88 | 03/08/88 | 28 |
| 36 | Lane #4, south side, east end, 0+85 ft | 02/10/88 | 03/09/88 | 28 |
| 37 | Lane #4, area #3, south side, east end 1+98 ft | 02/10/88 | 03/09/88 | 28 |
| 38 | Area #2, lane #3, east end 0+95 | 02/15/88 | 03/14/88 | 28 |
| 39 | Lane #3, area #2, east end, 1+15 ft | 02/17/88 | 03/16/88 | 28 |
| 40 | Area #2, Lane #4, East of 3+40' | 02/17/88 | 03/16/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI----- | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|----------------------------------|-----|-----|-----|-----|-------------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 AVERAGE | | | | |
| 26 | 710 | 720 | 790 | 740 | 0 | 0 740 | 35.590 | 1.124 | 87.5 | 98.0 |
| 27 | 720 | 700 | 695 | 745 | 0 | 0 715 | 22.730 | 0.660 | 72.0 | 76.9 |
| 28 | 720 | 770 | 830 | 810 | 0 | 0 783 | 48.563 | 1.699 | 100.0 | 100.0 |
| 29 | 759 | 750 | 825 | 790 | 0 | 0 781 | 33.971 | 2.384 | 100.0 | 100.0 |
| 30 | 662 | 638 | 720 | 740 | 0 | 0 690 | 47.917 | -0.209 | 43.0 | 0.0 |
| 31 | 600 | 640 | 760 | 760 | 0 | 0 690 | 82.462 | -0.121 | 46.0 | 0.0 |
| 32 | 750 | 670 | 745 | 770 | 0 | 0 734 | 43.851 | 0.770 | 75.7 | 83.3 |
| 33 | 670 | 690 | 810 | 880 | 0 | 0 763 | 99.791 | 0.626 | 70.9 | 74.8 |
| 34 | 875 | 790 | 860 | 880 | 0 | 0 851 | 41.708 | 3.626 | 100.0 | 100.0 |
| 35 | 720 | 730 | 810 | 810 | 0 | 0 768 | 49.244 | 1.371 | 95.7 | 100.0 |
| 36 | 700 | 685 | 760 | 785 | 0 | 0 733 | 47.697 | 0.681 | 72.7 | 78.2 |
| 37 | 710 | 710 | 780 | 770 | 0 | 0 743 | 37.749 | 1.126 | 87.5 | 98.1 |
| 38 | 700 | 730 | 825 | 805 | 0 | 0 765 | 59.582 | 1.091 | 86.4 | 97.0 |
| 39 | 770 | 760 | 830 | 800 | 0 | 0 790 | 31.623 | 2.846 | 100.0 | 100.0 |
| 40 | 720 | 760 | 780 | 850 | 0 | 0 778 | 54.391 | 1.425 | 97.5 | 100.0 |

APPENDIX I CURVE DEFAULT PROGRAM

The [FAACURVE] program was designed to permit FAA office personnel to change the defaults from airport to airport.

This program flow is as follows:

1. Load MS-DOS into computer.
2. Enter [A:] to transfer to A: Drive.
3. Insert OFFICE FAA-PAP disk into Drive A, type [FAASTART] and press [ENTER] key. From the Introduction Screen, type [CURVE] and press the [ENTER] key.
4. Screen 1 Figure I.1 will appear, explaining this program is restricted to FAA trained personnel only. Press any key to continue.
5. Screen 2 Figure I.2 will appear permitting FAA personnel to specify the airport, consultant and the specific contract the defaults will apply to. Press [Y] to continue.
6. Screen 3 Figure I.3 will appear permitting selecting of the design target specification. This screen is also a menu. Selecting [2] will load PAP programs and selecting [3] will return to MS-DOS.
7. The default selection and calculation Screen 4, Figure I.4 will appear. Selecting a default point by number, [1] through [3], will permit changing a default as follows:
 - [1] Point 1-All PAL above will receive 100% payment.
 - [2] Point 2-All PAL below will not receive any payment.
 - [3] Scaling Factor [1] is the least severe penalty. [0] is the most severe penalty (straight line). [.6] is a good selection.

For Points 1 and 2, enter PAL as a percent between 100 to 0.

For Scaling Factor 3, enter as a decimal between 1.0 to 0.

After entering a new amount, the program will calculate and display a new pay factor formula and several PAL/Pay Factor points on the proposed curve for the operator's review and approval. This process can be continued until the operator is satisfied with the results. At this point, the operator must enter [S] to save the default values he has selected and wants to use for this airport project.

FAA PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENT CONSTRUCTION
SELECTION OF FORMULA DEFAULTS

NOTE: THIS PROGRAM IS FOR USE BY FEDERAL AVIATION ADMINISTRATION
TRAINED AND AUTHORIZED OFFICE PERSONNEL ONLY.

This program modifies the defaults in the pay adjustment schedules
for specific airport construction projects.

Minor changes inputting default points can cause drastic changes
and errors in the pay factor formula.

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PRESS [X] TO EXIT TO DOS - OR - [S] TO OPERATE THE PAP PROGRAM
- OR - ANY OTHER KEY TO CONTINUE WITH THIS PROGRAM.
RESPONSE REQUEST MODE

FIGURE I.1
SCREEN 1

FAA PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENT CONSTRUCTION
SELECTION OF FORMULA DEFAULTS

1. Airport: Norfolk International Airport
Norfolk, VA
ORF

2. Consultant/Engineer: R. Kenneth Weeks, Engineers
Norfolk, VA

3. FAA Contract Number: AIP #3-51-0036-06
FAA Project Name: Terminal Apron Expansion

4. FAA Material
Specification: P-501, PORTLAND CEMENT CONCRETE PAVEMENT

IS THE INFORMATION LISTED ABOVE CORRECT [Y] FOR YES
OR ENTER THE NUMBER CORRESPONDING TO REQUIRED CORRECTION
RESPONSE REQUEST MODE

FIGURE I.2
SCREEN 2

FAA PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENT CONSTRUCTION
SELECTION OF FORMULA DEFAULTS

1. P-501, PORTLAND CEMENT CONCRETE PAVEMENT

2. LOAD PAP PROGRAMS AND FILES.

3. EXIT THIS PROGRAM TO MS-DOS.

4. DESIGN TARGET SPECIFICATION IN PSI: 700

ENTER THE DESIRED DESIGN TARGET SPECIFICATION IN PSI <700>:

INPUT MODE

FIGURE I.3
SCREEN 3

FAA PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENT CONSTRUCTION
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

```
*****
1. THE LOWEST PWL IN PERCENT TO RECEIVE 100% PAYMENT: 90
2. THE LOWEST PWL IN PERCENT TO RECEIVE MINIMUM PAYMENT: 60
3. THE MINIMUM PAY FACTOR IN PERCENT TO RECEIVE PAYMENT: 50
3. THE MIDPOINT SCALING FACTOR BETWEEN [1] AND [-1]: .6
*****
PAY FACTOR FORMULA IS: -3.212007 *PWL^2 + 6.484677 *PWL + -2.234484
*****
PAY FACTOR CURVE POINTS BASED ON ABOVE INPUT POINTS:
POINT A - ABOVE 90 % PWL IS 100 % PAYMENT.
85 % PWL = 95.68 % PAY FACTOR
80 % PWL = 89.76 % PAY FACTOR
75 % PWL = 82.23 % PAY FACTOR
70 % PWL = 73.09 % PAY FACTOR
65 % PWL = 62.35 % PAY FACTOR
60 % PWL = 50.00 % PAY FACTOR
POINT B - BELOW 60 % PWL IS ZERO PAYMENT.
```

ENTER THE NUMBER CORRESPONDING TO THE REQUIRED CORRECTION POINT
- OR - ENTER [S] TO SAVE - OR - [M] TO RETURN TO MENU
RESPONSE REQUEST MODE

FIGURE I.4
SCREEN 4

8. Entering a [M] will return the program to the Material Selection Screen, Screen 3,
9. The operator can enter [2] to return to the PAP program,
OR
Enter [3] to EXIT to MS-DOS.
10. The operator can now generate a FIELD FAA-PAP disk. This disk will be used at the construction site to enter information and pavement test data.
11. Insert a formatted disk, without any files on it, into Drive B.
12. Computer must be at MS-DOS level with the A> prompt and the OFFICE FAA-PAP disk be inserted into Drive A.
13. Type [DISKCOPY A: B:] and press the [ENTER] key. Required files will COPY from the office disk to the field disk. Type [DEL B:FAACURVE.EXE] and press the [ENTER] key to remove the FAACURVE file from the Field disk.
14. Make backup copy of the new FIELD FAA-PAP disk by DISKCOPY command.
15. Label the new FIELD FAA-PAP as follows:

FIELD INFORMATION AND DATA for (airport and city/state)

Enter FAASTART to run program.

DATE: (Use date Field program was made).

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APPENDIX J
PAP TEST RESULTS - GREATER PITTSBURGH
INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT DEFAULTS FOR AIRPORT PAVEMENT CONSTRUCTION
P-501, Portland Cement Concrete Pavement
for Greater Pittsburgh International Airport

1. THE LOWEST PWL IN PERCENT TO RECEIVE 100% PAYMENT: 90
2. THE LOWEST PWL IN PERCENT TO RECEIVE MINIMUM PAYMENT: 60
THE MINIMUM PAY FACTOR IN PERCENT TO RECEIVE PAYMENT: 50
3. THE MIDPOINT SCALING FACTOR BETWEEN [1] AND [-1]: .6

PAY FACTOR FORMULA IS: $-3.212007 * PWL^2 + 6.484677 * PWL + -2.234484$

Press any key to return to program.
RESPONSE REQUEST MODE

APPENDIX J (Continued)
PAP TEST RESULTS - GREATER PITTSBURGH
INTERNATIONAL AIRPORT

FAA ACCEPTANCE AND PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENTS
P-501, Portland Cement Concrete Pavement

06-07-1990 PAGE 1

Airport: Greater Pittsburgh International Airport
Pittsburgh, PA
PIT

Consultant/Engineer:

Construction Contractor: Trumbull

Pavement Testing Laboratory: ACDA

FAA Contract Number: 7758
FAA Project Name: Midfield Terminal Project
Work Area Project Name: BP-02 N/S Taxiways and Tunnel

Pavement Specification: P-501, Portland Cement Concrete Pavement
Design Target Specification in PSI: 750

Method of Testing: Flexural Beam
ASTM Number:

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--|-------------|-----------|---------------|
| 1 | TW-A2 next to taxiway | 08/15/89 | 09/12/89 | 28 |
| 2 | TW-A2 Lane next to existing taxiway | 08/15/89 | 09/12/89 | 28 |
| 3 | TW-F Sta 13+90 to 34+25, CL to 25' left | 08/16/89 | 09/13/89 | 28 |
| 4 | TW-F Sta 13+90 to 34+25, CL to 25' left | 08/16/89 | 09/13/89 | 28 |
| 5 | TW-A N-1 A2 Stub Sta 21+00 to 21+50 | 08/17/89 | 09/14/89 | 28 |
| 6 | TW-F Sta 34+25 & TW-D Sta 42+50 | 08/18/89 | 09/15/89 | 28 |
| 7 | TW-F Sta 34+25 & TW-D Sta 42+50 | 08/18/89 | 09/15/89 | 28 |
| 8 | TW-D Sta 28+50 to 14+00, CL to 25' right | 08/21/89 | 09/18/89 | 28 |
| 9 | TW-D Sta 28+50 to 14+00, CL to 25' right | 08/21/89 | 09/18/89 | 28 |
| 10 | TW-F Sta 13+00 to 34+25, CL to 25' right | 08/22/89 | 09/19/89 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|------|------|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 1 | 760 | 755 | 760 | 745 | 0 | 0 | 755 | 7.071 | 0.707 | 73.6 | 79.8 |
| 2 | 770 | 750 | 785 | 745 | 0 | 0 | 763 | 18.484 | 0.676 | 72.5 | 77.9 |
| 3 | 775 | 750 | 750 | 755 | 0 | 0 | 758 | 11.902 | 0.630 | 71.0 | 75.1 |
| 4 | 765 | 750 | 760 | 780 | 0 | 0 | 764 | 12.500 | 1.00 | 86.7 | 97.3 |
| 5 | 770 | 760 | 740 | 780 | 760 | 765 | 763 | 13.323 | 0.938 | 82.0 | 92.4 |
| 6 | 730 | 790 | 700 | 820 | 0 | 0 | 760 | 54.772 | 0.183 | 56.1 | 0.0 |
| 7 | 745 | 755 | 765 | 750 | 0 | 0 | 754 | 8.539 | 0.439 | 64.6 | 61.5 |
| 8 | 945 | 920 | 1000 | 1010 | 0 | 0 | 969 | 43.277 | 5.055 | 100.0 | 100.0 |
| 9 | 890 | 910 | 865 | 890 | 0 | 0 | 889 | 18.428 | 7.529 | 100.0 | 100.0 |
| 10 | 950 | 905 | 880 | 890 | 0 | 0 | 906 | 30.923 | 5.053 | 100.0 | 100.0 |

APPENDIX J (Continued)
PAP TEST RESULTS - GREATER PITTSBURGH
INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 2

Airport: Greater Pittsburgh International Airport, Pittsburgh, PA

FAA Project Name: Midfield Terminal Project

Work Area Project Name: BP-02 N/S Taxiways and Tunnel

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--|-------------|-----------|---------------|
| 11 | TW-A Sta 20+75, 21+25 & 21+75 | 08/22/89 | 09/19/89 | 28 |
| 12 | TW-F Sta 34+25 to 42+50, CL to 25' right | 08/23/89 | 09/20/89 | 28 |
| 13 | TW-D Sta 42+50 to 29+00, CL to 25' left | 08/23/89 | 09/20/89 | 28 |
| 14 | TW-D Sta 29+00 to 14+00, CL to 25' left | 08/24/89 | 09/21/89 | 28 |
| 15 | TW-D Sta 29+00 to 14+00, CL to 25' left | 08/24/89 | 09/21/89 | 28 |
| 16 | TW-W Sta 12+75 to 13+75, D-F tie in | 08/25/89 | 09/22/89 | 28 |
| 17 | TW-W Sta 12+75, 13+25 & 13+75 | 08/25/89 | 09/22/89 | 28 |
| 18 | TW-A Sta 98+11 to 124+36, CL to 25' left | 08/26/89 | 09/23/89 | 28 |
| 19 | TW-A Sta 98+11 to 124+36, CL to 25' left | 08/26/89 | 09/23/89 | 28 |
| 20 | TW-W Sta 13+00 to 14+75, D-F tie in | 08/28/89 | 09/25/89 | 28 |
| 21 | TW-W Sta 13+00 to 14+75, D-F tie in | 08/28/89 | 09/25/89 | 28 |
| 22 | TW-R&W, D-F tie in | 08/29/89 | 09/26/89 | 28 |
| 23 | TW-R&W, D-F tie in | 08/29/89 | 09/26/89 | 28 |
| 24 | TW-W Sta 14+00 to 15+00, D-F tie in | 08/30/89 | 09/27/89 | 28 |
| 25 | TW-W Sta 14+00 to 15+00, D-F tie in | 08/30/89 | 09/27/89 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|------|------|------|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 11 | 930 | 935 | 975 | 905 | 0 | 0 | 936 | 28.976 | 6.428 | 100.0 | 100.0 |
| 12 | 985 | 920 | 890 | 895 | 950 | 950 | 932 | 36.696 | 4.951 | 100.0 | 100.0 |
| 13 | 875 | 850 | 850 | 950 | 0 | 0 | 881 | 47.324 | 2.773 | 100.0 | 100.0 |
| 14 | 775 | 930 | 965 | 935 | 0 | 0 | 901 | 85.574 | 1.767 | 100.0 | 100.0 |
| 15 | 855 | 870 | 930 | 995 | 0 | 0 | 913 | 63.836 | 2.546 | 100.0 | 100.0 |
| 16 | 870 | 905 | 1025 | 865 | 0 | 0 | 916 | 74.652 | 2.227 | 100.0 | 100.0 |
| 17 | 930 | 960 | 925 | 865 | 0 | 0 | 920 | 39.791 | 4.272 | 100.0 | 100.0 |
| 18 | 1025 | 1140 | 1080 | 1030 | 0 | 0 | 1069 | 53.599 | 5.947 | 100.0 | 100.0 |
| 19 | 905 | 1065 | 890 | 1015 | 0 | 0 | 969 | 84.988 | 2.574 | 100.0 | 100.0 |
| 20 | 805 | 725 | 830 | 845 | 0 | 0 | 801 | 53.444 | 0.959 | 82.0 | 92.3 |
| 21 | 920 | 885 | 890 | 780 | 0 | 0 | 869 | 61.152 | 1.942 | 100.0 | 100.0 |
| 22 | 800 | 815 | 830 | 815 | 0 | 0 | 815 | 12.247 | 5.307 | 100.0 | 100.0 |
| 23 | 865 | 870 | 760 | 815 | 0 | 0 | 828 | 51.397 | 1.508 | 100.0 | 100.0 |
| 24 | 905 | 915 | 1000 | 830 | 0 | 0 | 913 | 69.582 | 2.335 | 100.0 | 100.0 |
| 25 | 810 | 825 | 745 | 1015 | 0 | 0 | 849 | 116.145 | 0.850 | 78.3 | 87.4 |

APPENDIX J (Continued)
PAP TEST RESULTS - GREATER PITTSBURGH
INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 3

Airport: Greater Pittsburgh International Airport, Pittsburgh, PA

FAA Project Name: Midfield Terminal Project

Work Area Project Name: BP-02 N/S Taxiways and Tunnel

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--|-------------|-----------|---------------|
| 26 | TW-F Sta 39+00 to 15+00 | 08/31/89 | 09/28/89 | 28 |
| 27 | TW-F Sta 39+00 to 15+00 | 08/31/89 | 09/28/89 | 28 |
| 28 | TW-F Sta 37+50 | 09/02/89 | 09/30/89 | 28 |
| 29 | TW-F Sta 37+50 | 09/02/89 | 09/30/89 | 28 |
| 30 | TW-D Sta 42+00 to 15+00 | 09/05/89 | 10/03/89 | 28 |
| 31 | TW-D Sta 42+00 to 15+00 | 09/05/89 | 10/03/89 | 28 |
| 32 | TW-D Sta 13+00 to 42+00, 25' to 37' left | 09/06/89 | 10/04/89 | 28 |
| 33 | TW-D Sta 13+00 to 42+00 | 09/06/89 | 10/04/89 | 28 |
| 34 | TW-A Sta 98+00 to 124+00, CL to 25' right | 09/07/89 | 10/05/89 | 28 |
| 35 | TW-A Sta 98+00 to 124+00, CL to 25' right | 09/07/89 | 10/05/89 | 28 |
| 36 | TW-A Sta 98+00 to 124+00, CL to 25' left | 09/08/89 | 10/06/89 | 28 |
| 37 | TW-A Sta 98+00 to 124+00, CL to 25' left | 09/08/89 | 10/06/89 | 28 |
| 38 | TW-A Sta 124+00 to 129+00, CL to 25' right | 09/09/89 | 10/07/89 | 28 |
| 39 | TW-A Sta 124+00 to 129+00, CL to 25' right | 09/09/89 | 10/07/89 | 28 |
| 40 | TW-A Sta 98+00 to 129+10, 25' to 37' right | 09/11/89 | 10/09/89 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 26 | 905 | 865 | 910 | 905 | 0 | 0 | 896 | 20.966 | 6.976 | 100.0 | 100.0 |
| 27 | 890 | 900 | 910 | 935 | 0 | 0 | 909 | 19.311 | 8.221 | 100.0 | 100.0 |
| 28 | 905 | 815 | 865 | 890 | 0 | 0 | 869 | 39.449 | 3.010 | 100.0 | 100.0 |
| 29 | 930 | 825 | 890 | 935 | 0 | 0 | 895 | 50.827 | 2.853 | 100.0 | 100.0 |
| 30 | 755 | 840 | 885 | 865 | 0 | 0 | 836 | 57.209 | 1.508 | 100.0 | 100.0 |
| 31 | 855 | 825 | 905 | 930 | 0 | 0 | 879 | 47.500 | 2.711 | 100.0 | 100.0 |
| 32 | 910 | 980 | 920 | 895 | 0 | 0 | 926 | 37.277 | 4.728 | 100.0 | 100.0 |
| 33 | 950 | 920 | 950 | 0 | 0 | 0 | 940 | 17.321 | 10.970 | 100.0 | 100.0 |
| 34 | 760 | 785 | 870 | 715 | 0 | 0 | 783 | 65.128 | 0.499 | 66.6 | 66.0 |
| 35 | 780 | 805 | 885 | 865 | 0 | 0 | 834 | 49.392 | 1.696 | 100.0 | 100.0 |
| 36 | 775 | 780 | 785 | 0 | 0 | 0 | 780 | 5.000 | 6.000 | 100.0 | 100.0 |
| 37 | 785 | 765 | 855 | 770 | 0 | 0 | 794 | 41.708 | 1.049 | 85.0 | 95.6 |
| 38 | 795 | 810 | 810 | 810 | 0 | 0 | 806 | 7.500 | 7.500 | 100.0 | 100.0 |
| 39 | 815 | 790 | 810 | 795 | 0 | 0 | 803 | 11.902 | 4.411 | 100.0 | 100.0 |
| 40 | 720 | 715 | 760 | 800 | 0 | 0 | 749 | 39.660 | -0.032 | 48.9 | 0.0 |

APPENDIX J (Continued)
PAP TEST RESULTS - GREATER PITTSBURGH
INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 4

Airport: Greater Pittsburgh International Airport, Pittsburgh, PA

FAA Project Name: Midfield Terminal Project

Work Area Project Name: BP-02 N/S Taxiways and Tunnel

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--|-------------|-----------|---------------|
| 41 | TW-A Sta 98+00 to 129+10, 25' to 37' right | 09/11/89 | 10/09/89 | 28 |
| 42 | TW-D & F Sta 15+10 to 18+00 | 09/12/89 | 10/10/89 | 28 |
| 43 | TW-D & F Sta 15+10 to 18+00 | 09/12/89 | 10/10/89 | 28 |
| 44 | TW-D1 Sta 16+75 to 17+75 | 09/13/89 | 10/11/89 | 28 |
| 45 | TW-D1 Sta 16+75 to 17+75 | 09/13/89 | 10/11/89 | 28 |
| 46 | TW-D2 Sta 24+00 to 26+50 | 09/14/89 | 10/12/89 | 28 |
| 47 | TW-D2 Sta 24+00 to 26+50 | 09/14/89 | 10/12/89 | 28 |
| 48 | TW-D2 Sta 24+50 to 25+25 | 09/15/89 | 10/13/89 | 28 |
| 49 | TW-D2 Sta 24+50 to 25+25 | 09/15/89 | 10/13/89 | 28 |
| 50 | TW-A Sta 124+50 to 127+50 | 09/18/89 | 10/16/89 | 28 |
| 51 | TW-A Sta 124+50 to 127+50 | 09/18/89 | 10/16/89 | 28 |
| 52 | TW-D6 Sta 29+25 to 40+50 | 09/19/89 | 10/17/89 | 28 |
| 53 | TW-D6 Sta 29+25 to 40+50 | 09/19/89 | 10/17/89 | 28 |
| 54 | TW-D4 Sta 33+75 to 36+00 | 09/20/89 | 10/18/89 | 28 |
| 55 | TW-D4 Sta 33+75 to 36+00 | 09/20/89 | 10/18/89 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR | |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|--------|---------|--------------|-------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 41 | 800 | 760 | 825 | 765 | 0 | 0 | 788 | 30.687 | 1.222 | 90.7 | 100.0 |
| 42 | 795 | 800 | 910 | 860 | 0 | 0 | 841 | 54.524 | 1.674 | 100.0 | 100.0 |
| 43 | 805 | 815 | 810 | 810 | 0 | 0 | 810 | 4.082 | 14.690 | 100.0 | 100.0 |
| 44 | 830 | 825 | 870 | 795 | 0 | 0 | 830 | 30.822 | 2.596 | 100.0 | 100.0 |
| 45 | 745 | 755 | 805 | 835 | 0 | 0 | 785 | 42.426 | 0.825 | 77.5 | 86.2 |
| 46 | 835 | 840 | 735 | 775 | 0 | 0 | 796 | 50.394 | 0.918 | 80.6 | 90.5 |
| 47 | 840 | 810 | 910 | 910 | 0 | 0 | 868 | 50.580 | 2.323 | 100.0 | 100.0 |
| 48 | 870 | 900 | 845 | 975 | 0 | 0 | 898 | 56.347 | 2.618 | 100.0 | 100.0 |
| 49 | 860 | 920 | 760 | 835 | 0 | 0 | 844 | 66.254 | 1.415 | 97.2 | 100.0 |
| 50 | 735 | 820 | 785 | 815 | 0 | 0 | 789 | 39.025 | 0.993 | 83.1 | 93.6 |
| 51 | 735 | 815 | 810 | 795 | 0 | 0 | 789 | 36.827 | 1.052 | 85.1 | 95.8 |
| 52 | 730 | 735 | 765 | 830 | 0 | 0 | 765 | 46.007 | 0.326 | 60.9 | 52.3 |
| 53 | 810 | 710 | 780 | 775 | 0 | 0 | 769 | 42.106 | 0.445 | 64.8 | 62.0 |
| 54 | 810 | 850 | 840 | 805 | 0 | 0 | 826 | 22.127 | 3.446 | 100.0 | 100.0 |
| 55 | 745 | 740 | 815 | 760 | 0 | 0 | 765 | 34.400 | 0.436 | 64.5 | 61.3 |

APPENDIX J (Continued)
PAP TEST RESULTS - GREATER PITTSBURGH
INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 5

Airport: Greater Pittsburgh International Airport, Pittsburgh, PA

FAA Project Name: Midfield Terminal Project

Work Area Project Name: BP-02 N/S Taxiways and Tunnel

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------------------|-------------|-----------|---------------|
| 56 | TW-D & F Sta 25+50 to 26+75 | 09/21/89 | 10/19/89 | 28 |
| 57 | TW-D & F Sta 25+50 to 26+75 | 09/21/89 | 10/19/89 | 28 |
| 58 | TW-A2 Sta 22+25 to 23+25 | 09/22/89 | 10/20/89 | 28 |
| 59 | TW-A, D & F | 09/25/89 | 10/23/89 | 28 |
| 60 | TW-A, D & F | 09/25/89 | 10/23/89 | 28 |
| 61 | TW A, D & F | 09/26/89 | 10/24/89 | 28 |
| 62 | TW A, D & F | 09/27/89 | 10/25/89 | 28 |
| 63 | TW A, D & F | 09/27/89 | 10/25/89 | 28 |
| 64 | TW-D & F Sta 41+50 to 43+25 | 09/28/89 | 10/26/89 | 28 |
| 65 | TW A Sta 110+25 to 112+25 | 09/29/89 | 10/27/89 | 28 |
| 66 | TW A Sta 100+25 to 112+25 | 09/29/89 | 10/27/89 | 28 |
| 67 | TW-A Sta 108+00 to 116+00 | 09/30/89 | 10/28/89 | 28 |
| 68 | TW-A Sta 108+00 to 116+00 | 09/30/89 | 10/28/89 | 28 |
| 69 | Apron Sta 104+62 to 113+11 | 10/04/89 | 11/01/89 | 28 |
| 70 | Apron Sta 104+62 to 133+11 | 10/04/89 | 11/01/89 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | AVERAGE | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|------|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | | | | | |
| 56 | 750 | 755 | 765 | 750 | 0 | 0 | 755 | 7.071 | 0.707 | 73.6 | 79.8 |
| 57 | 755 | 745 | 790 | 770 | 0 | 0 | 765 | 19.579 | 0.766 | 75.5 | 83.1 |
| 58 | 810 | 780 | 830 | 780 | 0 | 0 | 800 | 24.495 | 2.041 | 100.0 | 100.0 |
| 59 | 845 | 890 | 755 | 755 | 0 | 0 | 811 | 67.500 | 0.907 | 80.2 | 90.1 |
| 60 | 695 | 820 | 810 | 735 | 0 | 0 | 765 | 60.139 | 0.249 | 58.3 | 0.0 |
| 61 | 810 | 905 | 745 | 835 | 900 | 810 | 834 | 60.779 | 1.385 | 93.1 | 100.0 |
| 62 | 765 | 670 | 755 | 810 | 0 | 0 | 750 | 58.452 | 0.000 | 50.0 | 0.0 |
| 63 | 720 | 815 | 1025 | 870 | 0 | 0 | 858 | 127.704 | 0.842 | 78.1 | 87.0 |
| 64 | 860 | 900 | 790 | 750 | 0 | 0 | 825 | 67.577 | 1.110 | 87.0 | 97.6 |
| 65 | 1010 | 890 | 845 | 815 | 0 | 0 | 890 | 85.732 | 1.633 | 100.0 | 100.0 |
| 66 | 720 | 790 | 810 | 800 | 0 | 0 | 780 | 40.825 | 0.735 | 74.5 | 81.4 |
| 67 | 810 | 830 | 790 | 770 | 0 | 0 | 800 | 25.820 | 1.936 | 100.0 | 100.0 |
| 68 | 930 | 790 | 980 | 830 | 0 | 0 | 883 | 87.702 | 1.511 | 100.0 | 100.0 |
| 69 | 805 | 785 | 765 | 815 | 0 | 0 | 793 | 22.174 | 1.917 | 100.0 | 100.0 |
| 70 | 695 | 880 | 840 | 815 | 0 | 0 | 808 | 79.635 | 0.722 | 74.1 | 80.6 |

APPENDIX J (Continued)
PAP TEST RESULTS - GREATER PITTSBURGH
INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 6

Airport: Greater Pittsburgh International Airport, Pittsburgh, PA

FAA Project Name: Midfield Terminal Project

Work Area Project Name: BP-02 N/S Taxiways and Tunnel

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|------------------------------|-------------|-----------|---------------|
| 71 | Offset Sta 104+62 to 113+11 | 10/05/89 | 11/02/89 | 28 |
| 72 | Offset Sta 104+62 to 113+11 | 10/05/89 | 11/02/89 | 28 |
| 73 | Apron Sta 104+62 to 113+11 | 10/06/89 | 11/03/89 | 28 |
| 74 | Apron Sta 104+62 to 113+11 | 10/06/89 | 11/03/89 | 28 |
| 75 | TW-A Sta 23+63 | 10/07/89 | 11/04/89 | 28 |
| 76 | TW-A Sta 23+63 | 10/07/89 | 11/04/89 | 28 |
| 77 | Staging Sta 104+62 to 113+11 | 10/09/89 | 11/06/89 | 28 |
| 78 | Staging Sta 104+62 to 113+11 | 10/09/89 | 11/06/89 | 28 |
| 79 | Staging Sta 107+98 to 113+11 | 10/10/89 | 11/07/89 | 28 |
| 80 | Staging Lanes 4 & 6 | 10/11/89 | 11/08/89 | 28 |
| 81 | Staging Lanes 4 & 6 | 10/11/89 | 11/08/89 | 28 |
| 82 | Staging Lanes 8 & 10 | 10/12/89 | 11/09/89 | 28 |
| 83 | Staging Lanes 8 & 10 | 10/12/89 | 11/09/89 | 28 |
| 84 | Staging Lane 12 | 10/13/89 | 11/10/89 | 28 |
| 85 | Staging Lane 12 | 10/13/89 | 11/10/89 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | AVERAGE | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|------|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | | | | | |
| 71 | 680 | 860 | 850 | 900 | 0 | 0 | 823 | 97.425 | 0.744 | 74.8 | 81.9 |
| 72 | 760 | 930 | 860 | 730 | 0 | 0 | 820 | 92.014 | 0.761 | 75.4 | 82.8 |
| 73 | 705 | 807 | 780 | 740 | 0 | 0 | 758 | 44.788 | 0.179 | 56.0 | 0.0 |
| 74 | 710 | 860 | 900 | 840 | 0 | 0 | 828 | 82.209 | 0.943 | 81.4 | 91.6 |
| 75 | 800 | 810 | 830 | 830 | 0 | 0 | 818 | 15.000 | 4.500 | 100.0 | 100.0 |
| 76 | 820 | 800 | 790 | 750 | 0 | 0 | 790 | 29.439 | 1.359 | 95.3 | 100.0 |
| 77 | 860 | 1020 | 850 | 950 | 0 | 0 | 920 | 80.416 | 2.114 | 100.0 | 100.0 |
| 78 | 810 | 880 | 900 | 740 | 0 | 0 | 833 | 72.744 | 1.134 | 87.8 | 98.3 |
| 79 | 790 | 910 | 760 | 760 | 795 | 795 | 802 | 55.557 | 0.930 | 81.8 | 92.1 |
| 80 | 755 | 680 | 810 | 870 | 0 | 0 | 779 | 80.868 | 0.356 | 61.9 | 54.8 |
| 81 | 730 | 770 | 840 | 860 | 0 | 0 | 800 | 60.553 | 0.826 | 77.5 | 86.2 |
| 82 | 740 | 790 | 800 | 830 | 0 | 0 | 790 | 37.417 | 1.069 | 85.6 | 96.3 |
| 83 | 820 | 840 | 780 | 730 | 0 | 0 | 793 | 48.563 | 0.875 | 79.2 | 88.6 |
| 84 | 738 | 840 | 750 | 775 | 0 | 0 | 776 | 45.522 | 0.566 | 68.9 | 70.8 |
| 85 | 850 | 935 | 795 | 740 | 0 | 0 | 830 | 83.167 | 0.962 | 82.1 | 92.4 |

APPENDIX J (Continued)
PAP TEST RESULTS - GREATER PITTSBURGH
INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

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Airport: Greater Pittsburgh International Airport, Pittsburgh, PA

FAA Project Name: Midfield Terminal Project

Work Area Project Name: BP-02 N/S Taxiways and Tunnel

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------|-------------|-----------|---------------|
|---------|-----------------|-------------|-----------|---------------|

| | | | | |
|-----|--------------------------------------|----------|----------|----|
| 86 | Staging Lane 14 Sta 109+11 to 104+64 | 10/14/89 | 11/11/89 | 28 |
| 87 | Staging Lane 14 Sta 109+11 to 104+62 | 10/14/89 | 11/11/89 | 28 |
| 88 | TW-A Sta 45+12 to 43+37 | 10/16/89 | 11/13/89 | 28 |
| 89 | TW-A Sta 45+12 to 43+37 | 10/16/89 | 11/13/89 | 28 |
| 90 | TW-W & Staging | 10/17/89 | 11/14/89 | 28 |
| 91 | TW-W & Staging | 10/17/89 | 11/14/89 | 28 |
| 92 | Station 43+34 to 44+89 | 10/18/89 | 11/15/89 | 28 |
| 93 | TW-A3 Lane A6 | 10/20/89 | 11/17/89 | 28 |
| 94 | TW-A3 Lane A6 | 10/20/89 | 11/17/89 | 28 |
| 95 | TW-A Sta 112+50 | 10/21/89 | 11/18/89 | 28 |
| 96 | D & A Connection | 10/23/89 | 11/20/89 | 28 |
| 97 | D & A Connection | 10/23/89 | 11/20/89 | 28 |
| 98 | TW-A Tie in | 10/24/89 | 11/21/89 | 28 |
| 99 | TW-A Tie in | 10/24/89 | 11/21/89 | 28 |
| 100 | TW-D & F Sta 124+50 | 10/25/89 | 11/22/89 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|------|------|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 86 | 840 | 810 | 830 | 790 | 0 | 0 | 818 | 22.174 | 3.044 | 100.0 | 100.0 |
| 87 | 770 | 790 | 845 | 780 | 0 | 0 | 796 | 33.510 | 1.380 | 96.0 | 100.0 |
| 88 | 835 | 745 | 695 | 845 | 0 | 0 | 780 | 72.342 | 0.415 | 63.8 | 59.6 |
| 89 | 730 | 930 | 765 | 720 | 0 | 0 | 786 | 97.756 | 0.371 | 62.4 | 56.0 |
| 90 | 860 | 850 | 1000 | 795 | 0 | 0 | 876 | 87.309 | 1.446 | 98.2 | 100.0 |
| 91 | 950 | 810 | 890 | 875 | 0 | 0 | 881 | 57.500 | 2.283 | 100.0 | 100.0 |
| 92 | 840 | 740 | 850 | 780 | 0 | 0 | 803 | 51.881 | 1.012 | 83.7 | 94.3 |
| 93 | 780 | 805 | 885 | 950 | 0 | 0 | 855 | 77.567 | 1.354 | 95.1 | 100.0 |
| 94 | 850 | 975 | 990 | 720 | 0 | 0 | 884 | 125.922 | 1.062 | 85.4 | 96.1 |
| 95 | 975 | 975 | 935 | 950 | 0 | 0 | 959 | 19.738 | 10.570 | 100.0 | 100.0 |
| 96 | 750 | 805 | 860 | 1105 | 0 | 0 | 880 | 156.578 | 0.830 | 77.7 | 86.5 |
| 97 | 835 | 950 | 860 | 845 | 0 | 0 | 873 | 52.678 | 2.325 | 100.0 | 100.0 |
| 98 | 690 | 795 | 720 | 800 | 0 | 0 | 751 | 54.829 | 0.023 | 50.8 | 0.0 |
| 99 | 755 | 760 | 790 | 850 | 0 | 0 | 789 | 43.661 | 0.888 | 79.6 | 89.2 |
| 100 | 870 | 900 | 930 | 920 | 0 | 0 | 905 | 26.458 | 5.858 | 100.0 | 100.0 |

APPENDIX J (Continued)
PAP TEST RESULTS - GREATER PITTSBURGH
INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

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Airport: Greater Pittsburgh International Airport, Pittsburgh, PA

FAA Project Name: Midfield Terminal Project

Work Area Project Name: BP-02 N/S Taxiways and Tunnel

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-------------------------------|-------------|-----------|---------------|
| 101 | TW-D & F Sta 124+50 | 10/25/89 | 11/22/89 | 28 |
| 102 | | 10/26/89 | 11/23/89 | 28 |
| 103 | | 10/26/89 | 11/23/89 | 28 |
| 104 | TW-A5 Sta 50+50 to 51+00 | 10/28/89 | 11/25/89 | 28 |
| 105 | TW-A5 Sta 50+50 to 51+00 | 10/28/89 | 11/25/89 | 28 |
| 106 | TW-A5 Sta 115+00 to 113+25 | 10/31/89 | 11/28/89 | 28 |
| 107 | TW-A5 Sta 115+00 to 113+25 | 10/31/89 | 11/28/89 | 28 |
| 108 | TW-N1 Sta 121+00 to 131+00 | 11/01/89 | 11/29/89 | 28 |
| 109 | TW-N1 Sta 47+25 to 130+90 | 11/04/89 | 12/02/89 | 28 |
| 110 | TW-N1 Sta 47+25 to 130+90 | 11/04/89 | 12/02/89 | 28 |
| 111 | TW-D & F Sta 128+25 to 123+75 | 11/07/89 | 12/05/89 | 28 |
| 112 | TW-D & F Sta 128+25 to 123+75 | 11/07/89 | 12/05/89 | 28 |
| 113 | TW-A-N1 Sta 128+12 to 128+37 | 11/20/89 | 12/18/89 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|------|-----|-----|----|----|---------|---------|--------|---------|--------------|
| | #1 | #2 | #3 | #4 | #5 | #6 | AVERAGE | | | | |
| 101 | 850 | 800 | 800 | 870 | 0 | 0 | 830 | 35.590 | 2.248 | 100.0 | 100.0 |
| 102 | 870 | 860 | 840 | 770 | 0 | 0 | 835 | 45.092 | 1.885 | 100.0 | 100.0 |
| 103 | 810 | 790 | 830 | 820 | 0 | 0 | 813 | 17.078 | 3.660 | 100.0 | 100.0 |
| 104 | 820 | 770 | 750 | 820 | 0 | 0 | 790 | 35.590 | 1.124 | 87.5 | 98.0 |
| 105 | 760 | 750 | 790 | 790 | 0 | 0 | 773 | 20.616 | 1.091 | 86.4 | 97.0 |
| 106 | 785 | 790 | 810 | 965 | 0 | 0 | 838 | 85.684 | 1.021 | 84.0 | 94.7 |
| 107 | 845 | 1040 | 820 | 755 | 0 | 0 | 865 | 122.678 | 0.937 | 81.2 | 91.4 |
| 108 | 805 | 795 | 775 | 795 | 0 | 0 | 793 | 12.583 | 3.378 | 100.0 | 100.0 |
| 109 | 790 | 735 | 790 | 865 | 0 | 0 | 795 | 53.385 | 0.843 | 78.1 | 87.1 |
| 110 | 775 | 760 | 885 | 920 | 0 | 0 | 835 | 79.477 | 1.069 | 85.6 | 96.3 |
| 111 | 870 | 850 | 890 | 805 | 0 | 0 | 854 | 36.372 | 2.852 | 100.0 | 100.0 |
| 112 | 940 | 900 | 855 | 770 | 0 | 0 | 866 | 72.958 | 1.593 | 100.0 | 100.0 |
| 113 | 760 | 870 | 920 | 0 | 0 | 0 | 850 | 81.854 | 1.222 | 100.0 | 100.0 |

APPENDIX K
PAP TEST RESULTS - BY LOTS
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT DEFAULTS FOR AIRPORT PAVEMENT CONSTRUCTION
P-501, PORTLAND CEMENT CONCRETE PAVEMENT
for Norfolk International Airport

1. THE LOWEST PWL IN PERCENT TO RECEIVE 100% PAYMENT: 90
2. THE LOWEST PWL IN PERCENT TO RECEIVE MINIMUM PAYMENT: 60
THE MINIMUM PAY FACTOR IN PERCENT TO RECEIVE PAYMENT: 50
3. THE MIDPOINT SCALING FACTOR BETWEEN [1] AND [-1]: .6

PAY FACTOR FORMULA IS: $-3.212007 * PWL^2 + 6.484677 * PWL + -2.234484$

Press any key to return to program.
RESPONSE REQUEST MODE

APPENDIX K (Continued)
PAP TEST RESULTS - BY LOTS
NORFOLK INTERNATIONAL AIRPORT

FAA ACCEPTANCE AND PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENTS
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 1

Airport: Norfolk International Airport
Norfolk, VA
ORF

Consultant/Engineer: R. Kenneth Weeks, Engineers
Norfolk, VA

Construction Contractor: Williams Corp. of Va.
Norfolk, VA

Pavement Testing Laboratory: ATEL Associates of Va., Inc.
Norfolk, VA

FAA Contract Number: AIP #3-51-0036-06

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Apron Expansion, 1988

Pavement Specification: P-501, PORTLAND CEMENT CONCRETE PAVEMENT

Design Target Specification in PSI: 700

Method of Testing: Flexural Strength Beams

ASTM Number: ASTM-C-78

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|---------------------------------|-------------|-----------|---------------|
| 1 | Lane #1, north end at 0+80 | 11/24/87 | 12/22/87 | 28 |
| 2 | Lane #1, north end | 11/24/87 | 12/22/87 | 28 |
| 3 | Lane #3, north end at 0+80 | 11/25/87 | 12/23/87 | 28 |
| 4 | Lane #3, north end at 0+330 | 11/25/87 | 12/23/87 | 28 |
| 5 | Lane #5, north end | 11/30/87 | 12/28/87 | 28 |
| 6 | 0+330 Ft | 11/30/87 | 12/28/87 | 28 |
| 7 | Lane #7, north end at 0+80 | 12/02/87 | 12/30/87 | 28 |
| 8 | north end at 0+240 | 12/03/87 | 01/05/88 | 33 |
| 9 | Lane #9, north end, 0+130 yards | 12/07/87 | 01/05/88 | 29 |
| 10 | Lane #9, north end 0+370 | 12/07/87 | 01/05/88 | 29 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 1 | 655 | 660 | 705 | 710 | 0 | 0 | 683 | 29.011 | -0.603 | 29.9 | 0.0 |
| 2 | 775 | 750 | 795 | 785 | 0 | 0 | 776 | 19.311 | 3.949 | 100.0 | 100.0 |
| 3 | 720 | 715 | 810 | 890 | 0 | 0 | 784 | 83.204 | 1.007 | 83.6 | 94.1 |
| 4 | 720 | 710 | 785 | 790 | 0 | 0 | 751 | 42.106 | 1.217 | 90.6 | 100.0 |
| 5 | 675 | 730 | 735 | 780 | 0 | 0 | 730 | 43.012 | 0.697 | 73.2 | 79.2 |
| 6 | 745 | 740 | 765 | 807 | 0 | 0 | 764 | 30.478 | 2.108 | 100.0 | 100.0 |
| 7 | 750 | 720 | 770 | 810 | 0 | 0 | 763 | 37.749 | 1.656 | 100.0 | 100.0 |
| 8 | 730 | 764 | 815 | 830 | 0 | 0 | 785 | 46.155 | 1.836 | 100.0 | 100.0 |
| 9 | 730 | 740 | 760 | 795 | 0 | 0 | 756 | 28.687 | 1.961 | 100.0 | 100.0 |
| 10 | 780 | 750 | 815 | 800 | 0 | 0 | 786 | 28.100 | 3.069 | 100.0 | 100.0 |

APPENDIX K (Continued)
PAP TEST RESULTS - BY LOTS
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 2

Airport: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Apron Expansion, 1988

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--|-------------|-----------|---------------|
| 11 | 3rd slab from west, 66' from north to south | 12/08/87 | 01/05/88 | 28 |
| 12 | 3rd slab from west, 254' from north to south | 12/08/87 | 01/05/88 | 28 |
| 13 | Lane #11, North end 0+250 yds | 12/10/87 | 01/07/88 | 28 |
| 14 | Lane #11, north end, 0+410 ft | 12/10/87 | 01/07/88 | 28 |
| 15 | Lane #11, north end, 0+90 | 12/11/87 | 01/08/88 | 28 |
| 16 | Lane #11 | 12/11/87 | 01/08/88 | 28 |
| 17 | Lane #2, near runway, north end 0+100 | 12/12/87 | 12/26/87 | 14 |
| 18 | Lane #2, north end 0+320 | 12/12/87 | 12/26/87 | 14 |
| 19 | Lane #4, north end, 0+115 ft | 12/14/87 | 12/28/87 | 14 |
| 20 | Lane #4, north end 0+390 ft | 12/14/87 | 12/28/87 | 14 |
| 21 | Lane #6, north end 0+130 ft | 12/16/87 | 01/13/88 | 28 |
| 22 | Lane #6, 0+390 | 12/16/87 | 01/13/88 | 28 |
| 23 | Lane #8, north end, 0+95 ft | 12/17/87 | 01/14/88 | 28 |
| 24 | Lane #8, 0+245 ft | 12/18/87 | 01/15/88 | 28 |
| 25 | Lane #8, 0+366 ft | 12/18/87 | 01/15/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR | |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|--------|---------|--------------|-------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 11 | 695 | 680 | 735 | 755 | 0 | 0 | 716 | 34.731 | 0.468 | 65.6 | 63.7 |
| 12 | 725 | 700 | 810 | 850 | 0 | 0 | 771 | 70.519 | 1.010 | 83.7 | 94.3 |
| 13 | 735 | 716 | 790 | 830 | 0 | 0 | 768 | 52.028 | 1.302 | 93.4 | 100.0 |
| 14 | 695 | 695 | 750 | 720 | 0 | 0 | 715 | 26.141 | 0.574 | 69.1 | 71.3 |
| 15 | 725 | 669 | 780 | 760 | 0 | 0 | 734 | 48.638 | 0.689 | 73.0 | 78.7 |
| 16 | 675 | 750 | 730 | 810 | 0 | 0 | 741 | 55.734 | 0.740 | 74.7 | 81.7 |
| 17 | 585 | 620 | 670 | 670 | 0 | 0 | 636 | 41.508 | -1.536 | 0.0 | 0.0 |
| 18 | 660 | 640 | 720 | 725 | 0 | 0 | 686 | 42.696 | -0.322 | 39.3 | 0.0 |
| 19 | 640 | 620 | 715 | 684 | 0 | 0 | 665 | 42.859 | -0.822 | 22.6 | 0.0 |
| 20 | 675 | 655 | 745 | 700 | 0 | 0 | 694 | 38.810 | -0.161 | 44.6 | 0.0 |
| 21 | 670 | 720 | 760 | 790 | 0 | 0 | 735 | 51.962 | 0.674 | 72.5 | 77.8 |
| 22 | 670 | 712 | 790 | 710 | 0 | 0 | 721 | 50.210 | 0.408 | 63.6 | 59.1 |
| 23 | 775 | 745 | 760 | 770 | 0 | 0 | 763 | 13.229 | 4.725 | 100.0 | 100.0 |
| 24 | 710 | 740 | 795 | 780 | 0 | 0 | 756 | 38.595 | 1.457 | 98.6 | 100.0 |
| 25 | 830 | 880 | 940 | 955 | 0 | 0 | 901 | 57.500 | 3.500 | 100.0 | 100.0 |

APPENDIX K (Continued)
PAP TEST RESULTS - BY LOTS
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 3

Airport: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Apron Expansion, 1988

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--|-------------|-----------|---------------|
| 26 | Lane #8, north end 0+150 ft | 12/21/87 | 01/18/88 | 28 |
| 27 | Lane #10, north end, 3+35 | 01/04/88 | 02/01/88 | 28 |
| 28 | Lane #10, from 0+00 to 0+50 | 01/13/88 | 02/10/88 | 28 |
| 29 | Lane #12, north end 100+30 ft | 01/19/88 | 02/16/88 | 28 |
| 30 | Lane #12, north end, 3+10 ft | 01/19/88 | 02/16/88 | 28 |
| 31 | Lane #12, north end, 4+10 ft | 01/21/88 | 02/04/88 | 14 |
| 32 | Lane #14, east end, 1+10 ft | 01/22/88 | 02/19/88 | 28 |
| 33 | Area #2, center cross lane, seq. #2 | 02/01/88 | 02/29/88 | 28 |
| 34 | Lane #2, area #3, east end, 0+85 ft | 02/09/88 | 03/08/88 | 28 |
| 35 | Lane #2, area #3, east end, 1+95 ft | 02/09/88 | 03/08/88 | 28 |
| 36 | Lane #4, south side, east end, 0+85 ft | 02/10/88 | 03/09/88 | 28 |
| 37 | Lane #4, area #3, south side, east end 1+98 ft | 02/10/88 | 03/09/88 | 28 |
| 38 | Area #2, lane #3, east end 0+95 | 02/15/88 | 03/14/88 | 28 |
| 39 | Lane #3, area #2, east end, 1+15 ft | 02/17/88 | 03/16/88 | 28 |
| 40 | Area #2, Lane #4, East of 3+40' | 02/17/88 | 03/16/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI----- | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR | |
|---------|----------------------------------|-----|-----|-----|-----|-----|---------|--------|---------|--------------|-------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 26 | 710 | 720 | 790 | 740 | 0 | 0 | 740 | 35.590 | 1.124 | 87.5 | 98.0 |
| 27 | 720 | 700 | 695 | 745 | 0 | 0 | 715 | 22.730 | 0.660 | 72.0 | 76.9 |
| 28 | 720 | 770 | 830 | 810 | 0 | 0 | 783 | 48.563 | 1.699 | 100.0 | 100.0 |
| 29 | 759 | 750 | 825 | 790 | 0 | 0 | 781 | 33.971 | 2.384 | 100.0 | 100.0 |
| 30 | 662 | 638 | 720 | 740 | 0 | 0 | 690 | 47.917 | -0.209 | 43.0 | 0.0 |
| 31 | 600 | 640 | 760 | 760 | 0 | 0 | 690 | 82.462 | -0.121 | 46.0 | 0.0 |
| 32 | 750 | 670 | 745 | 770 | 0 | 0 | 734 | 43.851 | 0.770 | 75.7 | 83.3 |
| 33 | 670 | 690 | 810 | 880 | 0 | 0 | 763 | 99.791 | 0.626 | 70.9 | 74.8 |
| 34 | 875 | 790 | 860 | 880 | 0 | 0 | 851 | 41.708 | 3.626 | 100.0 | 100.0 |
| 35 | 720 | 730 | 810 | 810 | 0 | 0 | 768 | 49.244 | 1.371 | 95.7 | 100.0 |
| 36 | 700 | 685 | 760 | 785 | 0 | 0 | 733 | 47.697 | 0.681 | 72.7 | 78.2 |
| 37 | 710 | 710 | 780 | 770 | 0 | 0 | 743 | 37.749 | 1.126 | 87.5 | 98.1 |
| 38 | 700 | 730 | 825 | 805 | 0 | 0 | 765 | 59.582 | 1.091 | 86.4 | 97.0 |
| 39 | 770 | 760 | 830 | 800 | 0 | 0 | 790 | 31.623 | 2.846 | 100.0 | 100.0 |
| 40 | 720 | 760 | 780 | 850 | 0 | 0 | 778 | 54.391 | 1.425 | 97.5 | 100.0 |

APPENDIX K (Continued)
PAP TEST RESULTS - BY LOTS
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 4

Airport: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Apron Expansion, 1988

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--------------------------------------|-------------|-----------|---------------|
| 41 | Lane #1, area #2, east end, 0+88 ft | 02/18/88 | 03/17/88 | 28 |
| 42 | Lane #1, area #2, east end, 2+90 ft | 02/18/88 | 03/17/88 | 28 |
| 43 | Area #3, Lane #1, East end 0+65' | 02/22/88 | 03/21/88 | 28 |
| 44 | Lane #1, area #3, 1+95 ft | 02/22/88 | 03/21/88 | 28 |
| 45 | Lane #3, area #7, east end, 0+40 | 02/23/88 | 03/22/88 | 28 |
| 46 | Lane #3, area #3, 1+95 ft | 02/23/88 | 03/22/88 | 28 |
| 48 | Area #3, lane #6, east end 0+93 ft | 03/02/88 | 03/30/88 | 28 |
| 49 | Lane #6, area #3, east end, 1+98 ft | 03/02/88 | 03/30/88 | 28 |
| 50 | Lane #8, area #3, east end, 0+78 ft | 03/03/88 | 03/31/88 | 28 |
| 51 | Lane #8, area #3, east end, 1+95 ft | 03/03/88 | 03/31/88 | 28 |
| 52 | Lane #10, area #3, 0+70 ft | 03/07/88 | 04/04/88 | 28 |
| 53 | Lane #10, area #3, 1+98 ft | 03/07/88 | 04/04/88 | 28 |
| 54 | Lane #12, area #3, east end, 0+18 ft | 03/08/88 | 04/05/88 | 28 |
| 55 | Lane #12, area #3, 0+52 ft | 03/08/88 | 04/05/88 | 28 |
| 56 | Lane #5, area #3, 0+60 ft | 03/09/88 | 04/06/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PNL | % PAY FACTOR | |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|---------|--------------|-------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 41 | 720 | 720 | 830 | 800 | 0 | 0 | 768 | 56.199 | 1.201 | 90.0 | 100.0 |
| 42 | 610 | 675 | 695 | 710 | 0 | 0 | 673 | 44.064 | -0.624 | 29.2 | 0.0 |
| 43 | 770 | 850 | 880 | 865 | 0 | 0 | 841 | 49.054 | 2.880 | 100.0 | 100.0 |
| 44 | 700 | 650 | 780 | 770 | 0 | 0 | 725 | 61.373 | 0.407 | 63.6 | 59.0 |
| 45 | 680 | 705 | 760 | 810 | 0 | 0 | 739 | 58.077 | 0.667 | 72.2 | 77.4 |
| 46 | 630 | 640 | 730 | 720 | 0 | 0 | 680 | 52.281 | -0.383 | 37.2 | 0.0 |
| 48 | 870 | 810 | 890 | 920 | 0 | 0 | 873 | 46.458 | 3.713 | 100.0 | 100.0 |
| 49 | 740 | 760 | 800 | 800 | 0 | 0 | 775 | 30.000 | 2.500 | 100.0 | 100.0 |
| 50 | 850 | 835 | 870 | 900 | 0 | 0 | 864 | 28.100 | 5.828 | 100.0 | 100.0 |
| 51 | 710 | 725 | 800 | 815 | 0 | 0 | 763 | 52.678 | 1.186 | 89.5 | 99.7 |
| 52 | 820 | 755 | 855 | 860 | 0 | 0 | 823 | 48.391 | 2.531 | 100.0 | 100.0 |
| 53 | 630 | 650 | 760 | 705 | 0 | 0 | 686 | 58.506 | -0.235 | 42.2 | 0.0 |
| 54 | 720 | 700 | 860 | 835 | 0 | 0 | 779 | 80.454 | 0.979 | 82.6 | 93.1 |
| 55 | 760 | 730 | 860 | 890 | 0 | 0 | 810 | 77.028 | 1.428 | 97.6 | 100.0 |
| 56 | 670 | 720 | 905 | 820 | 0 | 0 | 779 | 104.752 | 0.752 | 75.1 | 82.3 |

APPENDIX K (Continued)
PAP TEST RESULTS - BY LOTS
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 5

Airport: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Apron Expansion, 1988

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|---|-------------|-----------|---------------|
| 57 | Lane #5, area #3, 1+80 ft | 03/09/88 | 04/06/88 | 28 |
| 58 | Area #3, Lane #7, 0+90' | 03/11/88 | 04/08/88 | 28 |
| 59 | Lane #7, area #7, east end, 1+95 | 03/11/88 | 04/08/88 | 28 |
| 60 | Lane #9, area #3, east end, 0+96 ft | 03/23/88 | 04/20/88 | 28 |
| 61 | Lane #9, area #3, east end, 1+95 | 03/23/88 | 04/20/88 | 28 |
| 62 | Lane #11, area #3, east end, 0+58 | 03/24/88 | 04/21/88 | 28 |
| 63 | Lane #11, area #3, east end, 1+42 ft | 03/24/88 | 04/21/88 | 28 |
| 64 | Area #4, Lane #15, North end, 0+75' | 03/30/88 | 04/27/88 | 28 |
| 65 | Lane #15, area #4, north end, 3+90 ft | 03/30/88 | 04/27/88 | 28 |
| 66 | Lane #16, area #4, north end, 0+70 ft | 04/05/88 | 05/03/88 | 28 |
| 67 | Lane #16, area #4, north end, 4+40 ft | 04/05/88 | 05/03/88 | 28 |
| 68 | Lane #14, area #4, from 10 ft side, 3+66 ft | 04/05/88 | 05/03/88 | 28 |
| 69 | Area #4, lane #14, north end, 2+68 ft | 04/06/88 | 05/04/88 | 28 |
| 70 | Lane #14, area #4, north end 5+95 ft | 04/06/88 | 05/04/88 | 28 |
| 73 | Lane #3, northeast area, at northeast 1/3 | 09/20/88 | 10/18/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 57 | 800 | 730 | 840 | 800 | 0 | 0 | 793 | 45.735 | 2.023 | 100.0 | 100.0 |
| 58 | 710 | 710 | 820 | 910 | 0 | 0 | 788 | 96.738 | 0.905 | 80.2 | 90.0 |
| 59 | 700 | 690 | 780 | 800 | 0 | 0 | 743 | 55.603 | 0.764 | 75.5 | 83.0 |
| 60 | 670 | 700 | 820 | 840 | 0 | 0 | 758 | 85.000 | 0.676 | 72.5 | 77.9 |
| 61 | 630 | 715 | 850 | 810 | 0 | 0 | 751 | 98.689 | 0.519 | 67.3 | 67.5 |
| 62 | 720 | 670 | 780 | 740 | 0 | 0 | 728 | 45.735 | 0.601 | 70.0 | 73.2 |
| 63 | 710 | 620 | 730 | 740 | 0 | 0 | 700 | 54.772 | 0.000 | 50.0 | 0.0 |
| 64 | 600 | 680 | 776 | 798 | 0 | 0 | 714 | 91.380 | 0.148 | 54.9 | 0.0 |
| 65 | 730 | 730 | 761 | 714 | 0 | 0 | 734 | 19.670 | 1.716 | 100.0 | 100.0 |
| 66 | 730 | 730 | 800 | 830 | 0 | 0 | 773 | 50.580 | 1.433 | 97.8 | 100.0 |
| 67 | 670 | 660 | 800 | 800 | 0 | 0 | 733 | 78.049 | 0.416 | 63.9 | 59.7 |
| 68 | 820 | 730 | 840 | 780 | 0 | 0 | 793 | 48.563 | 1.905 | 100.0 | 100.0 |
| 69 | 660 | 630 | 730 | 725 | 0 | 0 | 686 | 49.223 | -0.279 | 40.7 | 0.0 |
| 70 | 670 | 650 | 760 | 720 | 0 | 0 | 700 | 49.666 | 0.000 | 50.0 | 0.0 |
| 73 | 660 | 600 | 720 | 750 | 0 | 0 | 683 | 66.521 | -0.263 | 41.2 | 0.0 |

APPENDIX K (Continued)
PAP TEST RESULTS - BY LOTS
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 6

Airport: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Apron Expansion, 1988

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------------------------|-------------|-----------|---------------|
| 74 | Lane #3 southeast, 30 ft from end | 09/20/88 | 10/18/88 | 28 |
| 75 | Lane #5, 6+30 on east end | 09/21/88 | 10/19/88 | 28 |
| 76 | Lane #5, 4+80 on west end | 09/21/88 | 10/19/88 | 28 |
| 77 | Lane #7, 780 to 690 | 10/03/88 | 10/31/88 | 28 |
| 78 | Lane #7 | 10/05/88 | 11/02/88 | 28 |
| 79 | Lane #7 | 10/05/88 | 11/02/88 | 28 |
| 80 | Lane #9 | 10/05/88 | 11/02/88 | 28 |
| 81 | Lane #9 | 10/06/88 | 11/03/88 | 28 |
| 82 | Lane #11, west end | 10/07/88 | 11/04/88 | 28 |
| 83 | Lane #11, east end | 10/07/88 | 11/04/88 | 28 |
| 84 | Lane #2, east end | 10/08/88 | 11/05/88 | 28 |
| 85 | Lane #2, west end | 10/08/88 | 11/05/88 | 28 |
| 86 | Lane #4, east end | 10/10/88 | 11/07/88 | 28 |
| 87 | Lane #4, west end | 10/10/88 | 11/07/88 | 28 |
| 88 | Lane #8, at 65 ft | 10/12/88 | 11/09/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR | |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|---------|--------------|------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 74 | 660 | 610 | 780 | 775 | 0 | 0 | 706 | 84.791 | 0.074 | 52.5 | 0.0 |
| 75 | 670 | 690 | 710 | 840 | 0 | 0 | 728 | 76.757 | 0.358 | 61.9 | 55.0 |
| 76 | 730 | 630 | 860 | 870 | 0 | 0 | 773 | 114.419 | 0.634 | 71.1 | 75.3 |
| 77 | 600 | 620 | 860 | 830 | 0 | 0 | 728 | 136.473 | 0.202 | 56.7 | 0.0 |
| 78 | 640 | 710 | 730 | 0 | 0 | 0 | 693 | 47.258 | -0.141 | 46.1 | 0.0 |
| 79 | 550 | 730 | 790 | 0 | 0 | 0 | 690 | 124.900 | -0.080 | 47.8 | 0.0 |
| 80 | 660 | 860 | 930 | 0 | 0 | 0 | 817 | 140.119 | 0.833 | 75.6 | 83.3 |
| 81 | 620 | 665 | 750 | 780 | 0 | 0 | 704 | 74.092 | 0.051 | 51.7 | 0.0 |
| 82 | 605 | 540 | 830 | 820 | 0 | 0 | 699 | 148.233 | -0.008 | 49.7 | 0.0 |
| 83 | 605 | 620 | 700 | 790 | 0 | 0 | 679 | 85.086 | -0.250 | 41.7 | 0.0 |
| 84 | 600 | 685 | 901 | 910 | 0 | 0 | 774 | 155.801 | 0.475 | 65.8 | 64.2 |
| 85 | 700 | 770 | 715 | 740 | 0 | 0 | 731 | 30.653 | 1.019 | 84.0 | 94.6 |
| 86 | 680 | 640 | 875 | 735 | 0 | 0 | 733 | 102.673 | 0.317 | 60.6 | 51.4 |
| 87 | 610 | 820 | 800 | 0 | 0 | 0 | 743 | 115.902 | 0.374 | 60.5 | 51.3 |
| 88 | 620 | 580 | 840 | 920 | 0 | 0 | 740 | 165.731 | 0.241 | 58.0 | 0.0 |

APPENDIX K (Continued)
PAP TEST RESULTS - BY LOTS
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 7

Airport: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Apron Expansion, 1988

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--------------------------|-------------|-----------|---------------|
| 89 | Lane #8, west end | 10/12/88 | 11/09/88 | 28 |
| 90 | Lane #6, east end | 10/13/88 | 11/10/88 | 28 |
| 91 | Lane #6, west end | 10/13/88 | 11/10/88 | 28 |
| 92 | Lane #8, east end | 10/14/88 | 11/11/88 | 28 |
| 93 | Lane #8, west end | 10/14/88 | 11/11/88 | 28 |
| 94 | Lane #10, west end | 10/15/88 | 11/12/88 | 28 |
| 95 | Lane #10, east end | 10/15/88 | 11/12/88 | 28 |
| 96 | Lane #12, east end | 10/17/88 | 11/14/88 | 28 |
| 97 | Lane #12, west end | 10/17/88 | 11/14/88 | 28 |
| 98 | Lane #2, north end, 0-25 | 10/18/88 | 11/15/88 | 28 |
| 99 | Lane #2, south end, 0-25 | 10/18/88 | 11/15/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 89 | 530 | 580 | 890 | 830 | 0 | 0 | 708 | 178.955 | 0.042 | 51.4 | 0.0 |
| 90 | 620 | 710 | 980 | 850 | 0 | 0 | 790 | 158.114 | 0.569 | 69.0 | 71.0 |
| 91 | 600 | 690 | 800 | 840 | 0 | 0 | 733 | 108.743 | 0.299 | 60.0 | 0.0 |
| 92 | 635 | 610 | 880 | 810 | 0 | 0 | 734 | 131.996 | 0.256 | 58.5 | 0.0 |
| 93 | 610 | 615 | 760 | 860 | 0 | 0 | 711 | 121.132 | 0.093 | 53.1 | 0.0 |
| 94 | 595 | 610 | 910 | 810 | 0 | 0 | 731 | 154.293 | 0.203 | 56.8 | 0.0 |
| 95 | 745 | 670 | 800 | 820 | 0 | 0 | 759 | 67.129 | 0.875 | 79.2 | 88.6 |
| 96 | 575 | 575 | 750 | 790 | 0 | 0 | 673 | 113.761 | -0.242 | 41.9 | 0.0 |
| 97 | 600 | 630 | 750 | 780 | 0 | 0 | 690 | 88.318 | -0.113 | 46.2 | 0.0 |
| 98 | 505 | 505 | 830 | 920 | 0 | 0 | 690 | 216.756 | -0.046 | 48.5 | 0.0 |
| 99 | 525 | 510 | 825 | 855 | 0 | 0 | 679 | 186.698 | -0.114 | 46.2 | 0.0 |

APPENDIX L
PAP TEST RESULTS - 28 DAYS ONLY
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT DEFAULTS FOR AIRPORT PAVEMENT CONSTRUCTION
P-501, PORTLAND CEMENT CONCRETE PAVEMENT
for Norfolk International Airport

1. THE LOWEST PWL IN PERCENT TO RECEIVE 100% PAYMENT: 90
2. THE LOWEST PWL IN PERCENT TO RECEIVE MINIMUM PAYMENT: 60
THE MINIMUM PAY FACTOR IN PERCENT TO RECEIVE PAYMENT: 50
3. THE MIDPOINT SCALING FACTOR BETWEEN [1] AND [-1]: .6

PAY FACTOR FORMULA IS: $-3.212007 * PWL^2 + 6.484677 * PWL + -2.234484$

Press any key to return to program.
RESPONSE REQUEST MODE

APPENDIX L (Continued)
PAP TEST RESULTS - 28 DAYS ONLY
NORFOLK INTERNATIONAL AIRPORT

FAA ACCEPTANCE AND PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENTS
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990 PAGE 1

Airport: Norfolk International Airport
Norfolk, VA
ORF

Consultant/Engineer: R. Kenneth Weeks, Engineers
Norfolk, VA

Construction Contractor: Williams Corp. of Va.
Norfolk, VA

Pavement Testing Laboratory: ATEL Associates of Va., Inc.
Norfolk, VA

FAA Contract Number: AIP #3-51-0036-06
FAA Project Name: Terminal Apron Expansion
Work Area Project Name: Only 28-day tests

Pavement Specification: P-501, PORTLAND CEMENT CONCRETE PAVEMENT
Design Target Specification in PSI: 700

Method of Testing: Flexural Strength Beams
' ASTM Number: ASTM-C-78

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------|-------------|-----------|---------------|
| 1 | Lot 1 & 2 | 11/24/87 | 12/22/87 | 28 |
| 2 | Lot 3 & 4 | 11/25/87 | 12/23/87 | 28 |
| 3 | Lot 5 & 6 | 11/30/87 | 12/28/87 | 28 |
| 4 | Lot 7 & 8 | 12/02/87 | 12/30/87 | 28 |
| 5 | Lot 9 & 10 | 12/07/87 | 01/05/88 | 29 |
| 6 | Lots 11 & 12 | 12/08/87 | 01/05/88 | 28 |
| 7 | Lots 13 & 14 | 12/10/87 | 01/07/88 | 28 |
| 8 | Lots 15 & 16 | 12/11/87 | 01/08/88 | 28 |
| 11 | Lots 21 & 22 | 12/16/87 | 01/13/88 | 28 |
| 12 | Lot 23 | 12/17/87 | 01/14/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI----- | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|----------------------------------|-----|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 1 | 705 | 710 | 795 | 785 | 0 | 0 | 749 | 47.850 | 1.019 | 84.0 | 94.6 |
| 2 | 810 | 890 | 785 | 790 | 0 | 0 | 819 | 48.713 | 2.438 | 100.0 | 100.0 |
| 3 | 735 | 780 | 765 | 807 | 0 | 0 | 772 | 30.037 | 2.389 | 100.0 | 100.0 |
| 4 | 770 | 810 | 815 | 830 | 0 | 0 | 806 | 25.617 | 4.148 | 100.0 | 100.0 |
| 5 | 760 | 795 | 815 | 800 | 0 | 0 | 793 | 23.274 | 3.974 | 100.0 | 100.0 |
| 6 | 735 | 755 | 810 | 850 | 0 | 0 | 788 | 52.361 | 1.671 | 100.0 | 100.0 |
| 7 | 790 | 830 | 750 | 720 | 0 | 0 | 773 | 47.871 | 1.514 | 100.0 | 100.0 |
| 8 | 780 | 760 | 730 | 810 | 0 | 0 | 770 | 33.665 | 2.079 | 100.0 | 100.0 |
| 11 | 760 | 790 | 790 | 710 | 0 | 0 | 763 | 37.749 | 1.656 | 100.0 | 100.0 |
| 12 | 775 | 760 | 770 | 0 | 0 | 0 | 768 | 7.642 | 8.941 | 100.0 | 100.0 |

APPENDIX L (Continued)
PAP TEST RESULTS - 28 DAYS ONLY
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 2

Port: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Only 28-day tests

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|------------------|-------------|-----------|---------------|
| 13 | Lots 24 & 25 | 12/18/87 | 01/15/88 | 28 |
| 15 | Lots 26, 27 & 28 | 01/04/88 | 02/01/88 | 28 |
| 17 | Lots 29 & 30 | 01/19/88 | 02/16/88 | 28 |
| 18 | Lots 32 & 33 | 01/22/88 | 02/19/88 | 28 |
| 19 | Lots 34 & 35 | 02/09/88 | 03/08/88 | 28 |
| 20 | Lots 36 & 37 | 02/10/88 | 03/09/88 | 28 |
| 21 | Lots 38, 39 & 40 | 02/17/88 | 03/16/88 | 28 |
| 22 | Lots 41 & 42 | 02/18/88 | 03/17/88 | 28 |
| 23 | Lots 43 & 44 | 02/22/88 | 03/21/88 | 28 |
| 24 | Lots 45 & 46 | 02/23/88 | 03/22/88 | 28 |
| 25 | Lots 48 & 49 | 03/02/88 | 03/30/88 | 28 |
| 26 | Lots 50 & 51 | 03/03/88 | 03/31/88 | 28 |
| 27 | Lots 52 & 53 | 03/07/88 | 04/04/88 | 28 |
| 28 | Lots 54 & 55 | 03/08/88 | 04/05/88 | 28 |
| 29 | Lots 56 & 57 | 03/09/88 | 04/06/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 13 | 795 | 780 | 940 | 955 | 0 | 0 | 868 | 92.781 | 1.805 | 100.0 | 100.0 |
| 15 | 790 | 740 | 695 | 745 | 830 | 810 | 768 | 50.465 | 1.354 | 92.5 | 100.0 |
| 17 | 825 | 790 | 720 | 740 | 0 | 0 | 769 | 47.675 | 1.442 | 98.1 | 100.0 |
| 18 | 745 | 770 | 810 | 880 | 0 | 0 | 801 | 58.931 | 1.718 | 100.0 | 100.0 |
| 19 | 860 | 880 | 810 | 810 | 0 | 0 | 840 | 35.590 | 3.934 | 100.0 | 100.0 |
| 20 | 760 | 785 | 780 | 770 | 0 | 0 | 774 | 11.087 | 6.652 | 100.0 | 100.0 |
| 21 | 825 | 805 | 830 | 800 | 780 | 850 | 815 | 24.900 | 4.619 | 100.0 | 100.0 |
| 22 | 830 | 800 | 695 | 710 | 0 | 0 | 759 | 66.380 | 0.885 | 79.5 | 89.1 |
| 23 | 880 | 865 | 780 | 770 | 0 | 0 | 824 | 56.771 | 2.180 | 100.0 | 100.0 |
| 24 | 760 | 810 | 730 | 720 | 0 | 0 | 755 | 40.415 | 1.361 | 95.4 | 100.0 |
| 25 | 890 | 920 | 800 | 800 | 0 | 0 | 853 | 61.847 | 2.466 | 100.0 | 100.0 |
| 26 | 870 | 900 | 800 | 815 | 0 | 0 | 846 | 46.793 | 3.125 | 100.0 | 100.0 |
| 27 | 855 | 860 | 760 | 705 | 0 | 0 | 795 | 75.609 | 1.256 | 91.9 | 100.0 |
| 28 | 860 | 835 | 860 | 890 | 0 | 0 | 861 | 22.500 | 7.167 | 100.0 | 100.0 |
| 29 | 905 | 820 | 840 | 800 | 0 | 0 | 841 | 45.529 | 3.102 | 100.0 | 100.0 |

APPENDIX L (Continued)
PAP TEST RESULTS - 28 DAYS ONLY
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 3

Airport: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Only 28-day tests

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--------------------|-------------|-----------|---------------|
| 30 | Lots 58 & 59 | 03/11/88 | 04/08/88 | 28 |
| 31 | Lots 60 & 61 | 03/23/88 | 04/20/88 | 28 |
| 32 | Lots 62 & 63 | 03/24/88 | 04/21/88 | 28 |
| 33 | Lots 64 & 65 | 03/30/88 | 04/27/88 | 28 |
| 34 | Lots 66, 67 and 68 | 04/05/88 | 05/03/88 | 28 |
| 35 | Lots 69 & 70 | 04/06/88 | 05/04/88 | 28 |
| 37 | Lots 73 & 74 | 09/20/88 | 10/18/88 | 28 |
| 38 | Lots 75 & 76 | 09/21/88 | 10/19/88 | 28 |
| 39 | Lots 77 & 81 | 10/03/88 | 10/31/88 | 28 |
| 40 | Lots 78, 79 & 80 | 10/05/88 | 11/02/88 | 28 |
| 41 | Lots 82 & 83 | 10/07/88 | 11/04/88 | 28 |
| 42 | Lots 84 & 85 | 10/08/88 | 11/05/88 | 28 |
| 43 | Lots 86 & 87 | 10/10/88 | 11/07/88 | 28 |
| 44 | Lots 88 & 89 | 10/12/88 | 11/09/88 | 28 |
| 45 | Lots 90 & 91 | 10/14/88 | 11/11/88 | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | AVERAGE | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | | | | | |
| 30 | 820 | 910 | 780 | 800 | 0 | 0 | 828 | 57.373 | 2.222 | 100.0 | 100.0 |
| 31 | 820 | 840 | 850 | 810 | 0 | 0 | 830 | 18.257 | 7.120 | 100.0 | 100.0 |
| 32 | 780 | 740 | 730 | 740 | 0 | 0 | 748 | 22.174 | 2.142 | 100.0 | 100.0 |
| 33 | 776 | 798 | 761 | 714 | 0 | 0 | 762 | 35.575 | 1.750 | 100.0 | 100.0 |
| 34 | 800 | 830 | 800 | 800 | 840 | 780 | 808 | 22.287 | 4.861 | 100.0 | 100.0 |
| 35 | 730 | 725 | 760 | 720 | 0 | 0 | 734 | 17.970 | 1.878 | 100.0 | 100.0 |
| 37 | 720 | 750 | 780 | 775 | 0 | 0 | 756 | 27.500 | 2.045 | 100.0 | 100.0 |
| 38 | 710 | 840 | 860 | 870 | 0 | 0 | 820 | 74.386 | 1.613 | 100.0 | 100.0 |
| 39 | 860 | 830 | 750 | 780 | 0 | 0 | 805 | 49.329 | 2.129 | 100.0 | 100.0 |
| 40 | 710 | 730 | 730 | 790 | 860 | 930 | 792 | 87.273 | 1.050 | 85.2 | 95.9 |
| 41 | 830 | 820 | 700 | 790 | 0 | 0 | 785 | 59.161 | 1.437 | 97.9 | 100.0 |
| 42 | 901 | 910 | 715 | 740 | 0 | 0 | 817 | 103.339 | 1.127 | 87.6 | 98.1 |
| 43 | 875 | 735 | 820 | 800 | 0 | 0 | 808 | 57.807 | 1.860 | 100.0 | 100.0 |
| 44 | 840 | 900 | 890 | 830 | 0 | 0 | 870 | 42.426 | 4.007 | 100.0 | 100.0 |
| 45 | 980 | 850 | 800 | 840 | 0 | 0 | 868 | 78.049 | 2.146 | 100.0 | 100.0 |

APPENDIX L (Continued)
PAP TEST RESULTS - 28 DAYS ONLY
NORFOLK INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, PORTLAND CEMENT CONCRETE PAVEMENT

06-08-1990

PAGE 4

Airport: Norfolk International Airport, Norfolk, VA

FAA Project Name: Terminal Apron Expansion

Work Area Project Name: Only 28-day tests

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|------------|-----------------|----------------|--------------|------------------|
|------------|-----------------|----------------|--------------|------------------|

| | | | | |
|----|--------------|----------|----------|----|
| 46 | Lots 92 & 93 | 10/14/88 | 11/11/88 | 28 |
| 47 | Lots 94 & 95 | 10/15/88 | 11/12/88 | 28 |
| 48 | Lots 96 & 97 | 10/17/88 | 11/14/88 | 28 |
| 49 | Lots 98 & 99 | 10/18/88 | 11/15/88 | 28 |

| LOT NO. | -----TEST RESULT STRENGTH IN PSI----- | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|------------|---------------------------------------|-----|-----|-----|-----|-----|------------|-----------|------------|-----------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | |
| 46 | 880 | 810 | 760 | 860 | 0 | 0 | 828 | 53.774 | 2.371 | 100.0 |
| 47 | 910 | 810 | 800 | 820 | 0 | 0 | 835 | 50.662 | 2.665 | 100.0 |
| 48 | 750 | 790 | 750 | 780 | 0 | 0 | 768 | 20.616 | 3.274 | 100.0 |
| 49 | 830 | 920 | 825 | 855 | 0 | 0 | 858 | 43.684 | 3.605 | 100.0 |

APPENDIX M
PAP TEST RESULTS - BY LOTS
DULLES INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT DEFAULTS FOR AIRPORT PAVEMENT CONSTRUCTION.
P-501, Portland Cement Concrete Pavement
for Dulles International Airport

1. THE LOWEST PWL IN PERCENT TO RECEIVE 100% PAYMENT: 90
2. THE LOWEST PWL IN PERCENT TO RECEIVE MINIMUM PAYMENT: 60
THE MINIMUM PAY FACTOR IN PERCENT TO RECEIVE PAYMENT: 50
3. THE MIDPOINT SCALING FACTOR BETWEEN [1] AND [-1]: .6

PAY FACTOR FORMULA IS: $-3.212007 * PWL^2 + 6.484677 * PWL + -2.234484$

Press any key to return to program.
RESPONSE REQUEST MODE

APPENDIX M (Continued)
PAP TEST RESULTS - BY LOTS
DULLES INTERNATIONAL AIRPORT

FAA ACCEPTANCE AND PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENTS
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 1

Airport: Dulles International Airport
Washington DC
IAD

Consultant/Engineer:

Construction Contractor:

Pavement Testing Laboratory: ATEC Assoc. of Virginia, Inc.
Chantilly, VA 22021

FAA Contract Number:
FAA Project Name: Concrete Pavement Panel
Work Area Project Name: Runway No. 30 - By lots

Pavement Specification: P-501, Portland Cement Concrete Pavement
Design Target Specification in PSI: 650

Method of Testing:

ASTM Number:

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|------------------------------------|-------------|-----------|---------------|
| 1 | North Lane, Station 31+47 to 31+54 | 06/30/88 | 07/07/88 | 7 |
| 2 | North Lane, Station 45+70 to 45+80 | 07/01/88 | 07/08/88 | 7 |
| 3 | Station 50+60 to 50+70 | 07/01/88 | 07/08/88 | 7 |
| 4 | North Lane, Station 32+80 | 07/06/88 | 07/20/88 | 14 |
| 5 | North Lane, Station 34+20 | 07/06/88 | 07/20/88 | 14 |
| 6 | North Lane, Station 35+40 | 07/06/88 | 07/20/88 | 14 |
| 7 | North Lane, Station 36+60 | 07/06/88 | 08/03/88 | 28 |
| 8 | North Lane, Station 37+80 | 07/06/88 | 07/20/88 | 14 |
| 9 | North Lane, Station 39+20 | 07/06/88 | 07/20/88 | 14 |
| 10 | North Lane, Station 40+40 | 07/06/88 | 07/20/88 | 14 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR | |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|---------|--------------|-------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 1 | 530 | 570 | 840 | 870 | 0 | 0 | 703 | 177.271 | 0.296 | 59.9 | 0.0 |
| 2 | 550 | 590 | 860 | 850 | 0 | 0 | 713 | 165.404 | 0.378 | 62.6 | 56.6 |
| 3 | 645 | 590 | 760 | 770 | 0 | 0 | 691 | 88.164 | 0.468 | 65.6 | 63.7 |
| 4 | 550 | 570 | 735 | 740 | 0 | 0 | 649 | 102.825 | -0.012 | 49.6 | 0.0 |
| 5 | 595 | 610 | 710 | 740 | 0 | 0 | 664 | 72.039 | 0.191 | 56.4 | 0.0 |
| 6 | 570 | 550 | 675 | 690 | 0 | 0 | 621 | 71.458 | -0.402 | 36.6 | 0.0 |
| 7 | 610 | 670 | 715 | 705 | 0 | 0 | 675 | 47.434 | 0.527 | 67.6 | 68.1 |
| 8 | 635 | 605 | 720 | 730 | 0 | 0 | 673 | 61.981 | 0.363 | 62.1 | 55.4 |
| 9 | 560 | 560 | 750 | 750 | 0 | 0 | 655 | 109.697 | 0.046 | 51.5 | 0.0 |
| 10 | 720 | 670 | 695 | 690 | 0 | 0 | 694 | 20.565 | 2.127 | 100.0 | 100.0 |

APPENDIX M (Continued)
PAP TEST RESULTS - BY LOTS
DULLES INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 2

Airport: Dulles International Airport, Washington DC

FAA Project Name: Concrete Pavement Panel

Work Area Project Name: Runway No. 30 - By lots

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|--------------------------------|-------------|-----------|---------------|
| 11 | North Lane, Station 41+60 | 07/06/88 | 07/20/88 | 14 |
| 12 | North Lane, Station 42+80 | 07/06/88 | 07/20/88 | 14 |
| 13 | North Lane, Station 44+00 | 07/06/88 | 08/03/88 | 28 |
| 14 | South Lane, Station 50+40 | 07/07/88 | 07/21/88 | 14 |
| 15 | Station 30+00, 63 ft right | 07/08/88 | 07/22/88 | 14 |
| 16 | W2, Station 21+90 | 07/11/88 | 07/25/88 | 14 |
| 17 | W2, Station 12,28, 38 ft right | 07/11/88 | 07/25/88 | 14 |
| 18 | South Lane, Station 43+60 | 07/13/88 | 08/10/88 | 28 |
| 19 | South Lane, Station 43+00 | 07/13/88 | 07/27/88 | 14 |
| 20 | South Lane, Station 41+80 | 07/13/88 | 07/27/88 | 14 |
| 21 | South Lane, Station 40+60 | 07/13/88 | 07/27/88 | 14 |
| 22 | South Lane, Station 39+40 | 07/13/88 | 07/27/88 | 14 |
| 23 | South Lane, Station 38+20 | 07/13/88 | 08/10/88 | 28 |
| 24 | South Lane, Station 36+60 | 07/13/88 | 07/27/88 | 14 |
| 25 | South Lane, Station 35+40 | 07/13/88 | 07/27/88 | 14 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR | |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|--------|---------|--------------|-------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 11 | 610 | 655 | 755 | 805 | 0 | 0 | 706 | 89.478 | 0.629 | 71.0 | 75.0 |
| 12 | 755 | 745 | 745 | 805 | 0 | 0 | 763 | 28.723 | 3.917 | 100.0 | 100.0 |
| 13 | 715 | 660 | 690 | 690 | 0 | 0 | 689 | 22.500 | 1.722 | 100.0 | 100.0 |
| 14 | 700 | 710 | 710 | 740 | 0 | 0 | 715 | 17.321 | 3.753 | 100.0 | 100.0 |
| 15 | 695 | 680 | 700 | 720 | 0 | 0 | 699 | 16.520 | 2.951 | 100.0 | 100.0 |
| 16 | 555 | 695 | 695 | 640 | 0 | 0 | 646 | 66.128 | -0.057 | 48.1 | 0.0 |
| 17 | 725 | 650 | 680 | 740 | 0 | 0 | 699 | 41.307 | 1.180 | 89.3 | 99.5 |
| 18 | 685 | 745 | 715 | 735 | 0 | 0 | 720 | 26.458 | 2.646 | 100.0 | 100.0 |
| 19 | 685 | 650 | 790 | 745 | 0 | 0 | 718 | 62.250 | 1.084 | 86.1 | 96.8 |
| 20 | 805 | 665 | 700 | 795 | 0 | 0 | 741 | 69.447 | 1.314 | 93.8 | 100.0 |
| 21 | 665 | 635 | 705 | 685 | 0 | 0 | 673 | 29.861 | 0.753 | 75.1 | 82.4 |
| 22 | 665 | 715 | 700 | 750 | 0 | 0 | 708 | 35.237 | 1.632 | 100.0 | 100.0 |
| 23 | 645 | 680 | 700 | 665 | 0 | 0 | 673 | 23.274 | 0.967 | 82.2 | 92.6 |
| 24 | 640 | 640 | 690 | 665 | 0 | 0 | 659 | 23.936 | 0.366 | 62.2 | 55.6 |
| 25 | 700 | 700 | 730 | 770 | 0 | 0 | 725 | 33.166 | 2.261 | 100.0 | 100.0 |

APPENDIX M (Continued)
PAP TEST RESULTS - BY LOTS
DULLES INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 3

Airport: Dulles International Airport, Washington DC

FAA Project Name: Concrete Pavement Panel

Work Area Project Name: Runway No. 30 - By lots

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-------------------------------|-------------|-----------|---------------|
| 26 | South Lane, Station 34+20 | 07/13/88 | 07/27/88 | 14 |
| 27 | South Lane, Station 33+60 | 07/14/88 | 07/28/88 | 14 |
| 28 | W2, Station 18+43 | 07/14/88 | 07/28/88 | 14 |
| 29 | W2, Station 38+63 left | 08/19/88 | 09/02/88 | 14 |
| 30 | W2, Station 37+88 left | 08/19/88 | 09/02/88 | 14 |
| 31 | W2, Station 32+70, Centerline | 08/22/88 | 09/05/88 | 14 |
| 32 | W2, Station 34+90, Centerline | 08/22/88 | 09/05/88 | 14 |
| 33 | W2, Station 35+70, Right | 08/22/88 | 09/05/88 | 14 |
| 34 | W2, Station 39+63 Left | 08/23/88 | 09/06/88 | 14 |
| 35 | W2, Station 40+63 Right | 08/23/88 | 09/06/88 | 14 |
| 36 | W2, Station 45+13 Right | 08/23/88 | 09/06/88 | 14 |
| 37 | W2, Station 47+13 Left | 08/23/88 | 09/20/88 | 28 |
| 38 | W2, Station 46+38 Left | 08/23/88 | 09/06/88 | 14 |
| 39 | T2, Station 9+25 Centerline | 08/27/88 | 09/10/88 | 14 |
| 40 | W2, Station 47+38 Centerline | 08/31/88 | 09/14/88 | 14 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | AVERAGE | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|------|------|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | | | | | |
| 26 | 715 | 635 | 690 | 700 | 0 | 0 | 685 | 34.881 | 1.003 | 83.4 | 94.0 |
| 27 | 680 | 690 | 690 | 765 | 0 | 0 | 706 | 39.449 | 1.426 | 97.5 | 100.0 |
| 28 | 750 | 680 | 665 | 730 | 0 | 0 | 706 | 40.285 | 1.396 | 96.5 | 100.0 |
| 29 | 835 | 895 | 830 | 815 | 0 | 0 | 844 | 35.208 | 5.503 | 100.0 | 100.0 |
| 30 | 755 | 725 | 760 | 760 | 0 | 0 | 750 | 16.833 | 5.941 | 100.0 | 100.0 |
| 31 | 855 | 815 | 930 | 935 | 0 | 0 | 884 | 58.648 | 3.986 | 100.0 | 100.0 |
| 32 | 715 | 745 | 790 | 840 | 0 | 0 | 773 | 54.544 | 2.246 | 100.0 | 100.0 |
| 33 | 710 | 665 | 920 | 900 | 0 | 0 | 799 | 130.024 | 1.144 | 88.1 | 98.6 |
| 34 | 660 | 685 | 730 | 790 | 0 | 0 | 716 | 57.064 | 1.161 | 88.7 | 99.0 |
| 35 | 750 | 846 | 855 | 980 | 0 | 0 | 858 | 94.341 | 2.202 | 100.0 | 100.0 |
| 36 | 765 | 815 | 830 | 825 | 0 | 0 | 809 | 29.826 | 5.323 | 100.0 | 100.0 |
| 37 | 830 | 815 | 840 | 840 | 0 | 0 | 831 | 11.815 | 15.340 | 100.0 | 100.0 |
| 38 | 750 | 670 | 790 | 725 | 0 | 0 | 734 | 50.229 | 1.667 | 100.0 | 100.0 |
| 39 | 835 | 785 | 1120 | 1150 | 0 | 0 | 973 | 189.143 | 1.705 | 100.0 | 100.0 |
| 40 | 705 | 780 | 730 | 860 | 0 | 0 | 769 | 68.359 | 1.737 | 100.0 | 100.0 |

APPENDIX M (Continued)
PAP TEST RESULTS - BY LOTS
DULLES INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 4

Airport: Dulles International Airport, Washington DC

FAA Project Name: Concrete Pavement Panel

Work Area Project Name: Runway No. 30 - By lots

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-------------------------------|-------------|-----------|---------------|
| 41 | W2, Station 42+63, 25 ft Left | 08/31/88 | 09/14/88 | 14 |
| 42 | W2, Station 44+63, 25 ft Left | 09/01/88 | 09/15/88 | 14 |
| 43 | W2, Station 43+13, 25 ft Left | 09/01/88 | 09/15/88 | 14 |
| 44 | W2, Station 39+88, 25 ft Left | 09/01/88 | 09/15/88 | 14 |
| 45 | W2, Station 48+88, 25 ft Left | 09/02/88 | 09/16/88 | 14 |
| 46 | W2, Station 47+75, Centerline | 09/02/88 | 09/16/88 | 14 |
| 47 | R1, Station 48+25, Centerline | 09/02/88 | 09/16/88 | 14 |
| 48 | R2, Station 1+00, Centerline | 09/14/88 | 09/28/88 | 14 |
| 49 | R2, Station 1+75 Centerline | 09/14/88 | 09/28/88 | 14 |
| 50 | R1, Station 47+75 Centerline | 10/01/88 | 10/15/88 | 14 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|------|------|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 41 | 820 | 750 | 890 | 800 | 0 | 0 | 815 | 58.023 | 2.844 | 100.0 | 100.0 |
| 42 | 620 | 690 | 700 | 705 | 0 | 0 | 679 | 39.660 | 0.725 | 74.2 | 80.8 |
| 43 | 725 | 660 | 700 | 760 | 0 | 0 | 711 | 42.106 | 1.455 | 98.5 | 100.0 |
| 44 | 920 | 880 | 820 | 865 | 0 | 0 | 871 | 41.307 | 5.356 | 100.0 | 100.0 |
| 45 | 760 | 905 | 805 | 805 | 0 | 0 | 819 | 61.288 | 2.753 | 100.0 | 100.0 |
| 46 | 645 | 645 | 790 | 705 | 0 | 0 | 696 | 68.602 | 0.674 | 72.5 | 77.8 |
| 47 | 755 | 710 | 1090 | 1070 | 0 | 0 | 906 | 201.634 | 1.271 | 92.4 | 100.0 |
| 48 | 810 | 810 | 920 | 1000 | 0 | 0 | 885 | 92.556 | 2.539 | 100.0 | 100.0 |
| 49 | 890 | 930 | 1210 | 1110 | 0 | 0 | 1035 | 150.886 | 2.552 | 100.0 | 100.0 |
| 50 | 680 | 900 | 1160 | 1300 | 0 | 0 | 1010 | 275.439 | 1.307 | 93.6 | 100.0 |
| 51 | 845 | 885 | 1085 | 1050 | 0 | 0 | 966 | 118.910 | 2.660 | 100.0 | 100.0 |

APPENDIX N
PAP TEST RESULTS - 28 DAYS ONLY
DULLES INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT DEFAULTS FOR AIRPORT PAVEMENT CONSTRUCTION
P-501, Portland Cement Concrete Pavement
for Dulles International Airport

1. THE LOWEST PWL IN PERCENT TO RECEIVE 100% PAYMENT: 90
2. THE LOWEST PWL IN PERCENT TO RECEIVE MINIMUM PAYMENT: 60
THE MINIMUM PAY FACTOR IN PERCENT TO RECEIVE PAYMENT: 50
3. THE MIDPOINT SCALING FACTOR BETWEEN [1] AND [-1]: .6

PAY FACTOR FORMULA IS: $-3.212007 * PWL^2 + 6.484677 * PWL + -2.234484$

Press any key to return to program.
RESPONSE REQUEST MODE

APPENDIX N (Continued)
PAP TEST RESULTS - 28 DAYS ONLY
DULLES INTERNATIONAL AIRPORT

FAA ACCEPTANCE AND PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENTS
P-501, Portland Cement Concrete Pavement

06-07-1990 PAGE 1

Airport: Dulles International Airport
Washington DC
IAD

Consultant/Engineer:

Construction Contractor:

Pavement Testing Laboratory: ATEC Assoc. of Virginia, Inc.
Chantilly, VA 22021

FAA Contract Number:

FAA Project Name: Concrete Pavement Panel

Work Area Project Name: Best of two lots for Runway No. 30

Pavement Specification: P-501, Portland Cement Concrete Pavement

Design Target Specification in PSI: 650

Method of Testing:

ASTM Number:

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|------------|-----------------|----------------|--------------|------------------|
|------------|-----------------|----------------|--------------|------------------|

| | |
|----|--------------|
| 1 | Lots 1 & 2 |
| 2 | Lots 3 & 4 |
| 3 | Lots 5 & 6 |
| 4 | Lots 7 & 8 |
| 5 | Lots 9 & 10 |
| | |
| 6 | Lots 11 & 12 |
| 7 | Lots 13 & 14 |
| 8 | Lots 15 & 16 |
| 9 | Lots 17 & 18 |
| 10 | Lots 19 & 20 |

| LOT NO. | -----TEST RESULT STRENGTH IN PSI----- | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|------------|---------------------------------------|-----|-----|-----|-----|-----|------------|-----------|------------|-----------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | |
| 1 | 840 | 870 | 860 | 850 | 0 | 0 | 855 | 12.910 | 15.870 | 100.0 |
| 2 | 760 | 770 | 735 | 740 | 0 | 0 | 751 | 16.520 | 6.129 | 100.0 |
| 3 | 710 | 740 | 675 | 690 | 0 | 0 | 704 | 28.100 | 1.913 | 100.0 |
| 4 | 715 | 705 | 720 | 730 | 0 | 0 | 718 | 10.408 | 6.485 | 100.0 |
| 5 | 750 | 750 | 720 | 695 | 0 | 0 | 729 | 26.575 | 2.963 | 100.0 |
| | | | | | | | | | | |
| 6 | 755 | 805 | 755 | 805 | 0 | 0 | 780 | 28.868 | 4.503 | 100.0 |
| 7 | 715 | 690 | 710 | 740 | 0 | 0 | 714 | 20.565 | 3.100 | 100.0 |
| 8 | 700 | 720 | 695 | 695 | 0 | 0 | 703 | 11.902 | 4.411 | 100.0 |
| 9 | 725 | 740 | 745 | 735 | 0 | 0 | 736 | 8.539 | 10.100 | 100.0 |
| 10 | 790 | 745 | 805 | 795 | 0 | 0 | 784 | 26.575 | 5.033 | 100.0 |

APPENDIX N (Continued)
PAP TEST RESULTS - 28 DAYS ONLY
DULLES INTERNATIONAL AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-07-1990

PAGE 2

Airport: Dulles International Airport, Washington DC
FAA Project Name: Concrete Pavement Panel
Work Area Project Name: Best of two lots for Runway No. 30

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|---------------------|-------------|-----------|---------------|
| 11 | Lots 21 & 22 | | | |
| 12 | Lots 23 & 24 | | | |
| 13 | Lots 25 & 26 | | | |
| 14 | Lots 27 & 28 | | | |
| 15 | Lots 29 & 30 | | | |
| 16 | Lots 31 & 32 | | | |
| 17 | Lots 33 & 34 | | | |
| 18 | Lots 35 & 36 | | | |
| 19 | Lots 37 & 38 | | | |
| 20 | Lots 39 & 40 | | | |
| 21 | Lots 41 & 42 | | | |
| 22 | Lots 43 & 44 | | | |
| 23 | Lots 45 & 46 | | | |
| 24 | Lots 47 & 48 | | | |
| 25 | Lots 49, 50, and 51 | | | |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|------|------|------|------|------|---------|---------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | |
| 11 | 705 | 685 | 715 | 750 | 0 | 0 | 714 | 27.195 | 2.344 | 100.0 |
| 12 | 680 | 700 | 690 | 665 | 0 | 0 | 684 | 14.930 | 2.260 | 100.0 |
| 13 | 730 | 770 | 715 | 700 | 0 | 0 | 729 | 30.104 | 2.616 | 100.0 |
| 14 | 690 | 765 | 750 | 730 | 0 | 0 | 734 | 32.500 | 2.577 | 100.0 |
| 15 | 835 | 895 | 755 | 760 | 0 | 0 | 811 | 66.755 | 2.416 | 100.0 |
| 16 | 930 | 935 | 790 | 840 | 0 | 0 | 874 | 70.873 | 3.157 | 100.0 |
| 17 | 920 | 900 | 730 | 790 | 0 | 0 | 835 | 90.370 | 2.047 | 100.0 |
| 18 | 855 | 980 | 830 | 825 | 0 | 0 | 873 | 72.858 | 3.054 | 100.0 |
| 19 | 840 | 840 | 750 | 790 | 0 | 0 | 805 | 43.589 | 3.556 | 100.0 |
| 20 | 1120 | 1150 | 780 | 860 | 0 | 0 | 978 | 185.180 | 1.769 | 100.0 |
| 21 | 820 | 890 | 700 | 705 | 0 | 0 | 779 | 92.590 | 1.391 | 96.4 |
| 22 | 725 | 760 | 920 | 880 | 0 | 0 | 821 | 93.486 | 1.832 | 100.0 |
| 23 | 905 | 805 | 790 | 705 | 0 | 0 | 801 | 81.993 | 1.845 | 100.0 |
| 24 | 1090 | 1070 | 920 | 1000 | 0 | 0 | 1020 | 77.928 | 4.803 | 100.0 |
| 25 | 1210 | 1110 | 1160 | 1300 | 1085 | 1050 | 1153 | 91.638 | 5.484 | 100.0 |

APPENDIX O
PAP TEST RESULTS
BALTIMORE/WASHINGTON INTERNATIONAL

FAA PAYMENT ADJUSTMENT DEFAULTS FOR AIRPORT PAVEMENT CONSTRUCTION
P-501, Portland Cement Concrete Pavement
for Baltimore/Washington International

1. THE LOWEST PWL IN PERCENT TO RECEIVE 100% PAYMENT: 90
2. THE LOWEST PWL IN PERCENT TO RECEIVE MINIMUM PAYMENT: 60
THE MINIMUM PAY FACTOR IN PERCENT TO RECEIVE PAYMENT: 50
3. THE MIDPOINT SCALING FACTOR BETWEEN [1] AND [-1]: .6

PAY FACTOR FORMULA IS: $-3.212007 * PWL^2 + 6.484677 * PWL + -2.234484$

Press any key to return to program.
RESPONSE REQUEST MODE

APPENDIX O (Continued)
PAP TEST RESULTS
BALTIMORE/WASHINGTON INTERNATIONAL

FAA ACCEPTANCE AND PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENTS
P-501, Portland Cement Concrete Pavement

06-08-1990

PAGE 1

Airport: Baltimore/Washington International
Baltimore, MD
BWI

Consultant/Engineer:

Construction Contractor: P. Flanigan & Sons, Inc.
Baltimore, MD

Pavement Testing Laboratory: Penniman & Browne, Inc.
Baltimore, MD

FAA Contract Number: SAA-CO-87-010

FAA Project Name: 1987 Expansion

Work Area Project Name: Pier D/Y Headstand

Pavement Specification: P-501, Portland Cement Concrete Pavement

Design Target Specification in PSI: 700

Method of Testing:

ASTM Number:

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-------------------|-------------|-----------|---------------|
| 1 | 8/21/87 & 8/22/87 | 08/21/87 | | |
| 2 | | 08/24/87 | | |
| 3 | | 08/26/87 | | |
| 4 | | 08/28/87 | | |
| 5 | | 09/29/87 | | |
| 6 | | 10/01/87 | | |
| 7 | | 10/02/87 | | |
| 8 | | 10/02/87 | | |
| 9 | | 10/06/87 | | |
| 10 | | 10/07/87 | | |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|------|------|------|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 1 | 763 | 844 | 860 | 901 | 826 | 0 | 839 | 50.633 | 2.741 | 100.0 | 100.0 |
| 2 | 863 | 903 | 930 | 991 | 0 | 0 | 922 | 53.749 | 4.126 | 100.0 | 100.0 |
| 3 | 745 | 784 | 827 | 856 | 0 | 0 | 803 | 48.683 | 2.116 | 100.0 | 100.0 |
| 4 | 802 | 879 | 906 | 0 | 0 | 0 | 862 | 53.966 | 3.008 | 100.0 | 100.0 |
| 5 | 888 | 845 | 732 | 822 | 0 | 0 | 822 | 65.789 | 1.851 | 100.0 | 100.0 |
| 6 | 898 | 1071 | 990 | 938 | 0 | 0 | 974 | 74.692 | 3.672 | 100.0 | 100.0 |
| 7 | 996 | 836 | 865 | 872 | 0 | 0 | 892 | 70.901 | 2.712 | 100.0 | 100.0 |
| 8 | 901 | 845 | 839 | 840 | 0 | 0 | 856 | 29.949 | 5.217 | 100.0 | 100.0 |
| 9 | 977 | 981 | 1112 | 880 | 0 | 0 | 988 | 95.235 | 3.019 | 100.0 | 100.0 |
| 10 | 1025 | 1096 | 1008 | 1017 | 0 | 0 | 1037 | 40.270 | 8.356 | 100.0 | 100.0 |

APPENDIX O (Continued)
PAP TEST RESULTS
BALTIMORE/WASHINGTON INTERNATIONAL

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-08-1990

PAGE 2

Airport: Baltimore/Washington International, Baltimore, MD

FAA Project Name: 1987 Expansion

Work Area Project Name: Pier D/Y Headstand

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------|-------------|-----------|---------------|
|---------|-----------------|-------------|-----------|---------------|

| | | | | |
|----|---------------------|----------|--|--|
| 11 | 10/08/87 & 10/09/87 | 10/08/87 | | |
| 12 | | 10/12/87 | | |
| 13 | | 10/13/87 | | |
| 14 | | 10/14/87 | | |
| 15 | | 10/26/87 | | |
| 16 | | 10/27/87 | | |
| 17 | 10/28/87 & 10/29/87 | 10/28/87 | | |
| 18 | | 10/30/87 | | |
| 19 | | 11/02/ 7 | | |
| 20 | | 11/03/87 | | |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|------|------|-----|------|------|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 11 | 1117 | 1000 | 942 | 958 | 971 | 0 | 998 | 70.053 | 4.248 | 100.0 | 100.0 |
| 12 | 1120 | 845 | 1020 | 830 | 0 | 0 | 954 | 140.438 | 1.807 | 100.0 | 100.0 |
| 13 | 995 | 915 | 1015 | 995 | 0 | 0 | 980 | 44.347 | 6.314 | 100.0 | 100.0 |
| 14 | 830 | 915 | 890 | 955 | 0 | 0 | 898 | 52.361 | 3.772 | 100.0 | 100.0 |
| 15 | 800 | 645 | 865 | 820 | 0 | 0 | 783 | 95.612 | 0.863 | 78.8 | 88.0 |
| 16 | 820 | 900 | 890 | 920 | 0 | 0 | 883 | 43.493 | 4.196 | 100.0 | 100.0 |
| 17 | 1005 | 945 | 760 | 810 | 1030 | 1000 | 925 | 113.049 | 1.990 | 100.0 | 100.0 |
| 18 | 910 | 980 | 1030 | 890 | 0 | 0 | 953 | 64.485 | 3.916 | 100.0 | 100.0 |
| 19 | 760 | 855 | 770 | 790 | 0 | 0 | 794 | 42.696 | 2.196 | 100.0 | 100.0 |
| 20 | 795 | 710 | 865 | 740 | 0 | 0 | 778 | 68.130 | 1.138 | 87.9 | 98.4 |

APPENDIX P
PAP TEST RESULTS
WICHITA MID-CONTINENT AIRPORT

FAA PAYMENT ADJUSTMENT DEFAULTS FOR AIRPORT PAVEMENT CONSTRUCTION
P-501, Portland Cement Concrete Pavement
for Wichita Mid-Continent Airport

1. THE LOWEST PWL IN PERCENT TO RECEIVE 100% PAYMENT: 90
2. THE LOWEST PWL IN PERCENT TO RECEIVE MINIMUM PAYMENT: 60
THE MINIMUM PAY FACTOR IN PERCENT TO RECEIVE PAYMENT: 50
3. THE MIDPOINT SCALING FACTOR BETWEEN [1] AND [-1]: .6

PAY FACTOR FORMULA IS: $-3.212007 * PWL^2 + 6.484677 * PWL + -2.234484$

Press any key to return to program.
RESPONSE REQUEST MODE

APPENDIX P (Continued)
PAP TEST RESULTS
WICHITA MID-CONTINENT AIRPORT

FAA ACCEPTANCE AND PAYMENT ADJUSTMENT FOR AIRPORT PAVEMENTS
P-501, Portland Cement Concrete Pavement

06-08-1990

PAGE 1

Airport: Wichita Mid-Continent Airport
Wichita, Kansas
ICT

Consultant/Engineer:

Construction Contractor:

Pavement Testing Laboratory: Professional Engineering Cons.
Wichita, Kansas

FAA Contract Number: AIP 3-20-088-09 & 10
FAA Project Name: Runway 1L-19R Reconstruction
Work Area Project Name: Runway 1L-19R Reconstruction - 28-days

Pavement Specification: P-501, Portland Cement Concrete Pavement
Design Target Specification in PSI: 650

Method of Testing: Flexural Beams
ASTM Number: ASTM C-78

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------|-------------|-----------|---------------|
| 1 | 7-25-1 | 07/25/87 | | 28 |
| 2 | 7-27-1 | 07/27/87 | | 28 |
| 3 | 7-27-1 | 07/27/87 | | 28 |
| 4 | 7-30-1 | 07/30/87 | | 28 |
| 5 | 7-30-1 | 07/30/87 | | 28 |
| 6 | 7-30-3 | 07/30/87 | | 28 |
| 7 | 7-30-3 | 07/30/87 | | 28 |
| 8 | 8-01-1 | 08/01/87 | | 28 |
| 9 | 8-01-1 | 08/01/87 | | 28 |
| 10 | 8-01-3 | 08/01/87 | | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | |
| 1 | 777 | 777 | 766 | 869 | 0 | 0 | 797 | 48.114 | 3.060 | 100.0 |
| 2 | 823 | 766 | 849 | 853 | 0 | 0 | 823 | 40.103 | 4.308 | 100.0 |
| 3 | 762 | 747 | 781 | 781 | 0 | 0 | 768 | 16.480 | 7.145 | 100.0 |
| 4 | 702 | 763 | 708 | 648 | 0 | 0 | 705 | 47.013 | 1.175 | 89.2 |
| 5 | 761 | 829 | 669 | 791 | 0 | 0 | 763 | 68.262 | 1.648 | 100.0 |
| 6 | 706 | 734 | 701 | 744 | 0 | 0 | 721 | 20.998 | 3.393 | 100.0 |
| 7 | 771 | 650 | 750 | 696 | 0 | 0 | 717 | 54.573 | 1.223 | 90.8 |
| 8 | 780 | 710 | 752 | 725 | 0 | 0 | 742 | 30.859 | 2.973 | 100.0 |
| 9 | 743 | 752 | 729 | 749 | 0 | 0 | 743 | 10.210 | 9.133 | 100.0 |
| 10 | 684 | 760 | 682 | 663 | 0 | 0 | 697 | 42.890 | 1.102 | 86.7 |

APPENDIX P (Continued)
PAP TEST RESULTS
WICHITA MID-CONTINENT AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-08-1990

PAGE 2

Airport: Wichita Mid-Continent Airport, Wichita, Kansas
FAA Project Name: Runway 1L-19R Reconstruction
Work Area Project Name: Runway 1L-19R Reconstruction - 28-days

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------|-------------|-----------|---------------|
| 11 | 8-01-3 | 08/01/87 | | 28 |
| 12 | 8-05-1 | 08/05/87 | | 28 |
| 13 | 8-05-1 | 08/05/87 | | 28 |
| 14 | 8-05-3 | 08/05/87 | | 28 |
| 15 | 8-05-3 | 08/05/87 | | 28 |
| 16 | 8-07-1 | 08/07/87 | | 28 |
| 17 | 9-09-1 | 09/09/87 | | 28 |
| 18 | 9-09-1 | 09/09/87 | | 28 |
| 19 | 9-10-2 | 09/10/87 | | 28 |
| 20 | 9-10-2 | 09/10/87 | | 28 |
| 21 | 9-10-4 | 09/10/87 | | 28 |
| 22 | 9-10-4 | 09/10/87 | | 28 |
| 23 | 9-13-2 | 09/13/87 | | 28 |
| 24 | 9-13-2 | 09/13/87 | | 28 |
| 25 | 9-13-4 | 09/13/87 | | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI----- | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|----------------------------------|-----|-----|-----|-----|-----|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | |
| 11 | 723 | 672 | 710 | 710 | 0 | 0 | 704 | 22.036 | 2.439 | 100.0 |
| 12 | 749 | 725 | 735 | 715 | 0 | 0 | 731 | 14.514 | 5.581 | 100.0 |
| 13 | 698 | 713 | 725 | 780 | 0 | 0 | 729 | 35.749 | 2.210 | 100.0 |
| 14 | 785 | 810 | 685 | 695 | 0 | 0 | 744 | 63.031 | 1.487 | 99.6 |
| 15 | 723 | 674 | 556 | 576 | 0 | 0 | 632 | 79.492 | -0.223 | 42.6 |
| 16 | 830 | 775 | 616 | 677 | 0 | 0 | 725 | 96.106 | 0.775 | 75.8 |
| 17 | 696 | 813 | 725 | 794 | 0 | 0 | 757 | 55.528 | 1.927 | 100.0 |
| 18 | 710 | 661 | 706 | 764 | 0 | 0 | 710 | 42.161 | 1.429 | 97.6 |
| 19 | 616 | 657 | 601 | 682 | 0 | 0 | 639 | 37.175 | -0.296 | 40.1 |
| 20 | 641 | 631 | 680 | 695 | 0 | 0 | 662 | 30.631 | 0.384 | 62.8 |
| 21 | 691 | 676 | 757 | 713 | 0 | 0 | 709 | 35.274 | 1.680 | 100.0 |
| 22 | 804 | 779 | 770 | 760 | 0 | 0 | 778 | 18.839 | 6.808 | 100.0 |
| 23 | 760 | 660 | 795 | 805 | 0 | 0 | 755 | 66.207 | 1.586 | 100.0 |
| 24 | 672 | 747 | 617 | 694 | 0 | 0 | 683 | 53.830 | 0.604 | 70.1 |
| 25 | 836 | 796 | 742 | 783 | 0 | 0 | 789 | 38.742 | 3.594 | 100.0 |

APPENDIX P (Continued)
PAP TEST RESULTS
WICHITA MID-CONTINENT AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-08-1990

PAGE 3

Airport: Wichita Mid-Continent Airport, Wichita, Kansas

FAA Project Name: Runway 1L-19R Reconstruction

Work Area Project Name: Runway 1L-19R Reconstruction - 28-days

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------|-------------|-----------|---------------|
| 26 | 9-13-4 | 09/13/87 | | 28 |
| 27 | 9-17-2 | 09/17/87 | | 28 |
| 28 | 9-17-2 | 09/17/87 | | 28 |
| 29 | 9-17-4 | 09/17/87 | | 28 |
| 30 | 9-17-4 | 09/17/87 | | 28 |
| 31 | 9-26-1 | 09/26/87 | | 28 |
| 32 | 9-26-1 | 09/26/87 | | 28 |
| 33 | 9-26-2 | 09/26/87 | | 28 |
| 34 | 9-26-2 | 09/26/87 | | 28 |
| 35 | 9-30-2 | 09/30/87 | | 28 |
| 36 | 9-30-2 | 09/30/87 | | 28 |
| 37 | 9-30-4 | 09/30/87 | | 28 |
| 38 | 9-30-4 | 09/30/87 | | 28 |
| 39 | 10-1-2 | 10/01/87 | | 28 |
| 40 | 10-1-2 | 10/01/87 | | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 26 | 793 | 830 | 840 | 800 | 0 | 0 | 816 | 22.780 | 7.276 | 100.0 | 100.0 |
| 27 | 720 | 700 | 823 | 737 | 0 | 0 | 745 | 54.154 | 1.754 | 100.0 | 100.0 |
| 28 | 711 | 654 | 702 | 707 | 0 | 0 | 694 | 26.589 | 1.636 | 100.0 | 100.0 |
| 29 | 813 | 727 | 702 | 717 | 0 | 0 | 740 | 49.902 | 1.799 | 100.0 | 100.0 |
| 30 | 793 | 712 | 760 | 850 | 0 | 0 | 779 | 57.985 | 2.220 | 100.0 | 100.0 |
| 31 | 613 | 721 | 667 | 621 | 0 | 0 | 656 | 49.729 | 0.111 | 53.7 | 0.0 |
| 32 | 636 | 682 | 714 | 678 | 0 | 0 | 678 | 32.016 | 0.859 | 78.6 | 87.9 |
| 33 | 727 | 722 | 678 | 704 | 0 | 0 | 708 | 22.157 | 2.606 | 100.0 | 100.0 |
| 34 | 719 | 709 | 651 | 646 | 0 | 0 | 681 | 38.091 | 0.820 | 77.3 | 86.0 |
| 35 | 699 | 765 | 648 | 750 | 0 | 0 | 716 | 53.132 | 1.233 | 91.1 | 100.0 |
| 36 | 725 | 774 | 735 | 675 | 0 | 0 | 727 | 40.746 | 1.896 | 100.0 | 100.0 |
| 37 | 752 | 798 | 724 | 836 | 0 | 0 | 778 | 49.514 | 2.575 | 100.0 | 100.0 |
| 38 | 879 | 934 | 869 | 727 | 0 | 0 | 852 | 88.255 | 2.292 | 100.0 | 100.0 |
| 39 | 808 | 769 | 725 | 755 | 0 | 0 | 764 | 34.461 | 3.315 | 100.0 | 100.0 |
| 40 | 779 | 853 | 921 | 872 | 0 | 0 | 856 | 58.931 | 3.500 | 100.0 | 100.0 |

APPENDIX P (Continued)
PAP TEST RESULTS
WICHITA MID-CONTINENT AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-08-1990

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Airport: Wichita Mid-Continent Airport, Wichita, Kansas

FAA Project Name: Runway 1L-19R Reconstruction

Work Area Project Name: Runway 1L-19R Reconstruction - 28-days

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------|-------------|-----------|---------------|
| 41 | 10-1-4 | 10/01/87 | | 28 |
| 42 | 10-1-4 | 10/01/87 | | 28 |
| 43 | 10-2-2 | 10/02/87 | | 28 |
| 44 | 10-2-2 | 10/02/87 | | 28 |
| 45 | 10-3-1 | 10/03/87 | | 28 |
| 46 | 10-3-1 | 10/03/87 | | 28 |
| 47 | 10-6-2 | 10/06/87 | | 28 |
| 48 | 10-6-2 | 10/06/87 | | 28 |
| 49 | 10-6-4 | 10/06/87 | | 28 |
| 50 | 10-6-4 | 10/06/87 | | 28 |
| 51 | 10-7-5 | 10/07/87 | | 28 |
| 52 | 10-7-5 | 10/07/87 | | 28 |
| 53 | 10-9-1 | 10/09/87 | | 28 |
| 54 | 10-9-1 | 10/09/87 | | 28 |
| 55 | 10-9-3 | 10/09/87 | | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|-----|-----|------|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 41 | 862 | 808 | 867 | 872 | 0 | 0 | 852 | 29.781 | 6.791 | 100.0 | 100.0 |
| 42 | 862 | 789 | 835 | 905 | 0 | 0 | 848 | 48.630 | 4.066 | 100.0 | 100.0 |
| 43 | 873 | 897 | 810 | 795 | 0 | 0 | 844 | 49.013 | 3.953 | 100.0 | 100.0 |
| 44 | 784 | 911 | 745 | 821 | 0 | 0 | 815 | 70.976 | 2.328 | 100.0 | 100.0 |
| 45 | 825 | 790 | 770 | 755 | 0 | 0 | 785 | 30.277 | 4.459 | 100.0 | 100.0 |
| 46 | 793 | 828 | 852 | 831 | 0 | 0 | 826 | 24.454 | 7.197 | 100.0 | 100.0 |
| 47 | 843 | 887 | 838 | 828 | 0 | 0 | 849 | 26.090 | 7.628 | 100.0 | 100.0 |
| 48 | 838 | 867 | 938 | 959 | 0 | 0 | 901 | 57.321 | 4.370 | 100.0 | 100.0 |
| 49 | 867 | 765 | 791 | 816 | 0 | 0 | 810 | 43.477 | 3.674 | 100.0 | 100.0 |
| 50 | 842 | 755 | 768 | 803 | 0 | 0 | 792 | 39.013 | 3.640 | 100.0 | 100.0 |
| 51 | 865 | 875 | 843 | 955 | 0 | 0 | 885 | 48.864 | 4.799 | 100.0 | 100.0 |
| 52 | 969 | 944 | 840 | 810 | 0 | 0 | 891 | 77.577 | 3.103 | 100.0 | 100.0 |
| 53 | 880 | 895 | 740 | 845 | 0 | 0 | 840 | 69.881 | 2.719 | 100.0 | 100.0 |
| 54 | 857 | 867 | 855 | 680 | 0 | 0 | 815 | 89.987 | 1.831 | 100.0 | 100.0 |
| 55 | 755 | 877 | 808 | 1005 | 0 | 0 | 861 | 108.069 | 1.955 | 100.0 | 100.0 |

APPENDIX P (Continued)
PAP TEST RESULTS
WICHITA MID-CONTINENT AIRPORT

FAA PAYMENT ADJUSTMENT (CONTINUED)
P-501, Portland Cement Concrete Pavement

06-08-1990

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Airport: Wichita Mid-Continent Airport, Wichita, Kansas

FAA Project Name: Runway 1L-19R Reconstruction

Work Area Project Name: Runway 1L-19R Reconstruction - 28-days

| LOT NO. | SAMPLE LOCATION | SAMPLE DATE | TEST DATE | AGE OF SAMPLE |
|---------|-----------------|-------------|-----------|---------------|
| 56 | 10-9-3 | 10/09/87 | | 28 |
| 57 | 10-12-2 | 10/12/87 | | 28 |
| 58 | 10-12-2 | 10/12/87 | | 28 |
| 59 | 10-12-4 | 10/12/87 | | 28 |
| 60 | 10-12-4 | 10/12/87 | | 28 |
| 61 | 10-21-1 | 10/21/87 | | 28 |
| 62 | 10-21-1 | 10/21/87 | | 28 |
| 63 | 10-22-2 | 10/22/87 | | 28 |
| 64 | 10-22-5 | 10/22/87 | | 28 |
| 65 | 10-22-5 | 10/22/87 | | 28 |

| LOT NO. | TEST RESULT STRENGTH IN PSI | | | | | | | STD DEV | EST QL | EST PWL | % PAY FACTOR |
|---------|-----------------------------|------|-----|-----|-----|-----|---------|---------|--------|---------|--------------|
| | # 1 | # 2 | # 3 | # 4 | # 5 | # 6 | AVERAGE | | | | |
| 56 | 833 | 892 | 876 | 851 | 0 | 0 | 863 | 26.166 | 8.140 | 100.0 | 100.0 |
| 57 | 734 | 755 | 834 | 816 | 0 | 0 | 785 | 47.829 | 2.817 | 100.0 | 100.0 |
| 58 | 790 | 740 | 888 | 0 | 0 | 0 | 806 | 75.286 | 2.072 | 100.0 | 100.0 |
| 59 | 999 | 892 | 735 | 855 | 0 | 0 | 870 | 108.896 | 2.023 | 100.0 | 100.0 |
| 60 | 775 | 775 | 925 | 865 | 0 | 0 | 835 | 73.485 | 2.518 | 100.0 | 100.0 |
| 61 | 900 | 960 | 725 | 830 | 0 | 0 | 854 | 100.943 | 2.018 | 100.0 | 100.0 |
| 62 | 965 | 885 | 867 | 928 | 0 | 0 | 911 | 44.033 | 5.933 | 100.0 | 100.0 |
| 63 | 887 | 887 | 926 | 833 | 877 | 813 | 871 | 40.938 | 5.386 | 100.0 | 100.0 |
| 64 | 1122 | 1000 | 806 | 842 | 0 | 0 | 943 | 146.355 | 1.999 | 100.0 | 100.0 |
| 65 | 965 | 838 | 942 | 927 | 0 | 0 | 918 | 55.576 | 4.822 | 100.0 | 100.0 |